

AN ORDINANCE APPROVING A SITE PLAN REVISION FOR PROPERTY AT 7200 N. BROADWAY.

WHEREAS, pursuant to Section 32-37 of Ordinance No. 2.292 being the Gladstone Zoning Ordinance, public notice was made of a request for site plan approval at 7200 N. Broadway; and

WHEREAS, public hearings have been held after the publishing of the required notices; and

WHEREAS, the City Council finds that the planned development does not materially injure the property and the uses of the properties immediately adjacent to the proposed development; and

WHEREAS, the City Council finds that the site plan presents a unified and organized arrangement of buildings and facilities which have a functional relationship to the property comprising the development; and

WHEREAS, the City Council finds it is in the best interest of the citizens of the City of Gladstone that the site plan submitted by the applicant be approved subject to the terms and conditions set forth herein;

NOW, THEREFORE, BE IT ORDAINED BY THE COUNCIL OF THE CITY OF GLADSTONE, MISSOURI, AS FOLLOWS:

SECTION 1. SITE PLAN APPROVAL.

The Site Plan for 7200 N. Broadway is hereby approved subject to the terms and conditions set forth herein;

1. Any and all disturbed areas shall be sodded.
2. All manicured grass and landscaped areas shall be irrigated and maintained in perpetuity.
3. Install a minimum of 20 new shrub plantings adjacent to N. Broadway.
4. Install a minimum of 10 new shrub plantings adjacent to NE 72nd Street.
5. All mechanical equipment on the roof shall be screened from public view by a parapet or approved screening similar in design to the rest of the structure. This must be a minimum of twelve (12) inches above the tallest piece of mechanical equipment.
6. A compliant monument sign shall be used to serve the development. The monument sign will need a minimum of 240 sq. ft. of area landscaping around the sign.
7. All exterior lighting on the site shall be LED and designed to reduce adverse impact on adjoining properties.
8. The dumpster shall be enclosed with materials consistent with the primary building. Specific colors and materials shall be submitted and approved as part of the building permit.
9. Trash service, store deliveries, and gasoline refilling (underground commercial gasoline tanks) shall occur between the hours of 7:00 a.m. to 10:00 p.m.
10. Tractor trailers, storage containers, and other commercial vehicles (including delivery trucks) shall not be parked or stored overnight on the premises.

11. No more than 50% of each glazed window area of the building shall have signage.
12. Hours of operation permitted are 24 hours seven days per week.
13. Install a commercial grade bike rack on-site.
14. Install new curb, gutter, and sidewalk along the property line adjacent to N. Broadway.
15. Preserve the northern wooded tree line as a buffer to the residential neighborhood located to the north along NW 72nd Terrace.
16. Complete a Post-Construction Maintenance Agreement for storm water facilities.
17. Install a fire hydrant within four-hundred (400) feet of any portion of the building.
18. Extend and loop the 8-inch water main along N. Broadway.
19. Given the project location and that the development extends to property located in Kansas City, Missouri, this development is subject to Kansas City, Missouri approving the improvements on their parcel.
20. The installation and construction of a left turn lane or right-in/right-out for the entrance on N. Broadway at the property owner's expense.

SECTION 2. SEVERABILITY CLAUSE. The provisions of this ordinance are severable and if any provision hereof is declared invalid, unconstitutional or unenforceable, such determination shall not affect the validity of the remainder of this ordinance.

INTRODUCED, READ, PASSED, AND ADOPTED BY THE COUNCIL OF THE CITY OF GLADSTONE, MISSOURI, THIS 10TH DAY OF JUNE 2024.

Tina M. Spallo, Mayor

ATTEST:

Kris Keller, City Clerk

First Reading: June 10, 2024

Second Reading: June 10, 2024

File # 24-00002



Request for Council Action

RES ☐ # City Clerk Only

BILL ☒ # 24-19

ORD ☒ # ~~4-674~~

Date: 6/4/2024

Department: Community Development

Meeting Date Requested: 6/10/2024

Public Hearing: Yes ☒ Date: 6/10/2024

Subject: 7200 N. Broadway – Gas Station & Convenience Store – Site Plan Revision

Background:

Update: City Staff has requested the following from the applicant after the Planning Commission meeting on Monday, May 20th:

- To have the traffic engineers present at the City Council meeting to answer any traffic related questions in more detail.
- Provide renderings of the west side of the store that will give a better visual of the drive thru and backside of the store.
- To be prepared to discuss and show the potential left turn lane installation and the right-in/right-out traffic mitigation options in some detail.

Narrative: The applicant is requesting site plan approval for the purpose of constructing a new 5,000 sq. ft. gas station and convenience store located at 7200 N. Broadway. This property is currently vacant and zoned CP-2 which is an appropriate zoning for the proposed use.

This project was proposed in 2023 and denied by the Gladstone City Council. The property owner has made adjustments to the site plan and those adjustments include the following:

- The access point on NW 72nd Street has been shifted west to lineup with the Post Office access point.
- The water quality pond has been moved from the northern side of the property to the western side of the property away from the residential homes located to the north. This basin will be located on the KCMO parcel.
- The wooded area on the northern side of the property will primarily remain untouched.

This project will also incorporate a drive thru lane and window as well as two (2) electric vehicle (EV) charging stations and a commercial bike rack. There will be ten (10) fuel pumps covered by a canopy to serve customers.

The primary exterior building materials used will be brick and stucco.

The landscaping plans show new landscape throughout the property using various trees and shrubs. All disturbed areas will be sodded and irrigated.

A traffic study was conducted by Priority Engineers, Inc. and they provided a summary of their findings.

- “Analysis of unsignalized intersections indicate that they operate with acceptable levels of service both before and after the construction of the proposed development. The signalized intersection at NW 72nd Street and N Broadway Street has an overall level of service that is acceptable both before and after construction of the proposed development. The proposed entrance locations have sufficient sight distance. A left turn lane is warranted for the entrance on N Broadway Street in the PM Peak Hour. Due to geometric constraints of this location, the left turn lane will need to be designed so that it does not interfere with the southbound left turn lane at the signalized intersection with NW 72nd Street. No other improvements are required as a result of this development.”
- Given the conclusions and recommendations made by the traffic engineers, City Staff will be requiring the installation and construction of a left turn lane or right-in/right-out for the entrance on N. Broadway at the property owner’s expense.

Budget Discussion: N/A

Public/Board/Staff Input:

Public: There were approximately 5-10 people in the audience who attended the Planning Commission hearing that are in opposition to the proposed project. These individuals live in the neighborhood of NW 72nd Terrace, which is north of the proposed project.

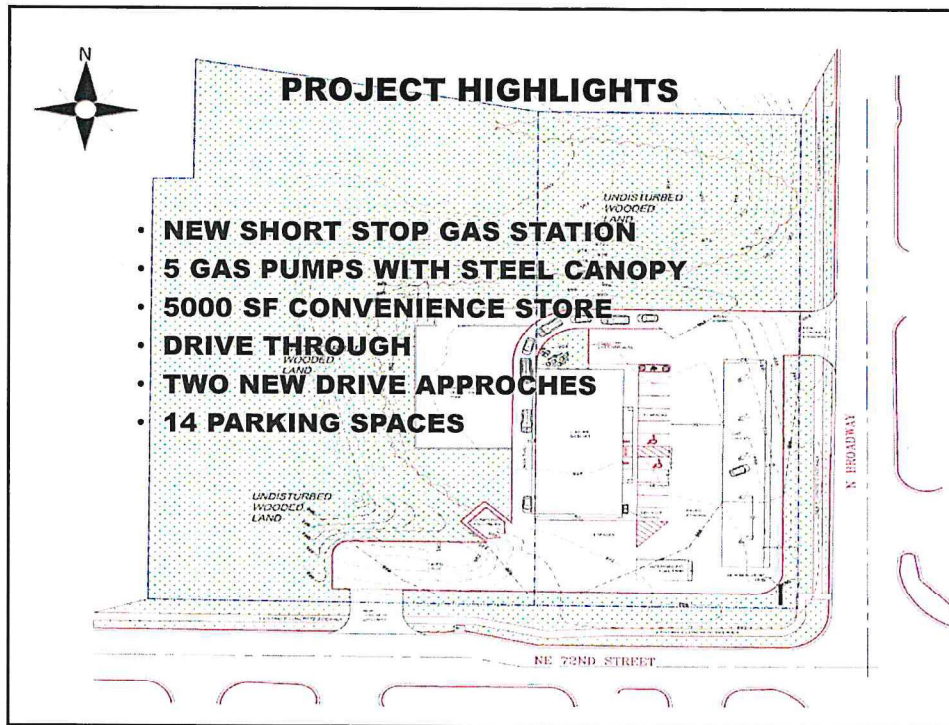
Board: The Planning Commission approved the project. (7 Yes – 1 No)

Provide Original Contracts, Leases, Agreements, etc. to: City Clerk and Vendor.

Austin Greer
Department Director/Administrator

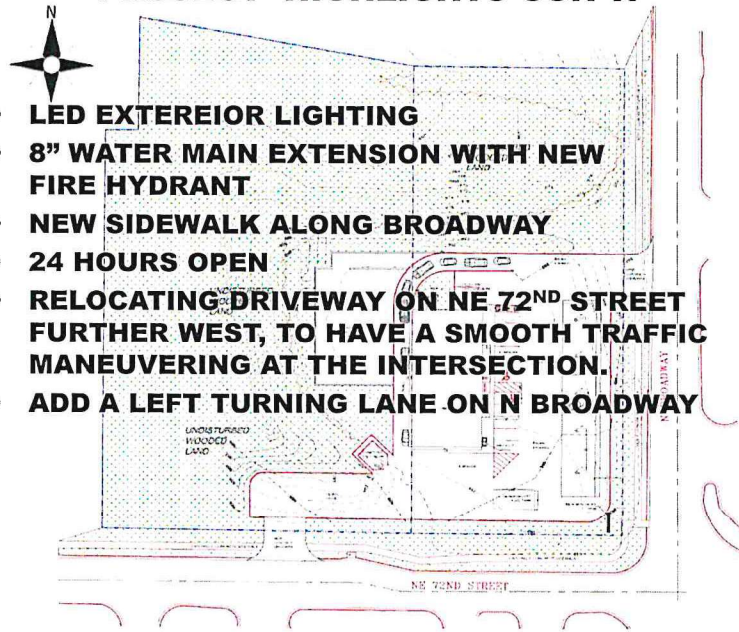
JM
City Attorney

BB
City Manager



PROJECT HIGHLIGHTS CON'T:

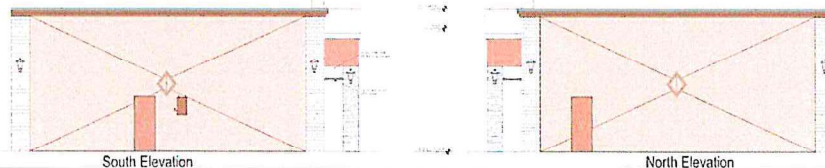
- LED EXTEREIOR LIGHTING
- 8" WATER MAIN EXTENSION WITH NEW FIRE HYDRANT
- NEW SIDEWALK ALONG BROADWAY
- 24 HOURS OPEN
- RELOCATING DRIVEWAY ON NE 72ND STREET FURTHER WEST, TO HAVE A SMOOTH TRAFFIC MANEUVERING AT THE INTERSECTION.
- ADD A LEFT TURNING LANE ON N BROADWAY



C-STORE BUILDING ELEVATIONS



- CONSTRUCTED OF CONCRETE BLOCKS
- METAL BAR JOIST ROOF SYSTEM
- BRICK AND STONE EXTERIOR
- CONCRETE STUCCO ON SIDE AND REAR
- HIGH PARAPET TO SCREEN MECHANICAL UNITS
- LESS THAN 50% GLAZING TO HAVE SIGNAGE
- MATCHING ENCLOSED TRASH DUMPSTER



SITE PLAN RENDERING



BUILDING & CANOPY RENDERING



BUILDING & CANOPY RENDERING



LANDSCAPING HIGHLIGHTS:

- **ONLY 30% AREA DEVELOPED**
- **70% AREA MOSTLY HAVING MATURE TREES TO REMAIN**
- **MAINTAINING EXISTING WOODED AREAS. NOT DISTURBING ANYTHING TO THE NORTH.**

LANDSCAPING HIGHLIGHTS CON'T:

- **BUILT IN IRRIGATION SYSTEM**
- **PLANTING TREES AND SHRUBS ALONG BROADWAY AND 72ND STREET**
- **ALL DISTURBED AREAS SODDED**
- **PLANTING NEW VEGETATION TO THE WEST**

PLANNING COMMISSION
GLADSTONE, MISSOURI
Gladstone Community Center
Monday, May 20th, 2024
7:00 pm

Item 1 on the Agenda: Roll Call.

Present: Kate Middleton
Bill Turnage
Jennifer McGee
Joseph Brancato
Cameron Nave Secretary
Robert Wilson
Steve Beamer Chair
Mike Ebenroth

Absent: Chase Cookson
Brenda Lowe, V-Chair
Kim Murch

Council & Staff Present:

Austin Greer, Assistant City Manager | Community Development Director
Alan Napoli, Community Development Administrator/Building Official
Angie Daugherty, Admin. Assistant
Jean B. Moore, Councilmember
Tina Spallo, Mayor

Item 2 on the Agenda: Pledge of Allegiance.

Chair Beamer led the group in reciting the Pledge of Allegiance to the United States of America.

Item 3 on the Agenda: Approval of the April 1st, 2024 Minutes. Chair Beamer asked if there was a motion to approve the minutes from the April 1st meeting.

Mr. Turnage moved to approve the minutes; Ms. McGee seconded. The minutes were approved, 8-0.

Item 4 on the Agenda: Consideration: On a Site Plan Revision on property located at 7200 N. Broadway.

Applicant: Gerald W. Menefee P.E.

Owner: Mohammad Hafiz

City Council consideration for this project is scheduled for Monday, June 10, 2024.

Mr. Greer read from the staff report:

The applicant is requesting site plan approval for the purpose of constructing a new 5,000 sq. ft. gas station and convenience store located at 7200 N. Broadway. This property is currently vacant and zoned CP-2 which is an appropriate zoning for the proposed use.

This project was proposed in 2023 and denied by the Gladstone City Council. The property owner has made adjustments to the site plan and those adjustments include the following:

- The access point on NW 72nd Street has been shifted west to lineup with the Post Office access point.
- The water quality pond has been moved from the northern side of the property to the western side of the property away from the residential homes located to the north. This basin will be located on the KCMO parcel.
- The wooded area on the northern side of the property will primarily remain untouched.

This project will also incorporate a drive thru lane and window as well as two (2) electric vehicle (EV) charging stations and a commercial bike rack. There will be ten (10) fuel pumps covered by a canopy to serve customers.

The primary exterior building materials used will be brick and stucco.

The landscaping plans show new landscape throughout the property using various trees and shrubs. All disturbed areas will be sodded and irrigated.

A traffic study was conducted by Priority Engineers, Inc. and they provided a summary of their findings.

- "Analysis of unsignalized intersections indicate that they operate with acceptable levels of service both before and after the construction of the proposed development. The signalized intersection at NW 72nd Street and N Broadway Street has an overall level of service that is acceptable both before and after construction of the proposed development. The proposed entrance locations have sufficient sight distance. A left turn lane is warranted for the entrance on N Broadway Street in the PM Peak Hour. Due to geometric constraints of this location, the left turn lane will need to be designed so that it does not interfere with the southbound left turn lane at the signalized intersection with NW 72nd Street. No other improvements are required as a result of this development."
- Given the conclusions and recommendations made by the traffic engineers, City Staff will be requiring the installation and construction of a left turn lane or right-in/right-out for the entrance on N. Broadway at the property owner's expense.
-

City Staff recommends that the following conditions be considered if the Planning Commission and City Council choose to approve this project request:

1. Any and all disturbed areas shall be sodded.
2. All manicured grass and landscaped areas shall be irrigated and maintained in perpetuity.
3. Install a minimum of 20 new shrub plantings adjacent to N. Broadway.
4. Install a minimum of 10 new shrub plantings adjacent to NE 72nd Street.
5. All mechanical equipment on the roof shall be screened from public view by a parapet or approved screening similar in design to the rest of the structure. This must be a minimum of twelve (12) inches above the tallest piece of mechanical equipment.

6. A compliant monument sign shall be used to serve the development. The monument sign will need a minimum of 240 sq. ft. of area landscaping around the sign.
7. All exterior lighting on the site shall be LED and designed to reduce adverse impact on adjoining properties.
8. The dumpster shall be enclosed with materials consistent with the primary building. Specific colors and materials shall be submitted and approved as part of the building permit.
9. Trash service, store deliveries, and gasoline refilling (underground commercial gasoline tanks) shall occur between the hours of 7:00 a.m. to 10:00 p.m.
10. Tractor trailers, storage containers, and other commercial vehicles (including delivery trucks) shall not be parked or stored overnight on the premises.
11. No more than 50% of each glazed window area of the building shall have signage.
12. Hours of operation permitted are 24 hours seven days per week.
13. Install a commercial grade bike rack on-site.
14. Install new curb, gutter, and sidewalk along the property line adjacent to N. Broadway.
15. Preserve the northern wooded tree line as a buffer to the residential neighborhood located to the north along NW 72nd Terrace.
16. Complete a Post-Construction Maintenance Agreement for stormwater facilities.
17. Install a fire hydrant within four-hundred (400) feet of any portion of the building.
18. Extend and loop the 8-inch water main along N. Broadway.
19. Given the project location and that the development extends to property located in Kansas City, Missouri, this development is subject to Kansas City, Missouri approving the improvements on their parcel.
20. The installation and construction of a left turn lane or right-in/right-out for the entrance on N. Broadway at the property owner's expense.

City Staff recommends that the request be **APPROVED** contingent upon the conditions listed above.

Mr. Menefee who is the applicant on the project presented a PowerPoint.

Mr. Menefee stated that this will be a convenience store with five gas pumps, a drive thru, 14 parking spaces, EV charging stations, exterior lighting along the north side, the water main extension and sidewalk, and open 24 hours. They will also add an access drive off of Broadway and NE 72nd St. Only 30% of the area will be developed and the other 70% has mature trees. They will have storage pipes on the northern edge of the site and those will be connected to the water retention pond on the west side of the structure. Thank you.

Ms. Middleton asked what part of this property is in Kansas City.

Mr. Menefee stated the western parcel that has the basin and west side of the driveway.

Mr. Turnage asked who will be in charge of redesigning the drive from Broadway.

Mr. Greer stated that private sector engineers hired by the property owner will likely design the project and submit the designs to city staff for review.

Ms. McGee asked where the retaining wall was going and how tall will it be.

Mr. Menefee stated the wall will be along the tree line and around 10 to 12 feet tall at the tallest point.

Mr. Wilson asked if he could explain the difference between the basin and a sand and oil separator pit.

Mr. Menefee stated it is based on the volume of the water that comes off the site. It is a large area and with a lot of rain fall this goes into the retention pond and the sand filtration is basically the same thing. The filter is made up of primarily tree bark and peat moss.

Mr. Brancato asked how the public is supposed to gain access to the drive thru and whether or not they will have to drive around the back of the building and face N. Broadway or NW 72nd Street. Also, will the drive thru be open for 24 hours as well?

Mr. Menefee stated he isn't sure about the hours that the drive thru will be open but assumes it will be dependent on customer demand. The drive thru comes in at the north side and goes south along the building facing NW 72nd St.

Mr. Beamer asked about approval from Kansas City. Do you all have a status on this?

Mr. Menefee stated they have not brought this project to Kansas City yet as we would like to get permission from the City of Gladstone first.

Mr. Beamer asked if this property has historically been vacant or have there been other approved plans on this site.

Mr. Greer stated yes, a Casey's gas station and a dentistry has been approved on this site historically but neither pursued the actual construction of the projects.

Mr. Beamer welcomed the audience to speak in favor or against the proposed project.

Mr. and Ms. Weatherford who reside at 403 NW 72nd Terrace stated that since there is a Casey's at one end of Broadway and a QuikTrip on the other so why do we need another gas station in the middle of residential? That area is full of residential homes. Will the sales from the Short Stop be mostly gas or alcohol? This is a very dangerous intersection and we are very concerned about traffic and wrecks. Are there plans to look at this intersection?

Ms. Josie Nabavian who resides at 400 NW 72nd Terrace asked what has changed from the last meeting? What is going to be the traffic pattern? There is a lot of traffic in that area. With the exit off of Broadway into the gas station, will this make a traffic delay?

Mr. Greer stated that a traffic study has been completed and the study indicates a left turn lane is warranted traveling northbound. Staff is requiring that the property owner add a left turn lane or a right-in/right-out to help mitigate traffic.

Mr. Tyson who resides at 308 NW 76th St. asked when you mention right-in and right-out will this be right lane going into the gas station parking lot and right turn only coming out of the parking lot on N. Broadway?

Mr. Greer stated yes sir.

Mr. Tyson stated that the city cannot control the traffic off of 76th St. or 72nd St.

Mr. Greer stated that the design of the right-in and right-out will be built high enough that most people will try not to drive over it.

Mr. Tyson brought up traffic control and that he doesn't think the police department does enough to stop people from speeding on Broadway. This property has been vacant for so long and I don't understand why they want to put a gas station there.

Ms. Vicki Marshall resides at 401 NW 72nd Terrace and her concern is that she feels like this project will be in her backyard. What if they have a gas leak from the tanks? When they first moved here they were told that it was zoned for an office building and that was in 1992.

Mr. Menefee stated that it is a requirement that they have a containment system that has a double wall tank that is surrounded by a plastic liner.

Ms. Taylor Sherrill who resides at 6305 N. Bales Avenue stated that this project from an environmental perspective does not seem to be compatible with the recent comprehensive plan and that this project does not fit the location.

MOTION: By Ms. Middleton, second by Mr. Ebenroth to consider a Site Plan Revision located at 7200 N Broadway.

Vote: Mr. Wilson	Yes
Mr. Brancato	Yes
Mr. Turnage	Yes
Ms. Middleton	No
Chair Beamer	Yes
Ms. McGee	Yes
Mr. Nave	Yes
Mr. Ebenroth	Yes

The motion carried. (7-1)

Item 5 on the Agenda: Communications from the City Council

Councilmember Jean Moore wanted to welcome everyone to the new space and Mr. Bob Wilson to the Planning Commission. She also thanked the residents for their participation tonight.

Item 6 on the Agenda: Communications from the City Staff

Mr. Greer welcomed Mr. Wilson to the Commission as well. With the storms that happened last night the city will be offering free brush disposable at Public Works today through Friday. City Hall will be closed next Monday for Memorial Day and Food, Art, and Drink will be at Linden Square on June 1st. Also, there will be no Planning Commission meeting on Monday, June 3rd.

Item 7 on the Agenda: Communications from the Planning Commission Members

Mr. Beamer welcomed Mr. Wilson to the Planning Commission and asked Mr. Wilson to tell them a little about himself.

Mr. Wilson stated that he is an architect by trade and is leading an architectural firm here in Kansas City. I was also on the Capital Improvements Committee and am very excited to join the Planning Commission and help the community.

Mr. Turnage wanted to thank the Public Works Department for sponsoring the beautification event.

Item 8 on the Agenda: Adjournment

Chair Beamer adjourned the meeting at 7:39 pm.

Respectfully submitted:

Steve Beamer, Chair

Approved as submitted _____

Angie Daugherty, Recording Secretary

Approved as corrected _____

DEVELOPMENT APPLICATION



CITY OF GLADSTONE
7010 N HOLMES STREET
GLADSTONE, MISSOURI 64118
PHONE: 436-4110 FAX: 436-2228

File #:
Application Date: 04/01/2024
PC Date: _____
CC Date: _____

Application Type:

- | | |
|--|---|
| <input type="checkbox"/> (PH) Special Use Permit (\$500) | <input type="checkbox"/> (PH) Right-of-Way Vacation (\$200) |
| <input type="checkbox"/> (PH) Zoning Change (\$500) | <input type="checkbox"/> (PH) Variance – BZA (\$200) |
| <input type="checkbox"/> (PH) Site Plan Revision (\$500) | <input type="checkbox"/> Final Plat/Replat (\$75) |

Address of Action: 400 NE 72ND STREET

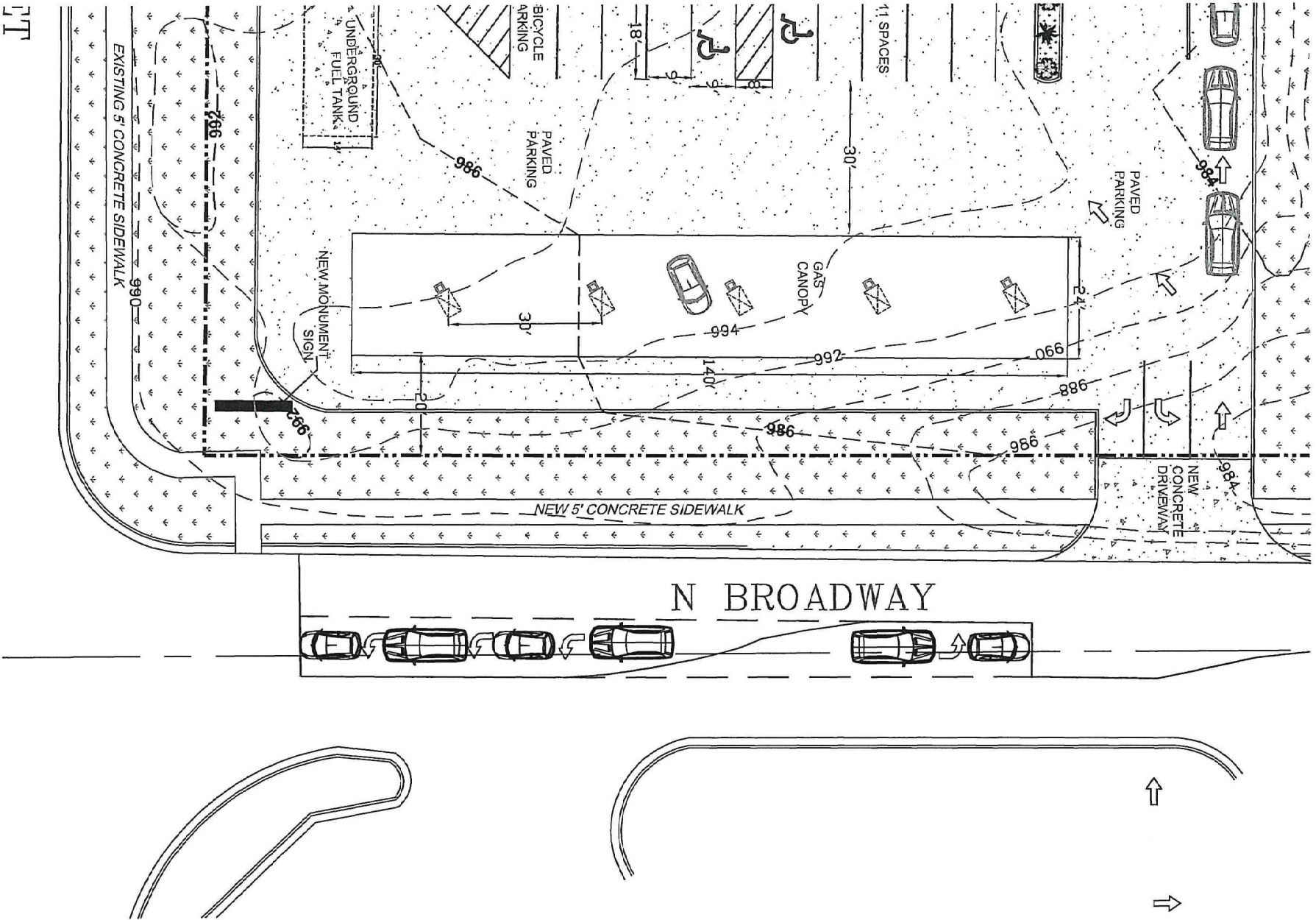
Legal Description: BEG SW COR LT 12 WILLOW CREEK E146, S340,
Attach under separate cover if SW21.21, W138, N TO POB
needed.

Proposed Change: CONSTRUCTION OF NEW GAS STATION WITH 5000
SF CONVENIENCE STORE AND 5 GAS DISPENSERS
AND DRIVE THRU

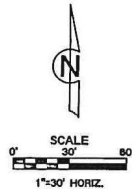
Applicant/Property Owner Information:

- ☐ Applicant/Engineer GERALDW MENEFEE, P.E.
Company KAM DESIGN GROUP LLC
Address 9000 E BANNISTER ROAD, KANSAS CITY MO 64134
Phone 8167972065 Fax: _____ E-Mail: kamdesign@aol.com
- ☐ Property Owner (if different than applicant) MOHAMMAD HAFIZ
Company _____
Address 1121 SW BLAZINGSTAR CT., LEE'S SUMMIT MO 64081
Phone 816 7861622 Fax: _____ E-Mail: mhafiz103@yahoo.com
- ☐ Architect DARRYL W HAWKINS AIA
Company INNOVATIVE DESIGN & RENOVATION
Address 8011 PASEO SUITE 201, KANSAS CITY, MO 64131
Phone 8164052159 Fax: _____ E-Mail: arkitec35@aol.com
Please indicate in one box above which person is to be the contact.

Applicant's Signature *Mohammad Hafiz* Date 4/1/24



Recorded in Clay County, Missouri
 Date and Time: 08/12/2010 at 08:58:37 AM
 Instrument Number: 2010027034
 Book: M Page: 12
 Instrument Type: SURV
 Page Count: 1
 Recording Fee: \$6800.00
 Grantor: 72ND & BROADWAY
 Grantee: 72ND & BROADWAY
 Robert T. Luten, Recorder



PLAN LEGEND

SURVEY MARKERS

- FOUND SECTION CORNER (MONUMENTATION AS NOTED)
- FOUND PROPERTY CORNER (MONUMENTATION AS NOTED)
- SET 1/2" IRON BAR WITH PLASTIC CAP
- BENCHMARK
- OK GAS LINE MARKER
- SMH SANITARY MANHOLE
- UTILITY LINES
- EGGH — ELECTRIC, OVERHEAD
- 100 — INDEX CONTOURS
- 100 — INTERMEDIATE CONTOURS

ELECTRIC

- GUY GUY ANCHOR
- LP LIGHT POLE
- PP POWER POLE

STORM

- CI CURB INLET
- SMH STORM MANHOLE

WATER

- WV WATER VALVE

TRAFFIC

- TSP TRAFFIC SIGNAL POLE
- TSC TRAFFIC SIGNAL CONTROLS
- TSP TRAFFIC SIGNAL VAULT

TELEPHONE

- FOM FIBER OPTIC MARKER

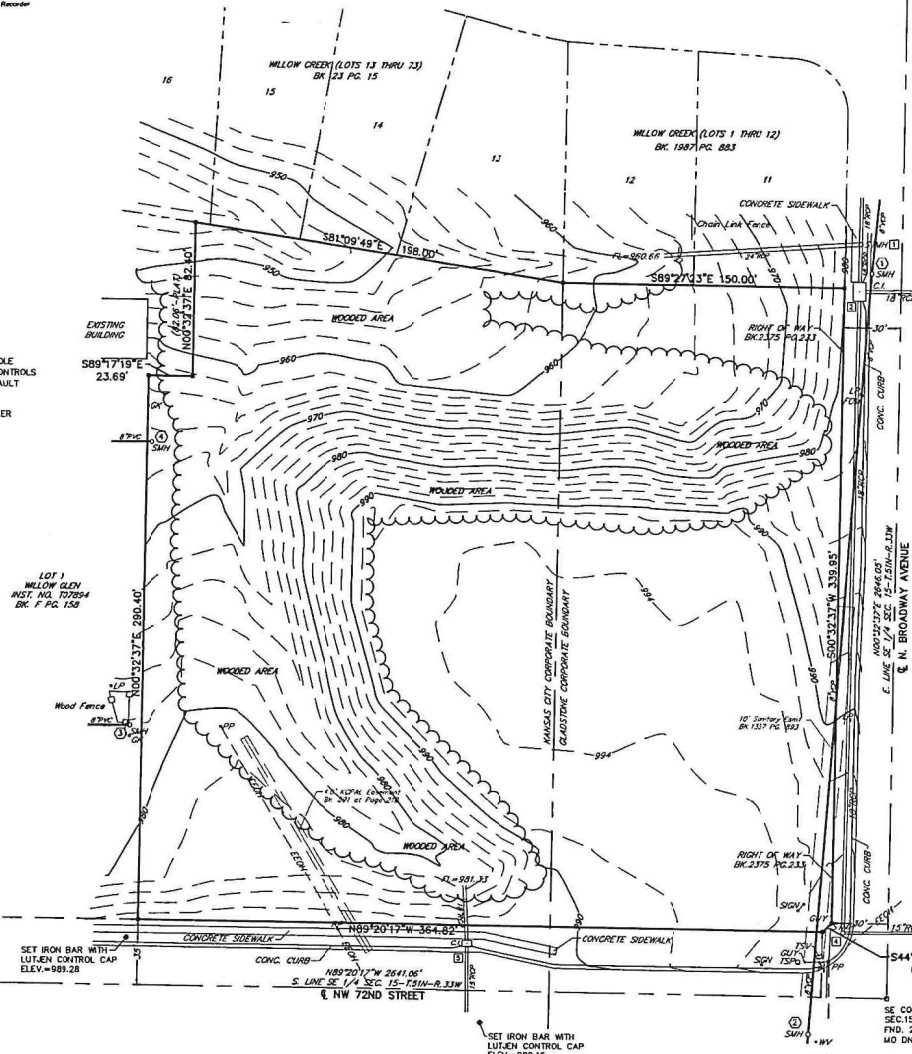
STORM INVERTS

- 1 TOP MH-986.66
FL IN S-971.16
FL IN N-976.06
FL OUT W-961.96
- 2 TOP CI-980.45
FL IN S-972.80
FL IN E-976.65
FL OUT N-973.45
- 3 TOP CI-980.45
FL OUT W-973.96
- 4 TOP MH-996.00
FL IN E-985.60
FL OUT N-982.70
- 5 TOP CI-988.79
FL IN S-983.69
FL OUT N-982.70

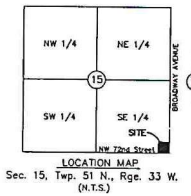
SANITARY INVERTS

- 1 TOP SMH-980.17
FL IN S-975.17
FL OUT W-974.97
- 2 TOP SMH-996.38
FL IN S-985.38
FL OUT N-984.38
- 3 TOP SMH-978.32
FL OUT W-966.92
- 4 TOP SMH-966.74
FL OUT W-955.24

LOT 1
MILLOW CREEK
NOTED NO. 707094
BK. F PG. 150



NE CORNER SE 1/4
 SEC. 15-T.51N-R.33W
 FND. 2" BRASS CAP
 MO DNR. DOC NO. 600-51378



Property Description:

A tract of land in the Southeast Quarter of Section 15, Township 51 North, Range 33 West of the 5th Principal Meridian in Kansas City and Gasstone, Clay County, Missouri, being bounded and described as follows: Beginning at the Southeast corner of Lot 11, MILLOW CREEK (LOTS 1 THRU 12), a subdivision of land in said Clay County, thence South 00°32'37" West, along the West right-of-way line of N. Broadway Avenue, as now established, 339.95 feet; thence South 44°27'23" West, continuing along said West right-of-way line, 6.92 feet to a point on the North right-of-way line of NW 72nd Street, as now established; thence North 89°27'19" West, along said North right-of-way line, 364.82 feet to the Southeast corner of MILLOW CREEK, a subdivision of land in said Clay County, Missouri; thence North 00°32'37" East, along the East line of said MILLOW CREEK (LOTS 1 THRU 12); thence South 89°27'19" East, continuing along said East line, 23.69 feet; thence North 00°32'37" East, continuing along said East line 82.40 feet (82.06' Plat) to a point on the South line of MILLOW CREEK (LOTS 13 THRU 23), a subdivision of land in said Clay County, Missouri; thence South 81°09'49" East, along the South line of said MILLOW CREEK (LOTS 13 THRU 23); thence South 89°27'23" East, along the South line of said MILLOW CREEK (LOTS 1 THRU 12); 150.00 feet to the Southwest corner of Lot 12, said of said MILLOW CREEK (LOTS 1 THRU 12); 150.00 feet to the Point of Beginning. Containing 125,666 square feet or 2.96 acres, more or less.

SURVEYOR'S NOTES:

- Property information referencing this survey was taken from the Commitment for Title Insurance Report, issued by Integrity Land Title Company, Inc., Firm File No. KC-IT-7089-10, with an effective of May 14, 2010 at 8:00 a.m.
- Bearings used herein are based on the Missouri State Plane Coordinate System, NAD 1983, West Zone. Vertical Datum is based on the North American Vertical Datum of 1988 (NAVD 88).
- The underground utilities shown herein have been located from field survey information, existing drawings and marking provided by Missouri One Call System, Inc. The surveyor makes no guarantee that underground utilities shown comprise all such utilities in the area, either in service or abandoned. The surveyor further does not certify that they are located as accurately as possible from information available at the time of survey. The surveyor has not physically located the underground facilities.
- Field work was completed in May 2010.

SE CORNER SE 1/4
 SEC. 15-T.51N-R.33W
 FND. 2" BRASS CAP
 MO DNR. DOC NO. 600-51391

CERTIFICATION

I hereby certify that this survey was prepared by me or under my direct personal supervision and that I am a duly licensed Professional Land Surveyor under the laws of the State of Missouri and that this survey was performed in accordance with the requirements of the current Missouri Minimum Standards for Professional Land Surveyors.

JASON S. ROTH
 DATE: 6-2-10

BOUNDARY / TOPOGRAPHIC SURVEY
 72ND AND BROADWAY
 SEC. 15 - T.51N - R.33W
 KANSAS CITY, CLAY COUNTY, MISSOURI

DATE OF SURVEY: 05-02-10

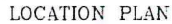
Location: S:\Projects\UNSUBS\15-51-33\10081-01-(72nd and Broadway)\10081-01-72nd and Broadway End - 6-2-10.dwg

Surveyed By: ZB / KB
 Reviewed By: BAL
 Drafted By: JR
 Luten Project No.: 10081



1301 Burlington, #103
 Kansas City, MO 64108
 816.467.4200
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 surveying
 planning
 engineering
 infrastructure

Sheet No.:
 1 of 1



400 NE 72ND STREET, GLADSTONE, MISSOURI



BEG SW COR LT 12 WILLOW CREEK E146, S340, SW21-21, W138, N TO POB

BEG SE COR LT 13 WILLOW CRK, S TO NL NW 72ND ST, W210, N290.4, E23.69, N82.06, SELY TO POB

 EXISTING/PROPOSED CONCRETE SURFACE
 GRASS COVER
 BUILDING OUTLINE
 PROPERTY LINE
 FIRE HYDRANT
 STREET CENTER LINE



EXISTING ZONING	CP1 (GLADSTONE)
PROPOSED ZONING	CP1
TOTAL LAND	1.19 ACRES
LAND AREA FOR EXISTING & PROPOSED STREET RIGHT-OF-WAY	NONE
NET LAND AREA OR ACRES PROPOSED USE	1.19 ACRES
BUILDING HEIGHT	M - GAS STATION WITH 5,000 SFT CONVENIENCE STORE SINGLE STORY BUILDING 11 FEET C-STORY A 5,000 SFT STORE
GROSS FLOOR AREA / BUILDING COVERAGE / FLOOR AREA RATIO / PARKING SPACES REQUIRED	0.10 % 24 SPACES PER 1000 SFT OF RETAIL SPACE (13 SPACES) 14 SPACES PLUS TWO ELECTRIC CAR CHARGING SPACES INCLUDING 1 ACCESSIBLE SPACE
PARKING SPACES PROVIDED	24 SPACES
BICYCLE PARKING REQUIRED	3 BICYCLE SPACES
BICYCLE PARKING PROVIDED	3 BICYCLE SPACES WITH 2 LONG TERM SPACE
BUSINESS START DATE	SPRING 2024
EASEMENTS	NONE
HOURS OF OPERATION	24 HOURS
EXISTING PARKING LOT	CONCRETE/ASPHALT COVERED
PROPOSED PARKING LOT	CONCRETE PAVEMENT

PLEASE SEE ELEVATION PLANS THAT SHOW THE BUILDING EXTERIORS

DEVELOPER
MPS CONTRACTING LLC
14926 BENSON STREET
OVERLAND PARK, KS 66221

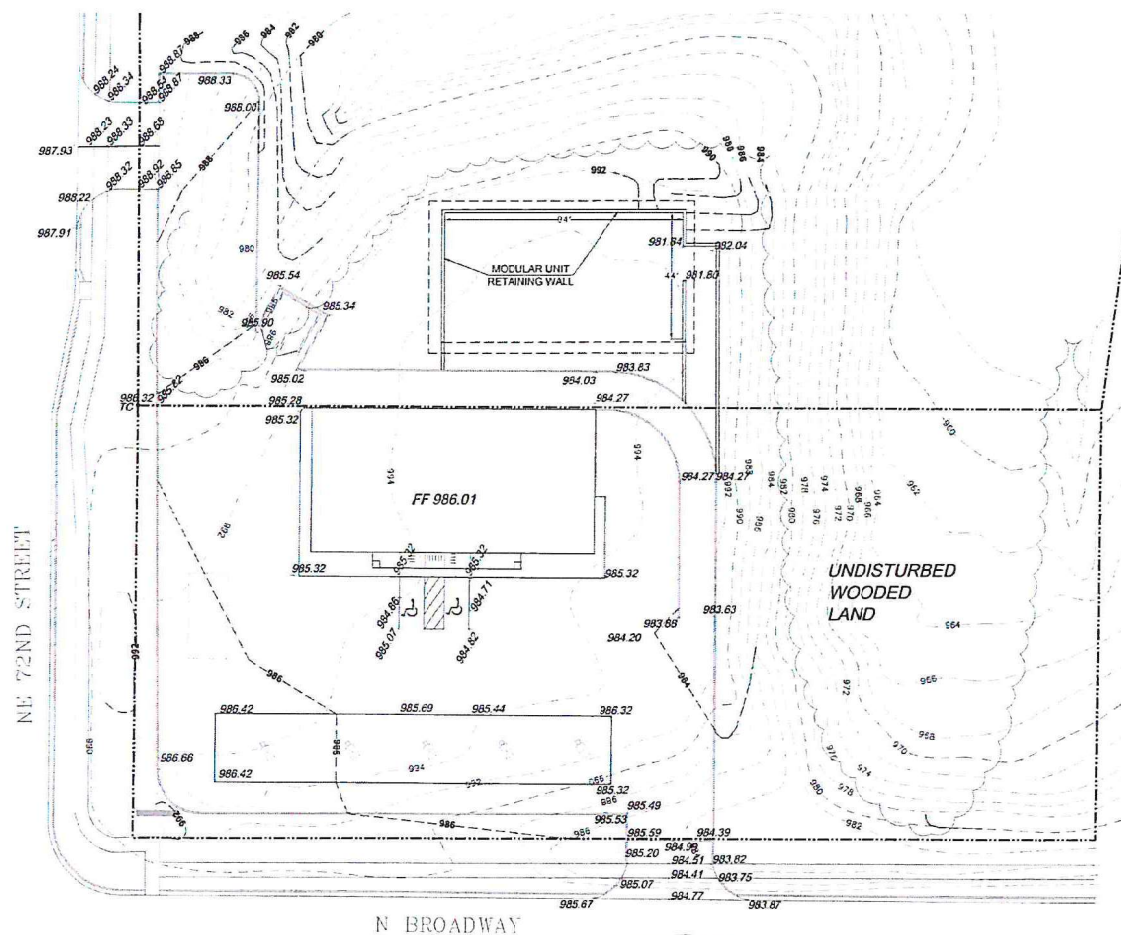
No.	Description
1	SITE PLAN
2	FLOOR PLAN & DETAILS
3	BUILDING ELEVATIONS
4	BUILDING ELEVATION RENDERING
5	GRADING PLAN
6	DETAILS SHEET I
7	DETAILS SHEET II
8	UTILITY PLAN
9	ELECTRICAL PHOTOMETRIC PLAN
10	LANDSCAPING PLAN



400 NE 72ND STREET
GLADSTONE, MISSOURI

Project number	2023-109
Drawn by	KRB
Checked by	GWM

SHEET 1



LEGEND

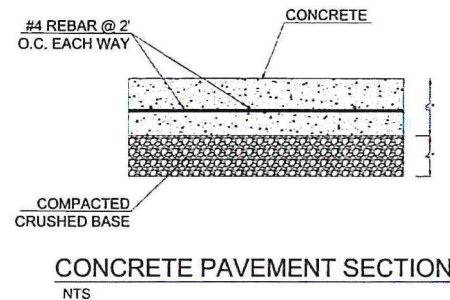
- BUILDING OUTLINE
- - - PROPERTY LINE
- 809.92 SPOT ELEVATIONS
- 809.92 TOP OF CURB ELEVATION
- 809.42 TOP OF PAVEMENT ELEVATION
- - - EXISTING CONTOUR
- - - PROPOSED CONTOUR

GRADING PLAN



GENERAL NOTES:

1. THE CONTRACTOR SHALL NOTIFY THE ENGINEER OF ANY OBSERVED DISCREPANCIES IN DIMENSIONS, DETAILING, OR OTHER ITEMS AS SHOWN ON THE PLANS OR SPECIFIED PRIOR TO PROCEEDING WITH WORK RELATED TO SAID DISCREPANCIES.
2. ALL WORK SHALL BE DONE IN ACCORDANCE WITH LOCAL CODES.
3. CONTRACTOR SHALL INCLUDE ALL LABOR, MATERIAL, AND EQUIPMENT TO PROVIDE COMPLETE AND FUNCTIONING INSTALLATIONS, AND ALL MATERIAL AND EQUIPMENT SHALL BE NEW UNLESS OTHERWISE SPECIFIED.
4. ACCEPTANCE OF WORK SHALL BE SUBJECT TO OWNERS REPRESENTATIVE APPROVAL OF WORK IN PLACE AS WELL AS SHOP DRAWINGS AND SAMPLE OF MATERIALS AND EQUIPMENT WHICH SHALL BE CHECKED BY CONTRACTOR BEFORE SUBMITTAL.
5. PROTECT ALL EXISTING UTILITIES ALONG THE SOUTH FOR FUTURE USE OF THE NEW BUILDING.
6. REMOVE ALL EXISTING PAVEMENT AND RESURFACE THE PARKING AREA WITH 6" CONCRETE PAVEMENT PLEASE FOLLOW THE DETAIL SHOWN ON THIS SHEET. THE TANK AREA SHALL BE PAVED WITH 8" CONCRETE PAVED WITH REINFORCEMENT.
7. INSTALL NEW DRIVEWAY ALONG THE WEST ACCESS ROAD. NEW DRIVE APPROACHES SHALL BE CONSTRUCTED PER KCMO STANDARD COMMERCIAL DRIVEWAY DRAWING. CONSTRUCT ADA COMPLIANCE ACCESSIBLE RAMPS ON EACH SIDE OF NEW DRIVEWAY.



Date	03/09/24
Drawn by	KRB
Checked by	GWM
Submitted for Owner Approval	
By	
Date	



Design Group LLC
9000 E. Bonner Road
Suite 100
Kansas City, Missouri 64114
(816) 797-2005

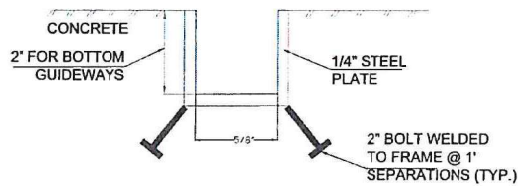
SHORT STOP GAS STATION PROJECT

400 NE 72ND STREET
GLADSTONE, MISSOURI

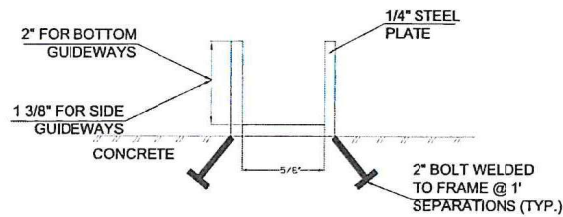
GRADING PLAN

Project Number: 2023-109
Drawn by: KRB
Checked by: GWM

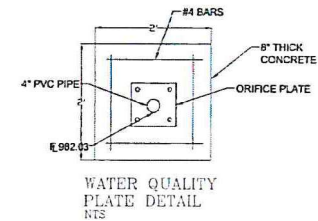
SHEET 5



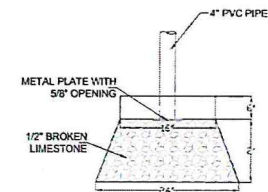
BOTTOM FRAME RESTRAINER FOR ORIFICE PLATE
NTS
DETAIL "C"



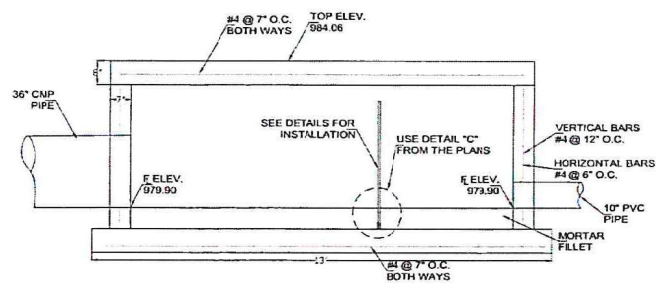
SIDE FRAME RESTRAINER FOR ORIFICE PLATE
NTS
DETAIL "D"



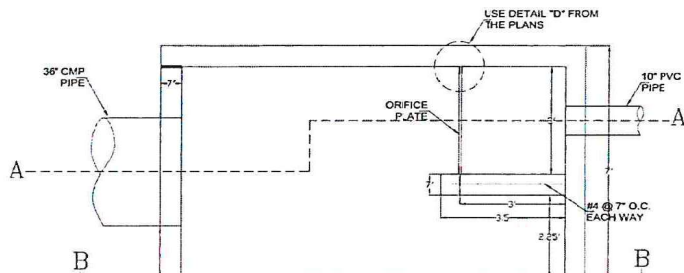
WATER QUALITY
PLATE DETAIL
NTS



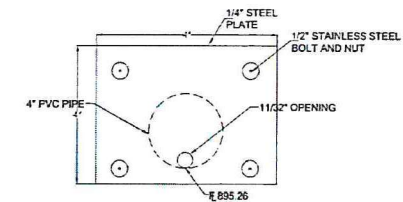
OUTFALL FOR WATER
QUALITY BASIN
NTS



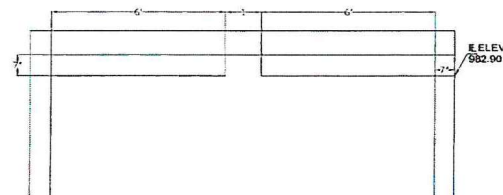
SECTION A-A



STRUCTURE PLAN VIEW

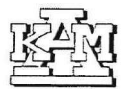


WATER QUALITY DRAIN OUTLET DETAIL
NTS



SECTION B-B

DATE	DESCRIPTION
01/10/2023	SUBMITTED FOR CANNAL APPROVAL



Design Group LLC
3000 E. Delaware Road
Suite 100
Kansas City, Missouri 64134
(816) 797-1245

SHORT STOP GAS STATION
PROJECT

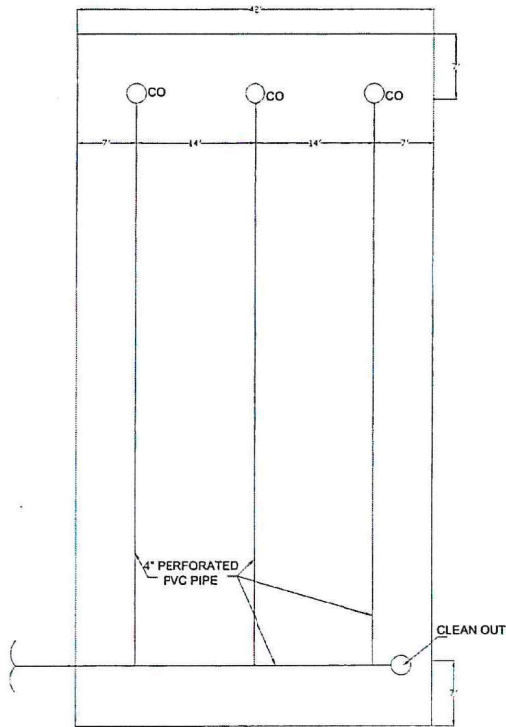
400 NE 72ND STREET
GLADSTONE, MISSOURI

DETAILS SHEET

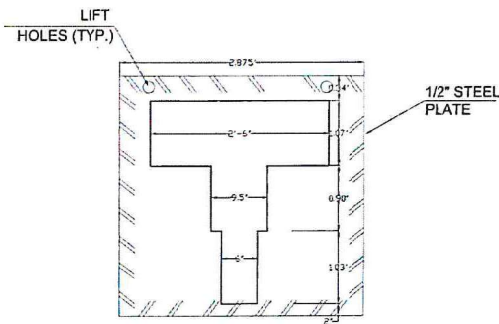
Project Number: 2023-109
Drawn by: KRB
Checked by: GWM

SHEET 6

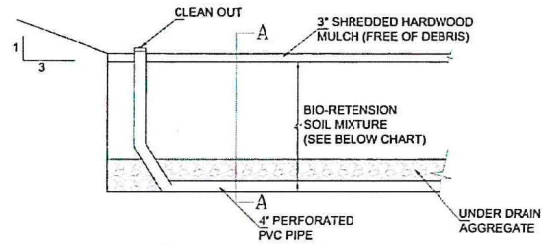




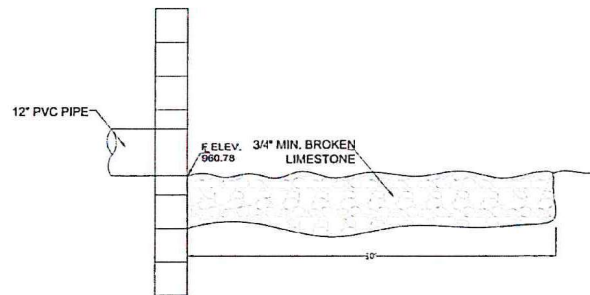
4" PVC PIPE PLAN FOR BIORETENSION BED
NTS



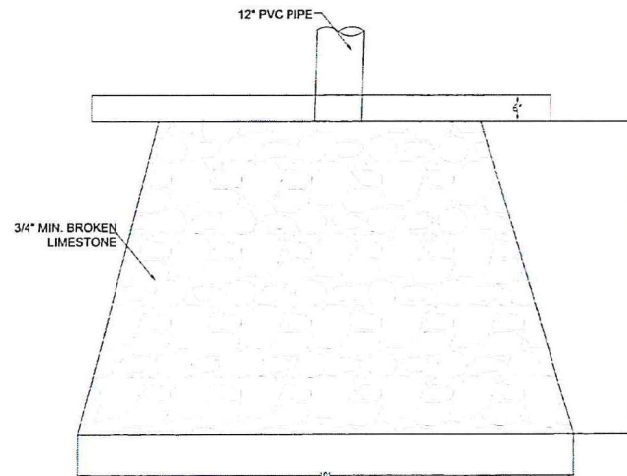
ORIFICE PLATE FOR DETENTION OUTFLOW
NTS



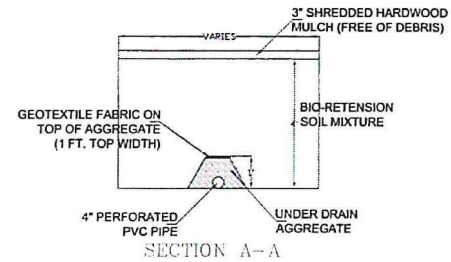
BIO-RETENSION BASIN TYPICAL X-SECTION
NTS



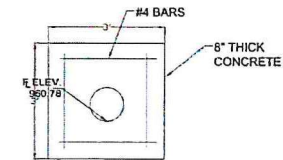
SECTION VIEW
NTS



OUTFALL FOR WATER
QUALITY BASIN
NTS



SECTION A-A



DETENTION DISCHARGE
PLATE DETAIL
NTS

BIO-RETENSION SOIL MIXTURE

COMPONENTS	RATIO BY VOLUME
FILTER SAND	70% (+/- 3%)
COCONUT COIR FIBER	20% (+/- 2%)
HIGH CARBON WOOD ASH	10% (+/- 1%)



DATE	DESCRIPTION	BY
07/05/23	QUANTITIES ON OWNER'S APPROVAL	



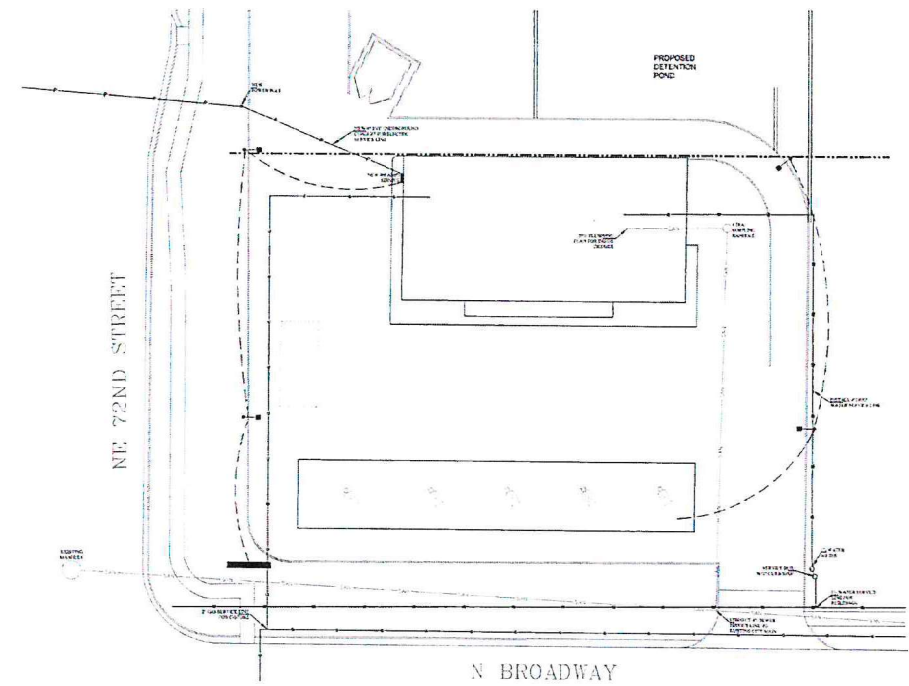
SHORT STOP GAS STATION PROJECT

400 NE 72ND STREET
GLADSTONE, MISSOURI

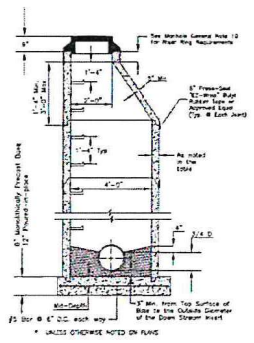
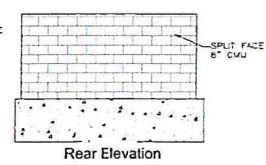
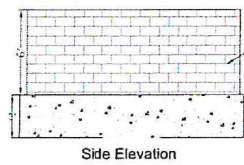
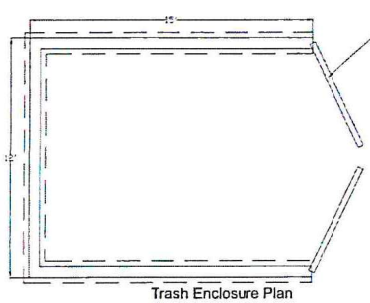
DETAILS SHEET II

Project Number	2023-109
Drawn by	KRB
Checked by	GWM

SHEET 7

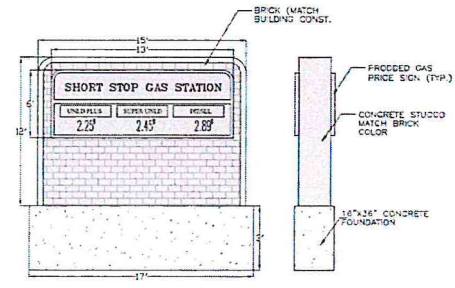


- LEGEND**
- BUILDING OUTLINE
 - PROPERTY LINE
 - WATER SERVICE LINE
 - GAS SERVICE LINE
 - SANITARY SERVICE LINE
 - ELECTRICAL SERVICE LINE
 - UNDERGROUND CONDUIT FOR LP'S



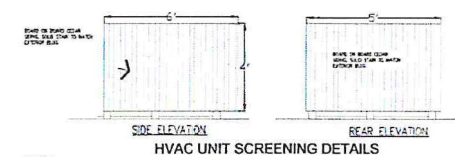
- MANHOLE GENERAL NOTES**
- All manhole risers of two (2) rows of 3/4 to 1 inch precast concrete joint riser.
 - All manhole risers to be placed in cement or in brick to be subsequently paved shall have manhole riser joint bearing surfaces and shall comply with Class B as established in ASTM C-478.
 - The inside diameter of the manhole shall be 4'-0" for pipe diameter from 18" thru 24" and shall be 2'-0" for pipe diameter from 27" thru 36". In addition, the riser diameter (ID) of manholes up to 20 feet deep shall be 4'-0", ID shall be 2'-0" for depths up to 25 feet and ID shall be 4'-0" for depths exceeding 25 feet unless otherwise noted on the plans.
 - All manhole bases (one-cast or poured-in-place) shall have No. 5 reinforcing bars placed on 6" centers both ways.
 - All standard manhole risers and covers to be Dwyer (D-100-100), Harsco (H-100-100) (frame) and H-100-100 (cover), or approved equal. All manhole risers to covers shall be shown to be equal. An extra segment for furnishing the riser and cover is shown in plans will not be made, but shall be considered as accessory to the riser, "Standard Riser".
 - Standard manhole steps to be steel core, plastic coated steps DWA, Inc. No. PS1-PR, PS2-PR, or approved equal.
 - Manhole girth adjustment diameter is 8". Minimum ultimate thickness for precast concrete girth adjustment ring is 4".
 - Reinforcement in all precast sections shall equal or exceed ASTM C-478 specifications.
 - Butyl material to be used at all precast sections, joints. Gaskets may be used for joints below the cone section, but the cone section itself shall not have gasket joints.
 - Riser Rings:
 - A. Manholes in Plaster: The thickness of the recycled rubber riser rings shall not be less than one (1) inch nor greater than four (4) inches. If the required thickness of riser rings exceeds 4 inches, a 4-inch or 6-inch precast concrete riser ring shall be installed between the rubber riser ring and the cone. Riser rings may be used up to 4 inches or 6 inches. The manhole riser rings shall be spaced to match the slope of the existing or proposed ground at the manhole. The joints between the cone, rubber riser rings, and casting shall be sealed with the manufacturer-suggested sealant.
 - B. Recycled Riser in Plaster: All manholes shall be provided with riser rings underneath the existing riser shown on drawings. All manhole riser rings shall be installed on top of the existing riser. The riser rings shall be spaced to match the slope of the existing or proposed ground at the manhole. The joints between the cone, rubber riser rings, and casting shall be sealed with the manufacturer-suggested sealant.
 - C. Brick and mortar adjustments will not be allowed.

4" DIA. STANDARD PRECAST MANHOLE (ECCENTRIC CONE)




NOTE:
THE CONTRACTOR SHALL APPLY SEPARATELY TO THE PERMIT DIVISION FOR SIGN PERMIT.

NEW MONUMENT SIGN



NOTE:
THE HEIGHT OF THE SCREENING APPARATUS SHALL BE AT LEAST 12" HIGHER THAN ANY EQUIPMENT ON THE ROOF.



Design Group LLC
8060 E. Bonanza Road
Suite 100
Kansas City, Missouri 64134
(816) 797-2000

SHORT STOP GAS STATION PROJECT

**400 NE 72ND STREET
GLADSTONE, MISSOURI**

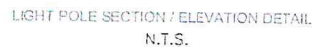
UTILITY PLAN

Project number: 2023-109
Drawn by: KRB
Checked by: GWM

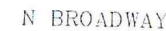
SHEET 8

- ① ROUTE 120V HOME RUN BELAY GRADE TO QUATZITE BOX SHOWN ON PLANS. ASSUMED VOLTAGE USED TO DETERMINE VOLTAGE DROP AND WIRE SIZES IS 120V, 1-PHASE.
- ② PARKING LOT LIGHT WITH STEEL POLE/LIGHT AND CONCRETE FOUNDATION REFERENCE LIGHT FIXTURE SPECIFICATION THIS SHEET.
- ③ ASSUMED LOCATIONS OF CONDUIT ENTRY INTO BUILDING FOR SITE LIGHTING. REFER TO BUILDING ELECTRICAL ENGINEERING PLANS AND BUILDING ELECTRICAL ENGINEER FOR UPDATED LOCATIONS OF CONDUIT ROUTING INTO THE BUILDING.
- ④ LIGHTING CONTROLS AND CONNECTIONS, PROVISIONS FOR ELECTRICAL POWER, AND CONDUIT ROUTING INTO BUILDING ARE NOT INCLUDED WITHIN THE SCOPE OF THIS WORK. REFER TO BUILDING ELECTRICAL ENGINEER FOR MORE INFORMATION. NOTIFY ENGINEER IF ACTUAL LOCATION OF ELECTRICAL CONNECTION/CONTROL IS IN A SIGNIFICANTLY DIFFERENT AREA OF BUILDING.
- ⑤ PROVIDE QUATZITE BOX IN APPROXIMATE LOCATION FOR FULL POINT TO CONNECT WITH HOME RUNS FROM SITE LIGHTING

MANUFACTURER	INNOVATIVE LIGHTING
LIGHT TYPE	LED LIGHT ENGINE
POWER	48 WATTS
TYPE	II
MODEL	EF2-U--28-3-N
INSTALLATION	POLE MOUNTED



1. THE CONTRACTOR SHALL INSTALL A LIGHT POLES AS SHOWN ON THIS SHEET. THE CONTRACTOR SHALL INSTALL NEW LIGHT FIXTURES ON ALL THESE POLES, IF WIRING TO ANY OF THESE POLES IS NOT FUNCTIONAL. INSTALL WIRING IN 3" PVC CONDUIT FOR POLE LOCATIONS.
2. TO COMPLY WITH FEDERAL, STATE, AND LOCAL STATUTES, NOTIFY MISSOURI ONE-CALL SYSTEM, INC. AT LEAST 48 HOURS PRIOR TO ANY DIGGING, TRENCHING, EXCAVATION, ETC. INFORMATION SHOWN ON THIS SHEET IS NOT GUARANTEED TO BE ACCURATE. THERE MAY BE UNDERGROUND AND OTHER UTILITIES NOT GUARANTEED TO BE SHOWN ON THIS SHEET. INCLUSIVE, THE CONTRACTOR IS RESPONSIBLE FOR MAKING HIS OWN DETERMINATION AS TO THE LOCATION OF SAKE AS MAY BE NECESSARY TO AVOID DAMAGE. THERE IS TO BE FIELD VERIFY LOCATIONS OF ALL UTILITIES OF ALL TYPES. THE CONTRACTOR SHALL BE BROUGHT TO ATTENTION OF THE ARCHITECT AND ENGINEER FOR DIRECTOR. PROVIDE EQUIPMENT GROUNDING CONDUCTOR THROUGHOUT EACH BRANCH CIRCUIT. THE CONTRACTOR MAY BE REQUIRED TO RE-LOCATE THE LIGHT POLES.
3. THE CONTRACTOR SHALL CONFIRM WITH HIS WIRING THAT NO CIRCUIT EXCEEDS 3328 VA. IF WIRING DEVIATES SIGNIFICANTLY FROM THE LAYOUT ON THE PLANS, ACCOUNT FOR MORE THAN 10% CIRCUIT BREAKER. PROVIDE GROUNDING CONDUCTOR SIZE BY A FACTOR OF ONE SIZE.
4. ALL WIRING SHALL BE ALLOWED TO BE IN 3" PVC CONDUIT. CONDUIT SHALL BE BELOW A TRAFFIC DRIVE AREA. TRANSITION TO EAT AT ELBOW PRIOR TO GOING ABOVE GRADE. USE CONDUIT BELOW ALL TRAFFIC AREAS AND TRANSITION MATERIALS ACCORDINGLY.
5. COORDINATE ALL THE PRELIMINARY UTILITY LOCATIONS, CUTTAGES, PAD REQUIREMENTS, ETC. WITH KCP&L FOR EXIST INSTALLATION REQUIREMENTS.



- NEW LIGHT POLE
- CANOPY LIGHT
- ☑ WALL MOUNTED LIGHT
- UNDERGROUND ELECTRIC



400 NE 72ND STREET
GLADSTONE, MISSOURI

Project number	2023-109
Drawn by	KRB
Checked by	GYM

SHEET 9

PLANT LIST

NO	SYMBOL	COMMON NAME	BOTANICAL NAME	SIZE
SHADE TREES				
5	SYM	SHANTUNG MAPLE	ACER TRUNCATUM	2.5" CAL
9	BDC	BALD CYPRESS	TAXODIUM DISTICHUM	2.5" CAL
EVERGREEN SHRUBS				
25	BOX	GREEN VELVET BOXWOOD	DUX'S 'GREEN VELVET'	3 GAL. CONTAINER
26	WY	WARD'S YEW	TAXUS MEDIA 'WARDII'	3 GAL. CONTAINER

LANDSCAPING NOTES:

1. ALL PLANT MATERIAL SHALL BE FIRST CLASS REPRESENTATIVES OF SPECIFIED SPECIES, VARIETY OR CULTIVAR, IN HEALTHY CONDITION WITH NORMAL WELL DEVELOPED BRANCHES AND ROOT PATTERNS. PLANT MATERIAL MUST BE FREE OF OBJECTIONABLE FEATURES. PLANTS SHALL COMPLY IN ALL APPLICABLE RESPECTS WITH PROPER MOST RECENT STANDARDS AS SET FORTH IN THE AMERICAN ASSOCIATION OF NURSERYMEN'S 'AMERICAN STANDARD OF NURSERY STOCK', ANSI Z60.1, AND THE GLADSTONE NURSERY AND LANDSCAPE ASSOCIATION.
2. ORNAMENTALS AND SHRUBS SHALL BE CONTAINER GROWN AND WILL BE FREE OF DISEASE AND PESTS. ABSOLUTELY NO BARE ROOT MATERIALS. FERTILIZER OF 10-20-10: ONE PELLET OR 1-2 OZ. SHALL BE ADDED TO SOIL AT TIME OF PLANTING.
3. ALL SHRUB AND PLANT BEDS TO BE MULCHED WITH 3" DEPTH DARK HARDWOOD MULCH. AS AN ALTERNATE IN SHRUB BEDS, 2" DEEP SMOOTH RIVER ROCK OVER PERMEABLE WEED BARRIER FABRIC USED FOR WEED PREVENTION MAY BE INSTALLED INSTEAD OF HARDWOOD MULCH. HARDWOOD MULCH TO BE INSTALLED IN ALL ORNAMENTAL GRASS BEDS.
4. PLANTING BEDS ARE TO BE FREE OF WEEDS AND GRASS. TREAT BEDS WITH A PRE-EMERGENT HERBICIDE PRIOR TO PLANTING AND MULCH PLACEMENT. APPLY IN ACCORDANCE WITH STANDARD TRADE PRACTICE.
5. ALL TREES SHALL BE FERTILIZED WITH FERTILOME BRAND LIQUID ROOT STIMULATOR, 1.5 TABLESPOONS PER GAL. OF WATER, AS A SUBSTITUTE, 1948-10 GRANULAR FERTILIZER, 75 LB. FOR 2" CAL. & 1.5 LBS. FOR 2" CAL. SHALL BE ADDED. INCORPORATE FERTILIZER INTO THE AMENDED PLANTING SOIL BEFORE PLANTING TREE. HOLE AREA FOR TREE TO BE TWICE (2x) THE DIAMETER OF THE ROOT BALL AND ROOT BALL SHALL BE MOUND. ALL TREES TO BE STAKED AND GUYPED WITH A MINIMUM OF 3 POSTS AND PROTECTED W/ COVERING AT TREE W/ GUY WIRE.
6. ALL PLANT MATERIALS SHALL BE PROTECTED FROM THE DRYING ACTION OF THE SUN AND WIND AFTER BEING DUG, WHILE BEING TRANSPORTED, AND WHILE AWAITING PLANTING. BALLS OF PLANTS WHICH CANNOT BE PLANTED IMMEDIATELY SHALL BE PROTECTED FROM DRYING ACTION BY COVERING THEM WITH MOIST MULCH. PERIODICALLY, APPLY WATER TO MULCH-COVERED BALLS TO KEEP MOIST. IF PLANTING SHOULD OCCUR DURING GROWING SEASON, APPLY ANTI-DESICCANT TO LEAVES BEFORE TRANSPORT TO REDUCE THE LIKELIHOOD OF WINDBURN. REAPPLY ANTI-DESICCANT AFTER PLANTING TO REDUCE TRANSPIRATION.
7. AFTER PLANTING IS COMPLETED, REPAIR INJURIES TO ALL PLANTS AS REQUIRED. LIMIT AMOUNT OF PRUNING TO A MINIMUM TO REMOVE DEAD OR INJURED TWIGS AND BRANCHES. PRUNE IN SUCH A MANNER AS NOT TO CHANGE THE NATURAL HABIT OR SHAPE OF THE PLANT. MAKE CUTS FLUSH, LEAVING NO STUBS. CUTS OF ONE INCH OR MORE TO BE PAINTED WITH TREE PAINT. CENTRAL LEADERS SHALL NOT BE REMOVED.
8. THE INSTALLATION OF ALL PLANT MATERIAL SHALL BE IN COMPLIANCE WITH THE REQUIREMENTS OF THE CITY OF GLADSTONE, MO.
9. ALL LANDSCAPE AREAS TO BE FREE OF ALL BUILDING DEBRIS AND TRASH. BACK FILLED WITH CLEAN FILL SOIL AND TOP DRESSED WITH 6" OF TOPSOIL. TOPSOIL SHALL HAVE A pH RANGE OF 5.5 TO 7 AND A 4% ORGANIC MATERIAL MINIMUM. ASTM D5268.
10. ALL PLANT BED AREAS TO RECEIVE DAILY COW MANURE SOIL CONDITIONER AT A RATE OF 4.5 CU. YDS. PER 1000 SF. AND ORGANIC COMPOST AT A RATE OF 4.5 CU. YDS. PER 1000 SF. TO DETERMINE THE AMOUNT OF PHOSPHOROUS AND POTASSIUM THE CONTRACTOR SHALL PERFORM A SOIL TEST AND ADD THOSE FERTILIZERS ACCORDING TO THE TEST RESULTS. AFTER APPLYING SOIL CONDITIONER AND FERTILIZER, THOROUGHLY TILL AREA TO A DEPTH OF 12". CONTRACTOR TO INSTALL A PERMEABLE LANDSCAPE WEED CONTROL FABRIC, 3 OZ. PER SQ. YD. MIN. IN ALL PLANT BEDS EXCEPT IN AREAS OF GROUND COVER, PERENNIAL OR ANNUAL PLANTINGS. PLANT BEDS TO BE "MOUNDING". ALL PLANT MATERIAL, PLANT BEDS, MULCH AND EDGING TO BE INSTALLED PER LANDSCAPE PLANS AND DETAILS. NYKE PRO MYCORRHIZAE GRANULES TO BE ADDED TO ALL PLANTINGS PER MANUFACTURERS RECOMMENDATIONS.
11. REESTABLISH FINISH GRADES TO WITHIN ALLOWABLE TOLERANCES ALLOWING 1-1/2" FOR 500 AND 2" FOR MULCH IN PLANT BEDS. HAND RAKE ALL AREAS TO SMOOTH EVEN SURFACES FREE OF DEBRIS, CLODS, ROCKS, AND VEGETATIVE MATTER GREATER THAN 1".
12. THE EXACT LOCATION OF ALL UTILITIES, STRUCTURES AND UNDERGROUND UTILITIES SHALL BE DETERMINED AND VERIFIED ON SITE BY THE LANDSCAPE CONTRACTOR PRIOR TO INSTALLATION OF THE MATERIALS. DAMAGE TO EXISTING UTILITIES AND OR STRUCTURES SHALL BE REPLACED TO THEIR ORIGINAL CONDITION BY THE LANDSCAPE CONTRACTOR AT NO COST TO THE OWNER.
13. LANDSCAPE CONTRACTOR IS RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS AND APPROVALS AND REQ'D INSPECTIONS BY LEGAL AUTHORITIES. THE LANDSCAPE CONTRACTOR SHALL UNCONDITIONALLY GUARANTEE ALL PLANT MATERIAL FOR ONE CALENDAR YEAR.
14. ANY SUBSTITUTIONS OF DEVIATIONS SHALL BE REQUESTED IN WRITING BY THE CONTRACTOR FOR APPROVAL BY THE OWNER OR LANDSCAPE ARCHITECT.
15. THE LANDSCAPE CONTRACTOR IS RESPONSIBLE FOR THE DESIGN, OBTAINING AND INSTALLATION OF ALL IRRIGATION COMPONENTS, SLEEVING, PIPE, METERS, PERMITS, CONNECTION AND CONTROL SYSTEMS. DESIGN DRAWINGS OF THE PROPOSED IRRIGATION SYSTEM SHALL BE SUBMITTED TO THE CITY FOR REVIEW AND APPROVAL PRIOR TO INSTALLATION.
16. EROSION CONTROL MAT TO BE NORTH AMERICAN SC 150-BN BIODEGRADABLE MAT OR EQUIVALENT.
17. ALL LAWN AREAS TO BE SOODED OR SEEDED WITH TURF TYPE TALL FESCUE BLEND IN LOCATIONS INDICATED ON PLANS. SEEDED LAWN TO BE HYDRO-SEEDED OR DRILLED. SOO AND SEED SHALL COMPLY WITH THE U.S. DEPT. OF AGRICULTURE RULES AND REGULATIONS UNDER THE FEDERAL SEED ACT AND EQUAL IN QUALITY TO STANDARDS FOR CERTIFIED SEED. LAWN SHALL BE TURF TYPE TALL FESCUE 3 WAY BLEND.

LAWN SEED MIX

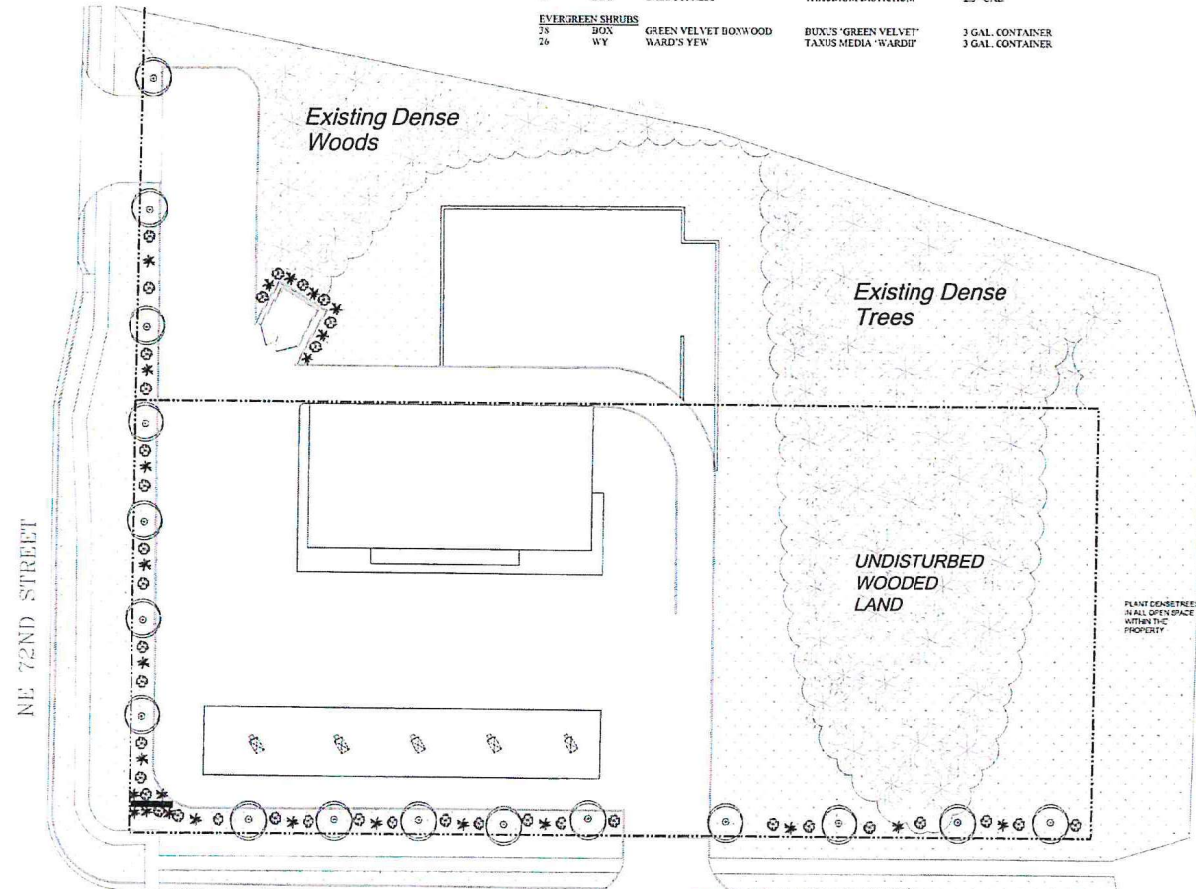
TRI-STAR® QUICK TURF MIXTURE OR SIMILAR BLEND:

SEEDING RATE: 8-10 LBS PER 1,000 SF

- 25% TITAN LTD FESCUE "TRI-STAR SEED COMPANY
- 25% FALCON IV TALL FESCUE SPURRING HILL, KS 66083
- 25% 2ND MILLENNIUM TALL FESCUE 800-574-3308
- 25% TURF PERENNIAL RYEGRASS

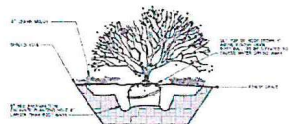
LEGEND

- NEW TREE
- ✱ NEW SHRUB PLANTINGS (LOW TREES)
- BUILDING OUTLINE
- PROPERTY LINE
- DENSE TREE LINE



N BROADWAY

LANDSCAPING PLAN



TYPICAL SHRUB PLANTING

TYPICAL TREE PLANTING DETAIL
NOTE: TREES ARE NOT TO BE PLANTED IN THE SAME LOCATION AS THE BUILDING FOOTPRINT.
NEW LOCATIONS ARE INDICATED BY TREE AND SHRUB SYMBOLS.

GENERAL NOTES

1. THE LANDSCAPING AREA SHALL BE INSTALLED WITH BUILT IN IRRIGATION SYSTEM.
2. ANY DAMAGES TO CURB AND SIDEWALK IN PUBLIC RIGHT OF WAY SHALL BE REPAIRED PER CITY STANDARD DETAIL AND SPECIFICATIONS.
3. THE TRASH ENCLOSURE STRUCTURE SHALL BE CONSTRUCTED OF THE SAME MATERIAL AS FOR THE MAIN BUILDING.
4. THE GAS METER AREA SHALL BE SCREENED WITH SHRUBS. THE ELECTRICAL METER AND SWITCHGEAR SHALL BE SCREENED WITH ENCLOSURE MATCHING THE BUILDING EXTERIOR.
5. 12 TREES SHALL BE PLANTED ALONG THE PUBLIC RIGHT OF WAY.

SHORT STOP GAS STATION
PROJECT

400 NE 72ND STREET
GLADSTONE, MISSOURI

LANDSCAPING PLAN

Project number: 2023-109
Drawn by: KRB
Checked by: GYM

SHEET 10



Property Owners Within 185' & Other Interested Parties

FROM: Community Development Department

DATE: May 2nd, 2024

SUBJECT: Gas Station & Convenience Store – Site Plan Revision

PUBLIC HEARING

All persons are hereby notified that the Gladstone Planning Commission will conduct a public hearing on Monday, May 20, 2024 at 7:00 PM in the Council Chamber of Gladstone City Hall on a request for a Site Plan Revision at 7200 N Broadway Ave. Legally described as 000000 NW 72ND ST BEG SW COR LT 12 WILLOW CREEK E146, S340, SW21.21, W138, N T O POB.

Applicant: Gerald W. Menefee P.E.

Owner: Mohammad Hafiz

Subsequently, at its regular meeting of June 10th, 2024, at 7:30 PM, the City Council will conduct a public hearing on the same request.

Project Summary: This project was proposed in 2023 and denied by the Gladstone City Council. The property owner has made adjustments to the site plan and is proposing to build a new gas station and convenience store on the vacant land located at 7200 N Broadway Avenue. The primary exterior building materials being used are brick and stucco. There will be two access points; one point on N Broadway Avenue and one point on NW 72nd Street. This property is zoned CP-2, Planned District, General Business and a gas station and convenience store is currently a permitted use for this commercial zoning.

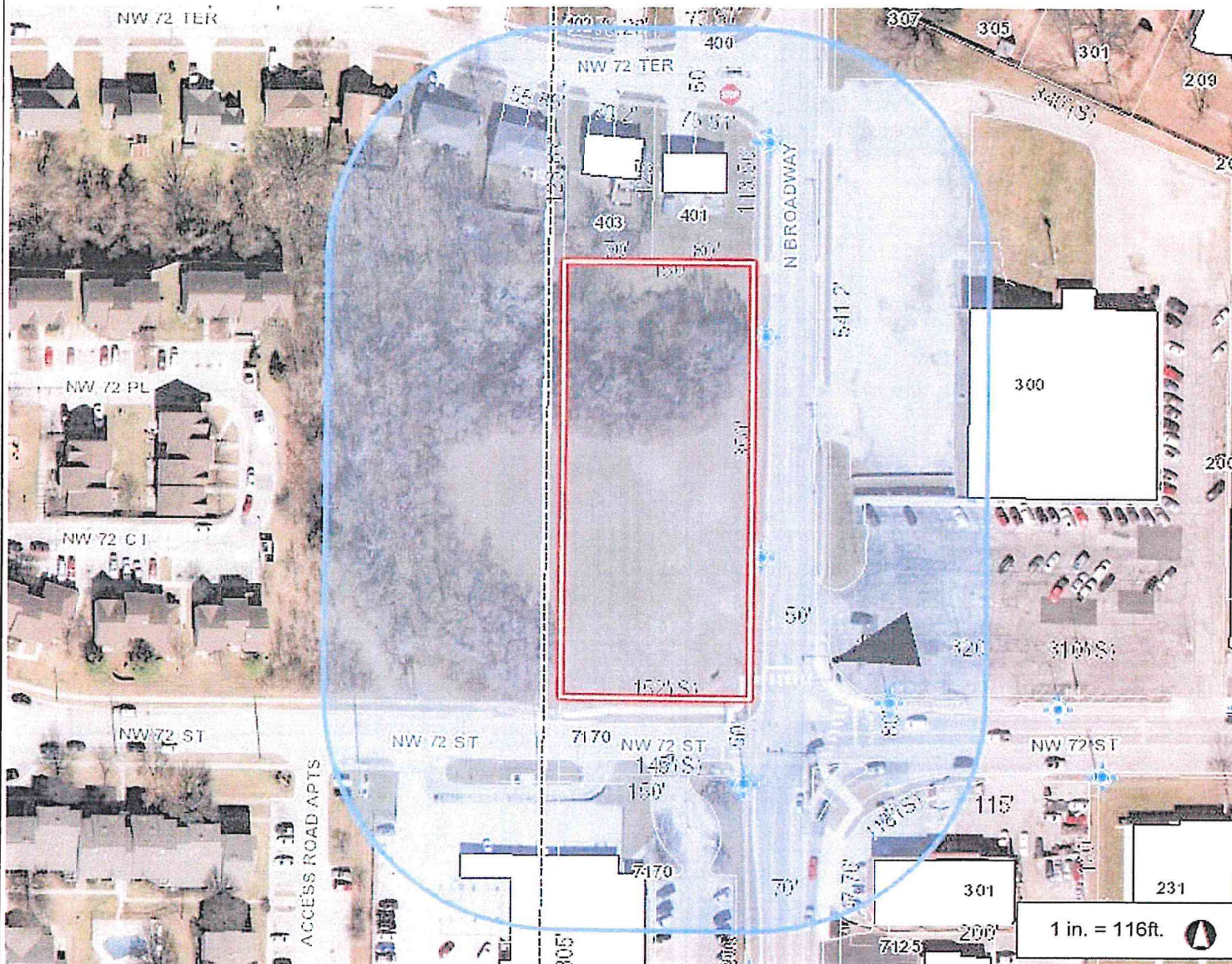
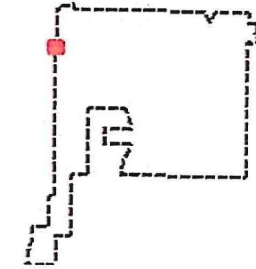
Primary Adjustments to the Site Plan:

- The access point on NW 72nd Street has been shifted west to lineup with the Post Office access point.
- The water detention basin has been moved from the northern side of the property to the western side of the property away from the residential homes located to the north. This basin will be located on the KCMO parcel.
- The wooded area on the northern side of the property will primarily remain untouched.

If you have any questions or concerns, please contact Austin Greer, Community Development Director & Assistant City Manager at austing@gladstone.mo.us and/or 816-423-4102.



Gladstone, MO



Legend

- Stop Sign
- KCPL Lights
- Gladstone Lights
- School Point
- Bike Parking
- Bus Stop
- Point of Interest
- Church
- Apartment Point
- Street Centerline
- Edge Of Pavement
- Driveway
- City Limits
- Parcel
- House Number
- Building Footprint
- School Polygon
- City Park
- Villages
- Apartment Polygon

Notes

This map is a user generated static output from an Internet mapping site and is for reference only. Data layers that appear on this map may or may not be accurate, current, or otherwise reliable.
THIS MAP IS NOT TO BE USED FOR NAVIGATION

(minus street right-of-ways), the final City Council action has to have a minimum of four (4) positive votes for the request to be approved. The application cannot be approved if three (3) vote "yes" and two (2) "no". For further information regarding this handout, please call or come by the Community Development Department at 7010 N. Holmes, 423-4110.

☐ City Code Variance Request: Board of Zoning Adjustment

REQUIREMENTS

Completed application
Owner's authorization signed (if applicable)
Legal description- County records
Information on the proposed change including pictures of the property, property surveys, written comments from impacted neighbors, etc.

DEPOSIT FEE

The \$200 fee listed on the form and paid at the time of application is a deposit toward the costs the City of Gladstone incurs during the processing of your application. This fee goes toward the following costs:

Office fee \$75.00
Certified mail notices to surrounding property owners within 185' - amount varies.*
Planning Commission Legal Notice- amount varies*

** Indicates fees for items required by State Law. The fee amount for certified mail will vary depending upon the number of property owners within 185 feet of your property. The Legal Notice fee will also vary generally depending upon the length of the legal description of your property.*

After the total costs are compiled for your application, you will be billed for any costs remaining over the initial \$200 application deposit fee. If the costs accrued are under \$200, you will be reimbursed for the difference.

As the money deposited for your application goes toward real costs paid by the City, there is no refund if your application is denied by the Board of Zoning Adjustment. If you withdraw your application before some of the costs are accrued by the City, you may be entitled to a refund.

Preliminary & Final Plat/Replat Submittals

REQUIREMENTS

Completed application
Owner's authorization signed (if applicable)
Legal description- County records
Digital copy of plans
(1) 11x17 paper copy
(3) 24x36 paper copies folded
(1) 24x36 Mylar Copy - Completion of the Plat

FEE

The \$75 fee listed on the form and paid at the time of application goes toward the costs the City of Gladstone incurs during the processing of your application. As the fee for your application goes toward real costs paid by the City, there is no refund.

**At completion of the plat, please submit to Community Development (1) 24x36 Mylar copy.

OWNER'S AUTHORIZATION

I, Mohammad Hachiz, do hereby authorize _____
(Owner's name) (Applicant's name)
to apply for the following action on my property at _____

- a. Rezone from to
- b. Site Plan Revision
- c. Special Use Permit
- d. Variance
- e. Plat/Replat

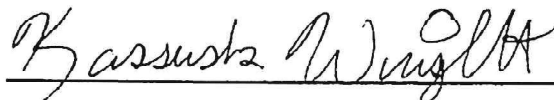
Date: 5/20/24 Owner's Signature: 

NOTARIZATION

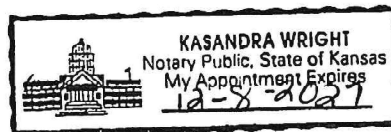
State of Kansas
 County of Wyandotte

Subscribed and sworn before me this 20th day of May, 2024.

Notary's Signature:



My Commission expires: 12-8-2027



Additional Required Documents

(check if needed)	Comments
Site Plan <u> </u>	
Traffic Study <u> </u>	
Landscaping Plans <u> </u>	
Stormwater <u> </u>	
(Pre - Post - BMP) <u> </u>	
Photometric Study <u> </u>	
Master Sign Plan <u> </u>	
Colored Elevation / Rendering <u> </u>	
Materials Board <u> </u>	

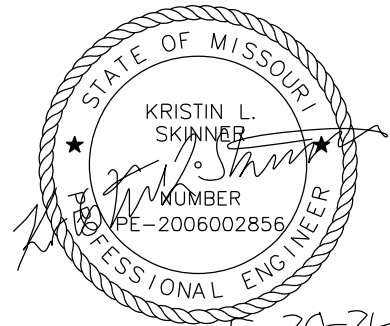
Gladstone Convenience Store

TRAFFIC IMPACT STUDY

May 20, 2024

Prepared For:
Mr. Muhammed Hafiz

Prepared By:
Priority Engineers, Inc.
PO Box 563
Garden City, MO 64747





May 20, 2024

Mr. Muhammed Hafiz

RE: Gladstone Convenience Store Traffic Impact Study – Gladstone, MO

Dear Mr. Hafiz:

In response to your request, Priority Engineers, Inc. has completed a traffic impact analysis for the above referenced project. The purpose of the analysis is to determine the potential traffic impacts associated with this development on the intersections and streets surrounding this site, primarily during the AM and PM peak hours. The following report documents our analysis and recommendations.

We appreciate the opportunity to work with you on this project. Please contact us with any questions or if you require additional information.

Sincerely,

PRIORITY ENGINEERS, INC.

A handwritten signature in blue ink that reads 'Kristin L. Skinner'.

Kristin L. Skinner, P.E., PTOE
President

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1) INTRODUCTION

The purpose of this study is to examine the potential traffic impacts associated with a proposed Gladstone Convenience Store development located within the municipal limits of Gladstone, in Clay County, Missouri. This proposed development will construct a convenience store located to the north and the west of the intersection of NW 72nd Street and N Broadway Street.

The study area is shown in Figure 1. The site layout is shown in Figure 2.

2) EXISTING CONDITIONS

The proposed Gladstone Convenience Store development is located on a parcel of undeveloped land located northwest of the intersection of N Broadway Street and NW 72nd Street. To the north and west of the proposed development there are existing residential developments. To the south of the proposed development is a USPS facility and to the east of the proposed development is the Gladstone Bowl bowling alley.

N Broadway Street, south of the intersection with NW 72nd Street has a cross-section of two lanes in each direction without separation and it has curb and gutter and an enclosed drainage system. This segment N Broadway Street has a posted speed limit of 35 MPH. North of the intersection with NW 72nd Street has a cross section that consists of one lane in each direction, and curb and gutter with an enclosed drainage system. The posted speed limit on this segment of N Broadway Street is 30 MPH. The Mid America Regional Council (MARC) has given N Broadway Street a functional classification of Minor Arterial south of NW 72nd Street and a functional classification of Minor Collector north of NW 72nd Street. The Gladstone Comprehensive Plan identifies N Broadway Street as an Arterial south of NW 72nd Street and as a Primary Collector to the north of NW 72nd Street.

NW 72nd Street, to the east, has a cross section with two through lanes in each direction. NW 72nd Street has curb and gutter and an enclosed drainage system. MARC has given NW 72nd Street a functional classification of Minor Arterial to the west. The Gladstone Comprehensive Plan identifies NW 72nd Street as an Arterial. NW 72nd Street has a posted speed limit of 35 MPH.

Peak Hour turning movement counts were collected for the following intersections:

- NE 72nd Street N Broadway Street
- NE 72nd Street and West Drive of the USPS facility
- N Broadway Street and Gladstone Bowl entrance

These counts were performed on January 17th of this year. The Peak Hour turning movement counts were performed from 7:00 to 9:00 AM and from 4:00 to 6:00 PM. The AM Peak Hour was found to be from 8:00 to 9:00 and the PM Peak Hour was found to be from 4:30 to 5:30 for the overall roadway network. The complete traffic counts are shown in Appendix II. The peak hour traffic volumes and existing lane configurations are shown in Figures 3-6.

3) PROPOSED DEVELOPMENT

The proposed development will build an approximately 5,000 SF convenience store with 10 vehicle fueling positions (VFP). The provided site plan shows a drive through window on the west side of convenience store. There will be two full access entrances into the development. The first proposed entrance is a full access entrance onto NE 72nd Street located opposite of the

west entrance into the USPS facility. Street. The second full access entrance will provide access onto N Broadway Street. This access will be located to the north of the existing Gladstone Bowl drive.

4) TRIP GENERATION

The vehicle trips generated by the proposed development were estimated using the Institute of Transportation Engineers' (ITE) Trip Generation, 11th Edition. Land Use 945, Convenience Store / Gas Station. Since this location has a drive-through window, both Land Use 935 (fast food restaurant with drive-through window and no indoor seating) and Land Use 934 (fast food restaurant with drive through window) were considered for a portion of the 5,000 SF store. It was determined that the trips generated by Land Use 945 is higher than Land Use 935 and it is slightly higher than Land Use 934, so the complete footprint of the store was considered using Land Use 945 for a more conservative trip generation estimate.

Land Use 945 has two subcategories in the ITE data set, and GFA of the Store (with independent variable of VFP and VFP (with independent variable of GFA). Selecting data from the VFP subcategory resulted in a more conservative trip generation and was selected for this study.

The estimated AM and PM peak hour traffic volumes associated with the full buildout of this development are shown in Table 1.

Table 1: ITE Trip Generation								
Land Use	Intensity	Daily	AM Peak Hour			PM Peak Hour		
			Total	In	Out	Total	In	Out
Convenience Store/Gas Station (VFP 9-15)	5,000 SF	3353	283	141	142	273	136	137

Pass-by trips are made as intermediate stops on the way from an origin to a primary trip destination without a route diversion. For this site, pass-by trips will be those vehicles already traveling through the intersection of NW 72nd Street and N Broadway Street. Chapter 10 and Appendix E of the ITE Trip Generation Handbook, 3rd Edition were consulted in estimating these trips. Research indicates that on average 76 percent of AM Peak Period Hour and 75 percent of PM Peak Hour for land use 945 are pass-by in nature. The Trip Generation volumes anticipated by the development are shown in Table 2 below.

Table 2: ITE Trip Generation

<i>Land Use</i>	<i>Intensity</i>	<i>ITE Code</i>	<i>AM Peak Hour</i>			<i>PM Peak Hour</i>		
			<i>Total</i>	<i>In</i>	<i>Out</i>	<i>Total</i>	<i>In</i>	<i>Out</i>
Convenience Store/Gas Station (VFP 9-15)	5,000 SF	945	283	141	142	273	136	137
			-215	-107	-108	-205	-102	-103
Subtotal			283	141	142	273	136	137
<i>Pass-By Trips</i>			-215	-107	-108	-205	-102	-103
Total New Trips			68	34	34	68	34	34

5) TRIP DISTRIBUTION AND ASSIGNMENT

Trips generated by the Gladstone Convenience Store development were distributed based on existing traffic flows and a general analysis of the surrounding area. The trips were distributed onto the existing street system approximately as follows:

- 15 percent to and from the north via N Broadway Street
- 40 percent to and from the south via N Broadway Street
- 40 percent to and from the east via NW 72nd Street
- 5 percent to and from the west via NW 72nd Street

Pass-by trips were distributed based upon the existing traffic patterns near the study intersection of NW 72nd Street and N Broadway Street.

6) LEVEL OF SERVICE AND VOLUME/CAPACITY ANALYSES

Capacity analysis was used to quantify the impacts of the increased traffic on the intersections studied. The methodology outlined in the Highway Capacity Manual, 7th Edition was used as a basis to perform the analysis for this study. Capacity analysis defines the quality of traffic operation for an intersection using a grading system called Level of Service (LOS). The LOS is defined in terms of average vehicle delay. Levels of service A through F have been established with A representing the best and F the worst.

Table 3: Level of Service Definitions

<i>Level of Service</i>	<i>Unsignalized Intersection</i>	<i>Signalized Intersection</i>
A	< 10 Seconds	< 10 Seconds
B	< 15 Seconds	< 20 Seconds
C	< 25 Seconds	< 35 Seconds
D	< 35 Seconds	< 55 Seconds
E	< 50 Seconds	< 80 Seconds
F	≥ 50 Seconds	≥ 80 Seconds

The study intersections were evaluated using Synchro based on part on Highway Capacity Manual methods. The analysis reports are included in Appendix II. Signal Timing Inputs were based upon data provided by City Staff.

Existing Conditions

The levels of service, lane configuration, and queue lengths for existing conditions are shown in Figures 5 and 6 in Appendix I.

During the AM and PM Peak Hours, the overall level of service for the signalized intersection at NW 72nd Street and North Broadway Street is a C in both the AM and PM Peak Hour.

At all STOP-controlled intersections within the study area, the minor movements operate with a level of service B or better during both AM and PM Peak Hours.

Existing + Proposed Development Conditions

The levels of service, lane configuration, and queue lengths for existing conditions are shown in Figures 9 and 10 in Appendix I.

The overall level of service remains a C in both Peak Hours for the signalized intersection with the addition of the traffic generated by the proposed development.

All STOP controlled intersections within the study area operate with a level of service C or better during both Peak Hours.

7) SIGHT DISTANCE

Intersection sight distance and stopping sight distance was measured at the proposed entrances into the development. Intersection sight distance represents the distance and time required for the driver to make the decision to turn and to complete the turn without slowing oncoming traffic. Stopping sight distance represents the amount of distance required for a driver to make an unexpected stopping maneuver based upon observing a 2' tall object in the roadway. At both locations, the AASHTO minimum sight distance for a 35 MPH design speed.

8) ACCESS MANAGEMENT

The proposed drive onto N Broadway Street is located between two existing intersections located on the east side of the street. The drive into Gladstone Bowl is approximately 110' from the intersection of NW 72nd Street and N Broadway Street. Typically, it would be recommended that proposed drive be aligned with an existing drive to minimize turning conflicts. It is not recommended that the drive be located at the Gladstone Bowl drive due to the proximity of this drive to the signalized intersection. The proposed drive however is located approximately as far north as possible and has an approximate offset of 35' from the entrance further to the north. The next entrance to the north has a spacing of approximately 160' to the north from the Gladstone Bowl Entrance.

APWA section 5200 spacing requirements can not be met due to the close proximity of the existing entrances on the east side of N Broadway Street. The proposed drive, however, is located as far north as possible to minimize the impact of the entrance on the function of the intersection.

The entrances at both NW 72nd Street and N Broadway Street were evaluated for right and left turn lanes in accordance with the methodology associated with NCHRP Report 457 using the turn lane guidelines found in MoDOT EPG section 940.9.

At the entrance on NW 72nd Street, neither a left turn lane (EPG Section 940.9.1 left turn guidelines for roads less than or equal to 40 MPH) nor a right turn lane guideline (EPG 940.9.8 right turn lane guidance for two lane roads) is met.

At the entrance onto N Broadway Street a right turn lane is not recommended (EPG 940.9.8 right turn lane guidance for two lane roads), but a left turn lane is recommended when the 40% left turn trend line is selected as per EPG guidance. This is documented in Figure 11 of Appendix I.

9) RECOMMENDATIONS & CONCLUSIONS

This study documents the impact of the proposed Gladstone Convenience Store development on the adjacent roadway network during the AM and PM Peak Hour. Analysis of unsignalized intersections indicate that they operate with acceptable levels of service both before and after the construction of the proposed development. The signalized intersection at NW 72nd Street and N Broadway Street has an overall level of service that is acceptable both before and after construction of the proposed development.

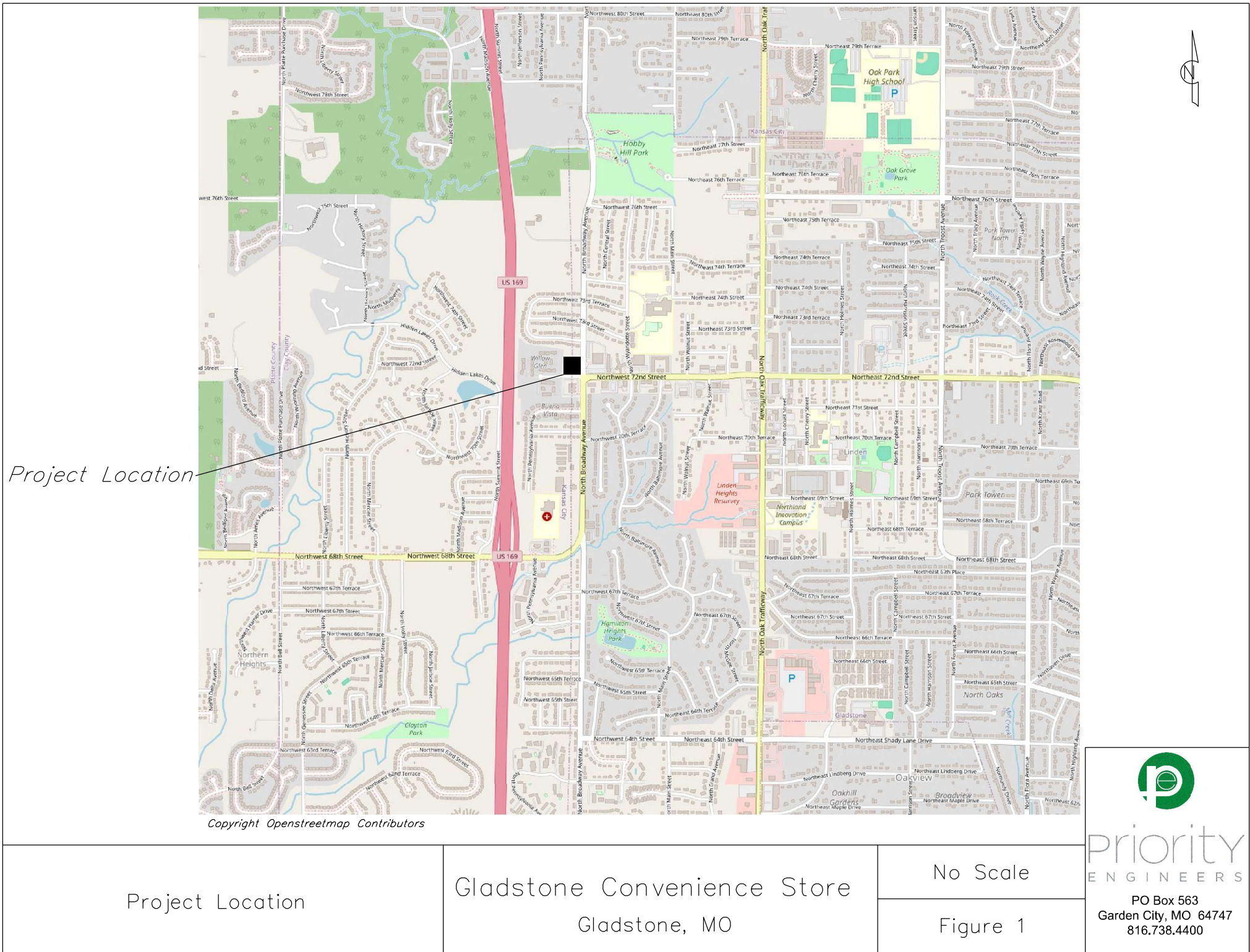
The proposed entrance locations have sufficient sight distance.

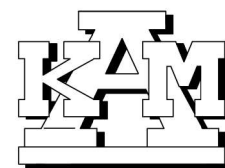
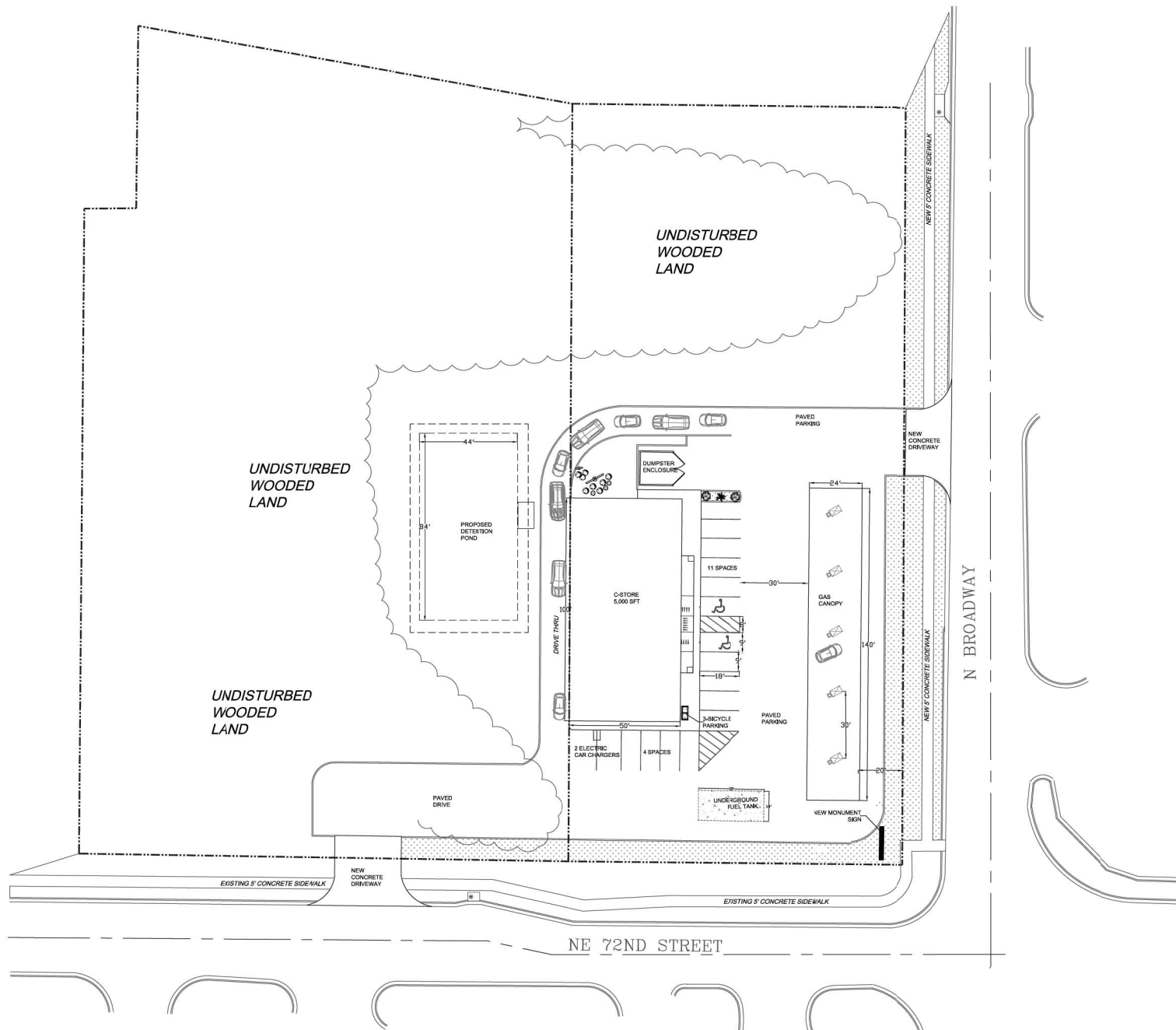
A left turn lane is recommended according to MoDOT guidelines for the entrance on N Broadway Street in the PM Peak Hour. Due to the geometric constraints of this location, if such a turn lane were constructed, it would need to be designed so that it does not interfere with the southbound left turn lane at the signalized intersection with NW 72nd Street. The levels of service at this entrance without the left turn lane are a B or better with a design queue of less than one vehicle.

No other improvements are required as a result of this development.

APPENDIX I

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Left Turn Lane Guidelines for Two-Lane Roads less than or equal to 40 mph (MoDOT EPG Figure 940.9.1)	Figure 11





Design Group LLC.
9000 E Bannister Road
Suite 100
Kansas City, Missouri 64134
(816) 797-2065



priority
ENGINEERS

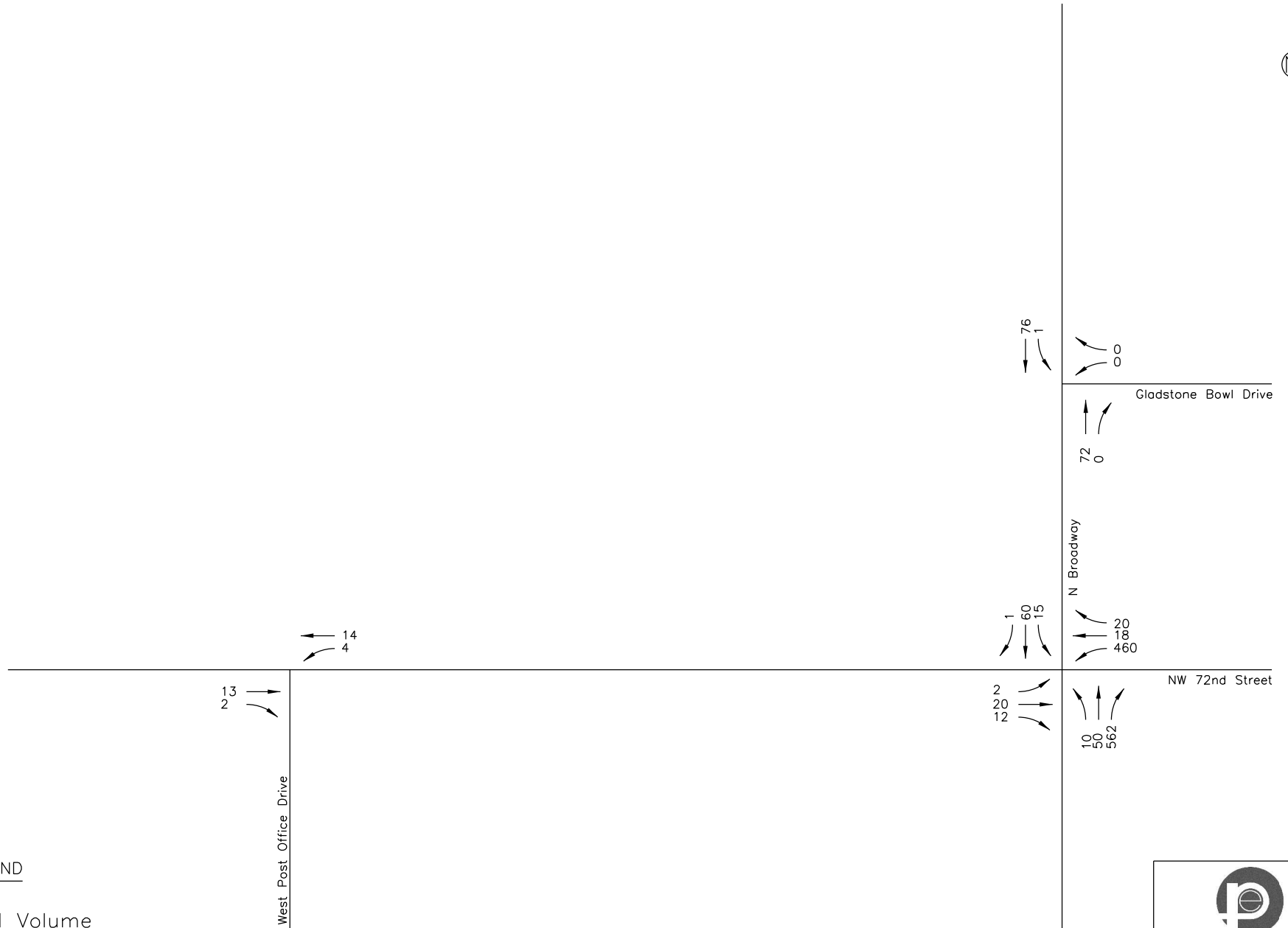
PO Box 563
Garden City, MO 64747
816.738.4400

Site Plan

Gladstone Convenience Store
Gladstone, MO

No Scale

Figure 2

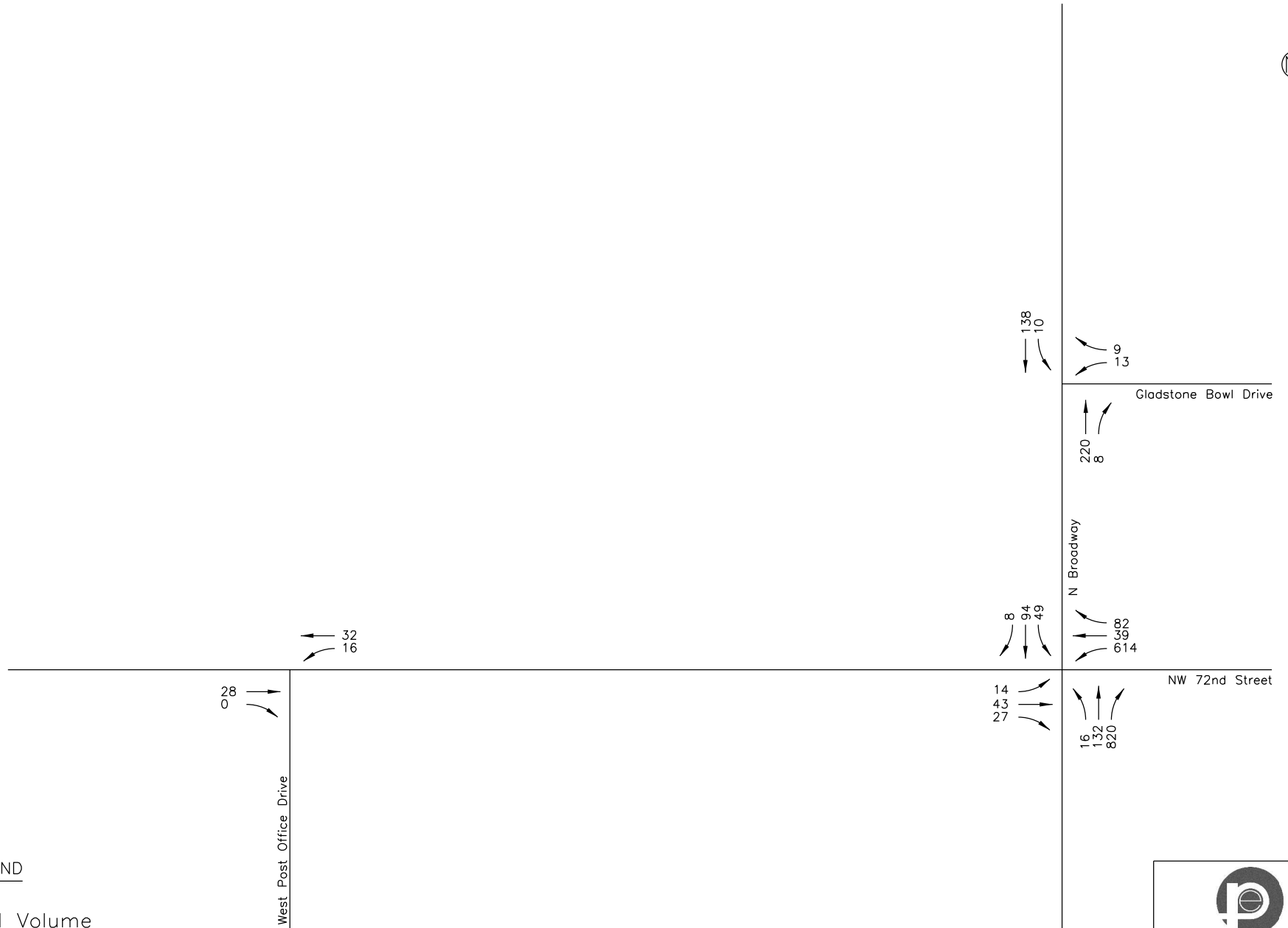


Existing AM Peak Hour
Traffic Volumes

Gladstone Convenience Store
Gladstone, MO

No Scale

Figure 3



Existing PM Peak Hour
Traffic Volumes

Gladstone Convenience Store
Gladstone, MO

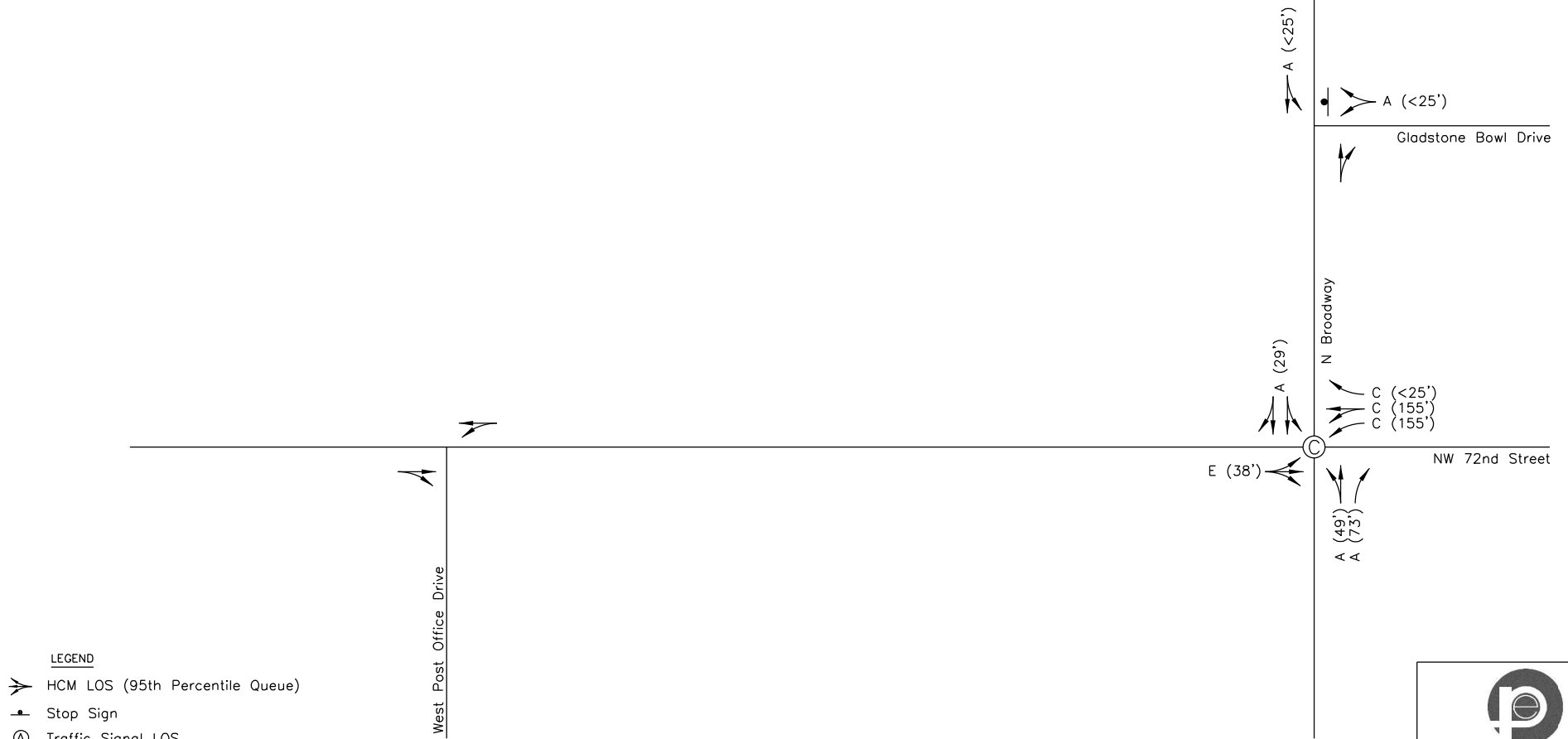
No Scale

Figure 4



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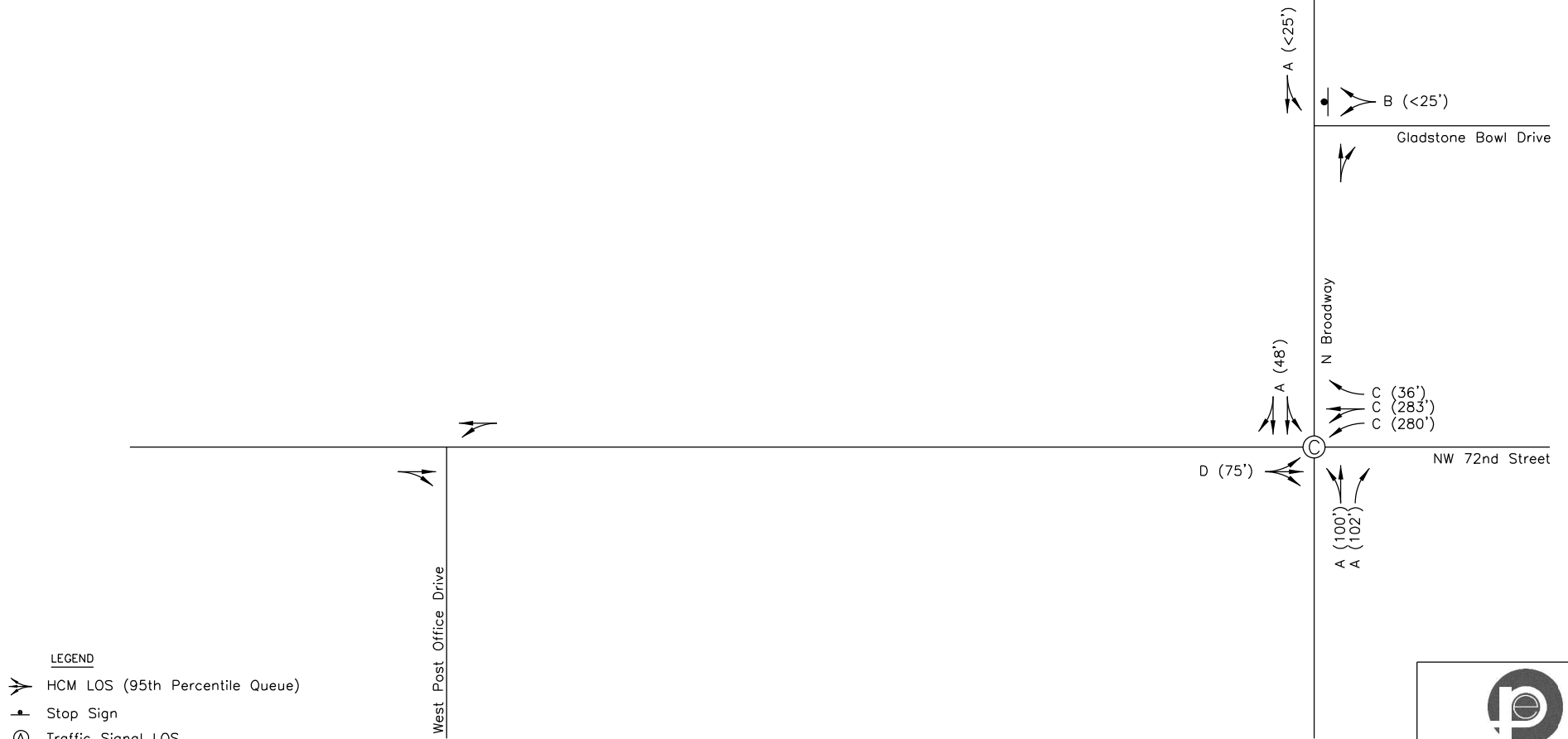


Existing AM Peak Hour
Lane Configuration &
Levels of Service

Gladstone Convenience Store
Gladstone, MO

No Scale
Figure 5


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Garden City, MO 64747
816.738.4400



Existing PM Peak Hour
Lane Configuration &
Levels of Service

Gladstone Convenience Store
Gladstone, MO

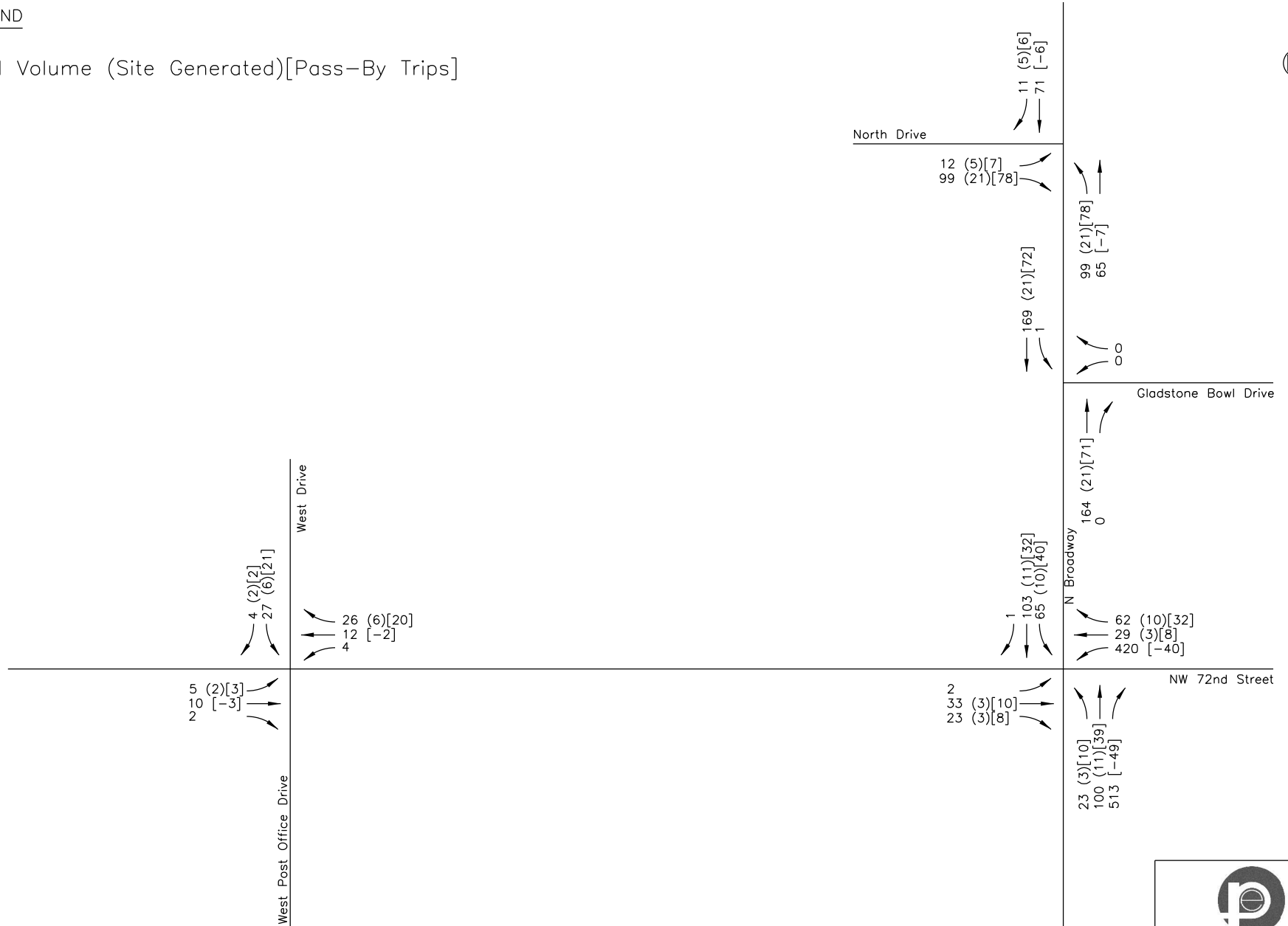
No Scale

Figure 6


priority
ENGINEERS
PO Box 563
Garden City, MO 64747
816.738.4400

LEGEND

 Total Volume (Site Generated)[Pass-By Trips]



Existing + Proposed Development
AM Peak Hour
Traffic Volumes

Gladstone Convenience Store
Gladstone, MO

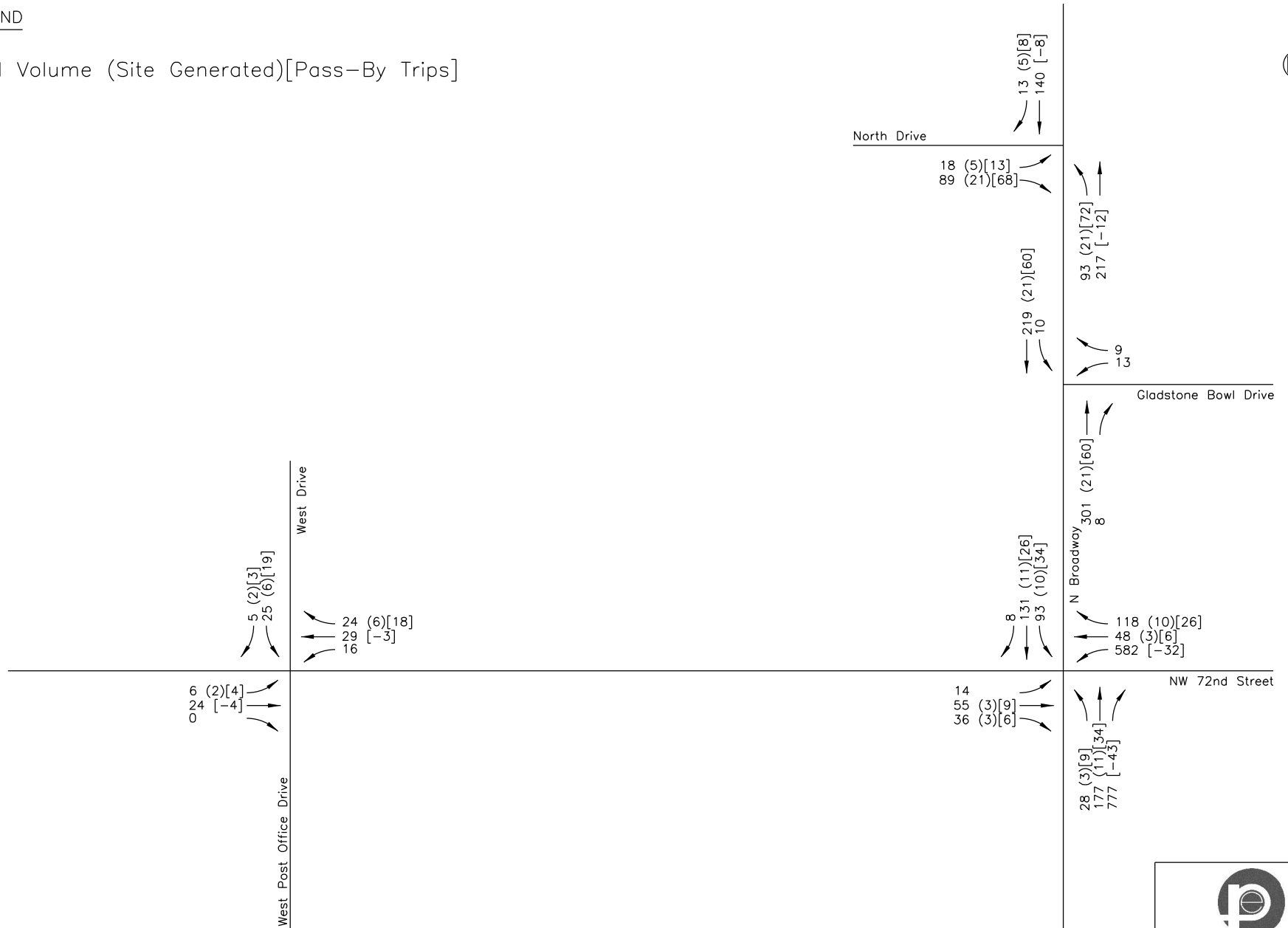
No Scale

Figure 7

LEGEND



Total Volume (Site Generated)[Pass-By Trips]

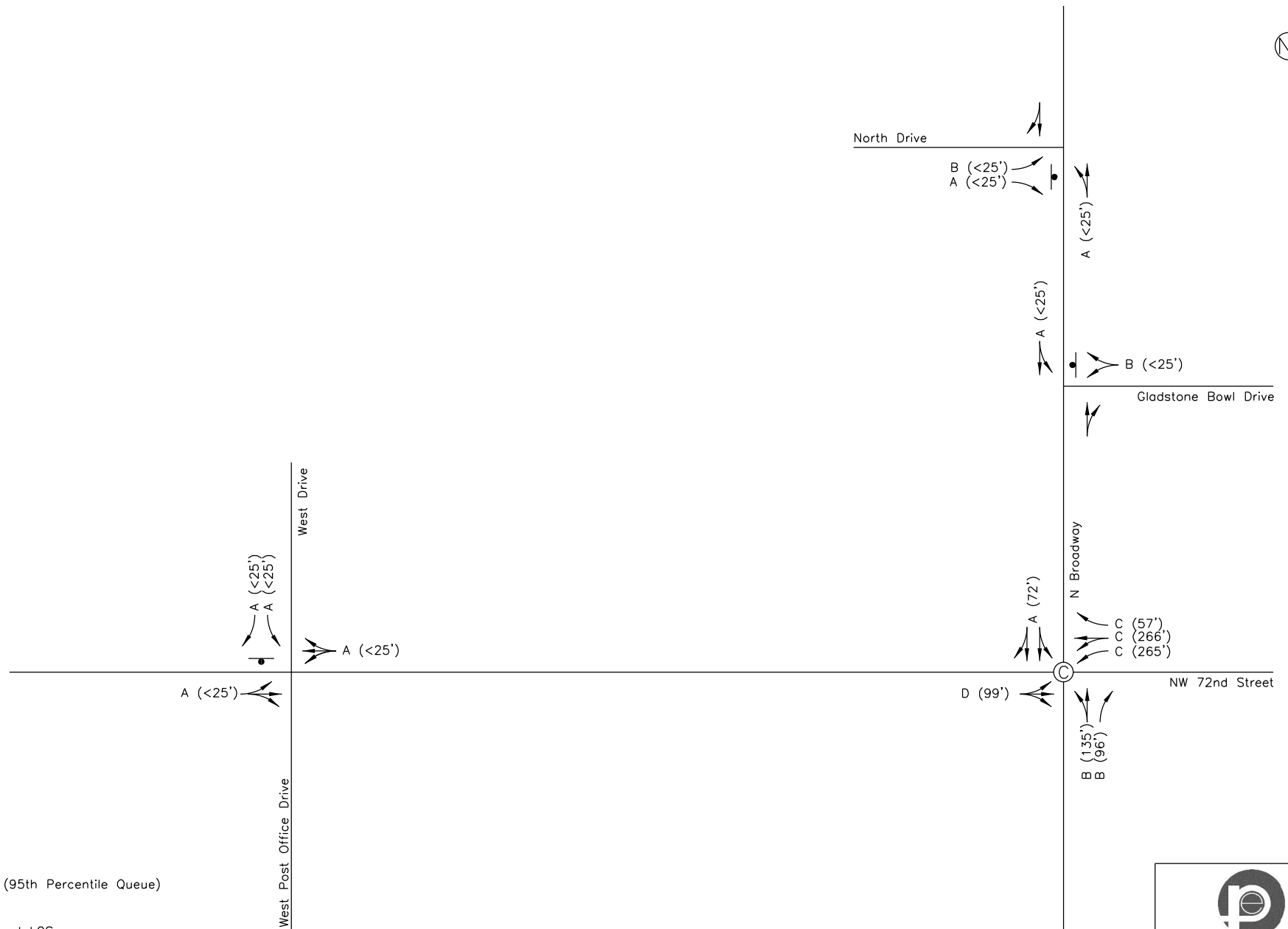


Existing + Proposed Development
PM Peak Hour
Traffic Volumes

Gladstone Convenience Store
Gladstone, MO

No Scale

Figure 8

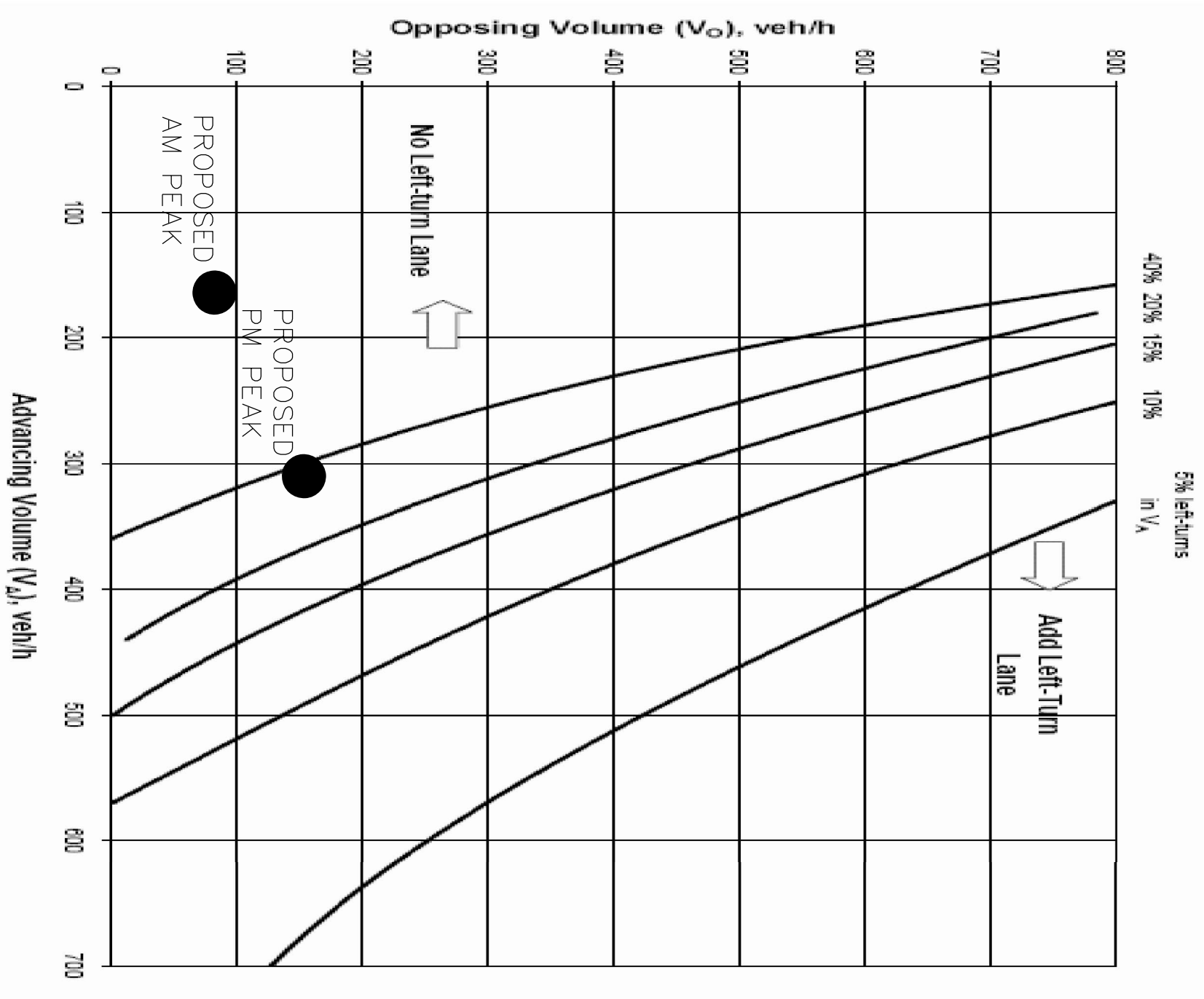


Existing + Proposed Development
PM Peak Hour
Lane Configuration &
Levels of Service

Gladstone Convenience Store
Gladstone, MO

No Scale

Figure 10



Left Turn Lane Guidelines
for Two-Lane Roads less
than or equal to 40 mph
(MODOT EPG Figure 940.9.1)

Gladstone
Convenience Store
Gladstone, MO

No Scale
Figure 11

APPENDIX II

Peak Hour Traffic Counts

Synchro Reports

Existing AM Peak Hour

Pages 1-3

Existing PM Peak Hour

Pages 4-6

Proposed AM Peak Hour

Pages 7-11

Proposed PM Peak Hour

Pages 12-16

Broadway & 72nd Street

Start Time	Southbound				Westbound				Northbound				Eastbound				Totals				
	Left	Through	Right	Ped Bike	Left	Through	Right	Ped Bike	Left	Through	Right	Ped Bike	Left	Through	Right	Ped Bike					
7:00	6	22	0		69	4	7		1	7	62		1	4	4	0		187			
7:15	3	22	0		99	2	4		0	5	79		2	1	0	1		218			
7:30	4	19	0		127	0	3		0	11	125		0	3	2	0		294			
7:45	6	22	1		100	5	11		0	13	136		0	4	1	0		299	998	1187	
8:00	7	23	0		110	2	4		3	11	109		1	3	2	0		275	1086	1275	
8:15	3	17	0		127	4	3		0	7	167		0	3	1	0		332	1200	1381	
8:30	3	14	0		128	5	6		3	16	115		0	3	5	1		299	1205	1393	
8:45	2	6	1		95	7	7		4	16	171		1	11	4	0		325	1231	1408	
Totals	15	60	1	0	0	460	18	20	0	0	10	50	562	0	0	2	20	12	1	0	1231
Trucks		1				6					1		5			2				PHF=	0.93
%		2%				1%					10%		1%			10%					

72nd Street & West Post Office Drive

Start Time	Southbound				Westbound				Northbound				Eastbound				Totals			
	Left	Through	Right	Ped Bike	Left	Through	Right	Ped Bike	Left	Through	Right	Ped Bike	Left	Through	Right	Ped Bike				
7:00					2	2	0	0						5	0	2	11			
7:15					0	1	0	0						1	0	7	9			
7:30					0	0	0	1						4	0	1	6			
7:45					2	2	0	0						1	0	0	5	31		
8:00					2	2	0	0						2	0	0	6	26		
8:15					0	3	0	0						2	0	0	5	22		
8:30					2	3	0	0						3	0	1	9	25		
8:45					0	6	0	0						6	2	0	14	34		
Totals	0	0	0	0	4	14	0	0	0	0	0	0	0	0	0	13	2	1	0	34
Trucks						2										2				
%						14%										15%				
																		PHF=		0.61

Broadway & Gladstone Bowl Drive

[illegible]

Broadway & 72nd Street

	Southbound					Westbound					Northbound					Eastbound							
Start Time	Left	Through	Right	Ped	Bike	Left	Through	Right	Ped	Bike	Left	Through	Right	Ped	Bike	Left	Through	Right	Ped	Bike	Totals		
16:00	18	18	3			127	12	15	0		4	28	166			2	10	4	0		407		
16:15	16	44	4			126	12	10	0		3	29	203			3	14	5	0		469		
16:30	7	32	2			123	14	13	1		5	28	212			4	11	9	0		461		
16:45	12	20	2			150	10	17	0		3	29	209			5	14	9	0		480	1817	2234
17:00	13	25	1			187	7	22	0		3	31	191			3	9	4	0		496	1906	2340
17:15	17	17	3			154	8	30	1		5	44	208			2	9	5	1		504	1941	2404
17:30	12	13	0			142	1	15	0		7	29	166			0	3	4	1		393	1873	2324
17:45	20	24	1			130	5	15	0		5	27	167			1	5	1	0		401	1794	2228
Totals	49	94	8	0	0	614	39	82	2	0	16	132	820	0	0	14	43	27	1	0	1941		
Trucks		3				4	1						7					1		PHF=	0.96		
Truck %		3%				1%	3%						1%					4%					

72nd Street & West Post Office Drive








Start Time	Southbound					Westbound					Northbound					Eastbound					Totals	
	Left	Through	Right	Ped	Bike	Left	Through	Right	Ped	Bike	Left	Through	Right	Ped	Bike	Left	Through	Right	Ped	Bike		
16:00						8	3		0							2			0		13	
16:15						4	7		0							5			0		16	
16:30						6	5		1							3			0		15	
16:45						4	9		0							8			0		21	65
17:00						3	7		0							8			0		18	70
17:15						3	11		1							9			0		24	78
17:30						1	7		0							6			1		15	78
17:45						0	7		0							3			0		10	67
Totals	0	0	0	0	0	16	32	0	2	0	0	0	0	0	0	0	28	0	0	0	78	
Trucks							1										1					
Truck %							3%										4%					
																			PHF=		0.81	

Broadway & Gladstone Bowl Drive

[illegible]




















3: N Broadway & 72nd Street

Existing AM Peak Hour

							
Lane Group	EBT	WBL	WBT	WBR	NBT	NBR	SBT
Lane Group Flow (vph)	37	257	257	22	65	604	82
v/c Ratio	0.45	0.57	0.57	0.04	0.07	0.54	0.04
Control Delay (s/veh)	39.8	28.0	27.9	0.2	14.9	4.0	14.1
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay (s/veh)	39.8	28.0	27.9	0.2	14.9	4.0	14.1
Queue Length 50th (ft)	11	108	108	0	16	0	10
Queue Length 95th (ft)	38	155	155	0	49	73	29
Internal Link Dist (ft)	204		604		384		28
Turn Bay Length (ft)				25			
Base Capacity (vph)	161	496	499	518	911	1105	1664
Starvation Cap Reductn	0	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0	0
Reduced v/c Ratio	0.23	0.52	0.52	0.04	0.07	0.55	0.05
Intersection Summary							

3: N Broadway & 72nd Street

Existing AM Peak Hour

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (veh/h)	2	20	12	460	18	20	10	50	562	15	60	1
Future Volume (veh/h)	2	20	12	460	18	20	10	50	562	15	60	1
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Lane Width Adj.	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach	No			No			No			No		
Adj Sat Flow, veh/h/ln	1870	1752	1870	1870	1870	1870	1752	1870	1870	1870	1870	1870
Adj Flow Rate, veh/h	2	22	13	509	0	22	11	54	0	16	65	1
Peak Hour Factor	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Percent Heavy Veh, %	2	10	2	2	2	2	10	2	2	2	2	2
Cap, veh/h	3	35	21	691	0	307	199	942		410	1672	26
Arrive On Green	0.04	0.04	0.04	0.19	0.00	0.19	0.61	0.61	0.00	0.61	0.61	0.61
Sat Flow, veh/h	89	977	577	3563	0	1585	234	1543	1585	564	2739	43
Grp Volume(v), veh/h	37	0	0	509	0	22	65	0	0	43	0	39
Grp Sat Flow(s),veh/h/ln	1643	0	0	1781	0	1585	1777	0	1585	1653	0	1694
Q Serve(g_s), s	1.7	0.0	0.0	10.1	0.0	0.9	0.0	0.0	0.0	0.0	0.0	0.7
Cycle Q Clear(g_c), s	1.7	0.0	0.0	10.1	0.0	0.9	1.1	0.0	0.0	0.7	0.0	0.7
Prop In Lane	0.05		0.35	1.00		1.00	0.17		1.00	0.37		0.03
Lane Grp Cap(c), veh/h	59	0	0	691	0	307	1141	0		1075	0	1034
V/C Ratio(X)	0.63	0.00	0.00	0.74	0.00	0.07	0.06	0.00		0.04	0.00	0.04
Avail Cap(c_a), veh/h	438	0	0	950	0	423	1141	0		1075	0	1034
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	0.00	0.00	1.00	0.00	1.00	1.00	0.00	0.00	1.00	0.00	1.00
Uniform Delay (d), s/veh	35.7	0.0	0.0	28.4	0.0	24.7	5.9	0.0	0.0	5.8	0.0	5.8
Incr Delay (d2), s/veh	21.2	0.0	0.0	3.6	0.0	0.2	0.1	0.0	0.0	0.1	0.0	0.1
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	1.0	0.0	0.0	4.4	0.0	0.3	0.4	0.0	0.0	0.3	0.0	0.2
Unsig. Movement Delay, s/veh												
LnGrp Delay(d), s/veh	56.9	0.0	0.0	32.0	0.0	24.9	6.0	0.0	0.0	5.9	0.0	5.9
LnGrp LOS	E			C		C	A			A		A
Approach Vol, veh/h	37			531			65			82		
Approach Delay, s/veh	56.9			31.7			6.0			5.9		
Approach LOS	E			C			A			A		
Timer - Assigned Phs	2			4			6			8		
Phs Duration (G+Y+Rc), s	49.8			6.7			49.8			18.5		
Change Period (Y+Rc), s	4.0			4.0			4.0			4.0		
Max Green Setting (Gmax), s	23.0			20.0			23.0			20.0		
Max Q Clear Time (g_c+l1), s	3.1			3.7			2.7			12.1		
Green Ext Time (p_c), s	0.4			0.2			0.6			2.5		

Intersection Summary

HCM 7th Control Delay, s/veh	27.7
HCM 7th LOS	C




Notes

User approved volume balancing among the lanes for turning movement.

Unsignalized Delay for [NBR] is excluded from calculations of the approach delay and intersection delay.








6: N Broadway & Gladstone Bowl Drive

Existing AM Peak Hour

Intersection						
Int Delay, s/veh	0.1					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	0	0	72	0	1	76
Future Vol, veh/h	0	0	72	0	1	76
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	50	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	79	79	79	79	79	79
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	0	91	0	1	96
Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	142	91	0	0	91	0
Stage 1	91	-	-	-	-	-
Stage 2	51	-	-	-	-	-
Critical Hdwy	6.63	6.23	-	-	4.13	-
Critical Hdwy Stg 1	5.43	-	-	-	-	-
Critical Hdwy Stg 2	5.83	-	-	-	-	-
Follow-up Hdwy	3.519	3.319	-	-	2.219	-
Pot Cap-1 Maneuver	844	966	-	-	1503	-
Stage 1	932	-	-	-	-	-
Stage 2	966	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	843	966	-	-	1503	-
Mov Cap-2 Maneuver	843	-	-	-	-	-
Stage 1	932	-	-	-	-	-
Stage 2	965	-	-	-	-	-
Approach	WB	NB		SB		
HCM Control Delay, s/v	0	0		0.1		
HCM LOS	A					
Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT		
Capacity (veh/h)	-	-	-	47	-	
HCM Lane V/C Ratio	-	-	-	0.001	-	
HCM Control Delay (s/veh)	-	-	0	7.4	0	
HCM Lane LOS	-	-	A	A	A	
HCM 95th %tile Q(veh)	-	-	-	0	-	

3: N Broadway & 72nd Street

Existing PM Peak Hour




















							
Lane Group	EBT	WBL	WBT	WBR	NBT	NBR	SBT
Lane Group Flow (vph)	88	339	342	85	155	854	157
v/c Ratio	0.72	0.70	0.70	0.16	0.21	0.74	0.13
Control Delay (s/veh)	51.3	33.4	33.4	7.8	18.9	6.7	16.9
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay (s/veh)	51.3	33.4	33.4	7.8	18.9	6.7	16.9
Queue Length 50th (ft)	26	134	135	4	53	0	25
Queue Length 95th (ft)	#75	#280	#283	36	100	102	48
Internal Link Dist (ft)	204		604		384		28
Turn Bay Length (ft)				25			
Base Capacity (vph)	171	501	504	523	736	1151	1206
Starvation Cap Reductn	0	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0	0
Reduced v/c Ratio	0.51	0.68	0.68	0.16	0.21	0.74	0.13

Intersection Summary

95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.




3: N Broadway & 72nd Street

Existing PM Peak Hour

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (veh/h)	14	43	27	614	39	82	16	132	820	49	94	8
Future Volume (veh/h)	14	43	27	614	39	82	16	132	820	49	94	8
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Lane Width Adj.	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach	No			No			No			No		
Adj Sat Flow, veh/h/ln	1870	1870	1841	1870	1856	1870	1870	1870	1870	1870	1856	1870
Adj Flow Rate, veh/h	15	45	28	669	0	85	17	138	0	51	98	8
Peak Hour Factor	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Percent Heavy Veh, %	2	2	4	2	3	2	2	2	2	2	3	2
Cap, veh/h	21	63	39	836	0	372	120	905		546	1101	94
Arrive On Green	0.07	0.07	0.07	0.23	0.00	0.23	0.54	0.54	0.00	0.54	0.54	0.54
Sat Flow, veh/h	299	897	558	3563	0	1585	124	1690	1585	874	2055	175
Grp Volume(v), veh/h	88	0	0	669	0	85	155	0	0	81	0	76
Grp Sat Flow(s),veh/h/ln	1755	0	0	1781	0	1585	1814	0	1585	1447	0	1657
Q Serve(g_s), s	3.7	0.0	0.0	13.3	0.0	3.3	0.0	0.0	0.0	0.0	0.0	1.7
Cycle Q Clear(g_c), s	3.7	0.0	0.0	13.3	0.0	3.3	3.1	0.0	0.0	1.6	0.0	1.7
Prop In Lane	0.17		0.32	1.00		1.00	0.11		1.00	0.63		0.11
Lane Grp Cap(c), veh/h	122	0	0	836	0	372	1025	0		854	0	888
V/C Ratio(X)	0.72	0.00	0.00	0.80	0.00	0.23	0.15	0.00		0.10	0.00	0.09
Avail Cap(c_a), veh/h	468	0	0	950	0	423	1025	0		854	0	888
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	0.00	0.00	1.00	0.00	1.00	1.00	0.00	0.00	1.00	0.00	1.00
Uniform Delay (d), s/veh	34.2	0.0	0.0	27.0	0.0	23.2	8.8	0.0	0.0	8.5	0.0	8.5
Incr Delay (d2), s/veh	15.6	0.0	0.0	5.5	0.0	0.7	0.3	0.0	0.0	0.2	0.0	0.2
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	2.0	0.0	0.0	5.9	0.0	1.2	1.2	0.0	0.0	0.6	0.0	0.6
Unsig. Movement Delay, s/veh												
LnGrp Delay(d), s/veh	49.7	0.0	0.0	32.6	0.0	23.9	9.1	0.0	0.0	8.7	0.0	8.7
LnGrp LOS	D			C		C	A			A		A
Approach Vol, veh/h	88			754			155			157		
Approach Delay, s/veh	49.7			31.6			9.1			8.7		
Approach LOS	D			C			A			A		
Timer - Assigned Phs	2			4			6			8		
Phs Duration (G+Y+Rc), s	44.2			9.2			44.2			21.6		
Change Period (Y+Rc), s	4.0			4.0			4.0			4.0		
Max Green Setting (Gmax), s	23.0			20.0			23.0			20.0		
Max Q Clear Time (g_c+I1), s	5.1			5.7			3.7			15.3		
Green Ext Time (p_c), s	1.3			0.5			1.4			2.3		
Intersection Summary												
HCM 7th Control Delay, s/veh				26.9								
HCM 7th LOS				C								
Notes												
User approved volume balancing among the lanes for turning movement.												
Unsignalized Delay for [NBR] is excluded from calculations of the approach delay and intersection delay.												

6: N Broadway & Gladstone Bowl Drive

Existing PM Peak Hour

Intersection						
Int Delay, s/veh	0.8					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	13	9	220	8	10	138
Future Vol, veh/h	13	9	220	8	10	138
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	50	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	82	82	82	82	82	82
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	16	11	268	10	12	168
Major/Minor	Minor1	Major1		Major2		
Conflicting Flow All	382	273	0	0	278	0
Stage 1	273	-	-	-	-	-
Stage 2	109	-	-	-	-	-
Critical Hdwy	6.63	6.23	-	-	4.13	-
Critical Hdwy Stg 1	5.43	-	-	-	-	-
Critical Hdwy Stg 2	5.83	-	-	-	-	-
Follow-up Hdwy	3.519	3.319	-	-	2.219	-
Pot Cap-1 Maneuver	607	765	-	-	1283	-
Stage 1	772	-	-	-	-	-
Stage 2	904	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	601	765	-	-	1283	-
Mov Cap-2 Maneuver	601	-	-	-	-	-
Stage 1	772	-	-	-	-	-
Stage 2	896	-	-	-	-	-
Approach	WB	NB		SB		
HCM Control Delay, s/v	10.7	0		0.59		
HCM LOS	B					
Minor Lane/Major Mvmt	NBT	NBRWBLn1		SBL	SBT	
Capacity (veh/h)	-	-		659	243	-
HCM Lane V/C Ratio	-	-		0.041	0.01	-
HCM Control Delay (s/veh)	-	-		10.7	7.8	0.1
HCM Lane LOS	-	-		B	A	A
HCM 95th %tile Q(veh)	-	-		0.1	0	-

3: N Broadway & 72nd Street

Existing + Proposed Development AM Peak Hour






















Lane Group	EBT	WBL	WBT	WBR	NBT	NBR	SBT
Lane Group Flow (vph)	62	240	243	67	133	552	182
v/c Ratio	0.64	0.55	0.56	0.14	0.15	0.51	0.12
Control Delay (s/veh)	50.7	28.3	28.3	5.2	15.0	3.9	13.8
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay (s/veh)	50.7	28.3	28.3	5.2	15.0	3.9	13.8
Queue Length 50th (ft)	16	102	103	0	35	0	24
Queue Length 95th (ft)	#64	151	153	22	88	69	56
Internal Link Dist (ft)	204		604		384		28
Turn Bay Length (ft)				25			
Base Capacity (vph)	165	488	492	511	880	1078	1488
Starvation Cap Reductn	0	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0	0
Reduced v/c Ratio	0.38	0.49	0.49	0.13	0.15	0.51	0.12

Intersection Summary

95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.




3: N Broadway & 72nd Street

Existing + Proposed Development AM Peak Hour

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (veh/h)	2	33	23	420	29	62	23	100	513	65	103	1
Future Volume (veh/h)	2	33	23	420	29	62	23	100	513	65	103	1
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Lane Width Adj.	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach	No			No			No			No		
Adj Sat Flow, veh/h/ln	1870	1752	1870	1870	1870	1870	1752	1870	1870	1870	1870	1870
Adj Flow Rate, veh/h	2	35	25	474	0	67	25	108	0	70	111	1
Peak Hour Factor	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Percent Heavy Veh, %	2	10	2	2	2	2	10	2	2	2	2	2
Cap, veh/h	3	46	33	665	0	296	215	897		712	1239	12
Arrive On Green	0.05	0.05	0.05	0.19	0.00	0.19	0.60	0.60	0.00	0.60	0.60	0.60
Sat Flow, veh/h	53	921	658	3563	0	1585	262	1487	1585	1042	2054	19
Grp Volume(v), veh/h	62	0	0	474	0	67	133	0	0	93	0	89
Grp Sat Flow(s),veh/h/ln	1631	0	0	1781	0	1585	1750	0	1585	1416	0	1699
Q Serve(g_s), s	2.8	0.0	0.0	9.4	0.0	2.7	0.0	0.0	0.0	0.0	0.0	1.6
Cycle Q Clear(g_c), s	2.8	0.0	0.0	9.4	0.0	2.7	2.3	0.0	0.0	1.6	0.0	1.6
Prop In Lane	0.03		0.40	1.00		1.00	0.19		1.00	0.75		0.01
Lane Grp Cap(c), veh/h	81	0	0	665	0	296	1113	0		938	0	1025
V/C Ratio(X)	0.76	0.00	0.00	0.71	0.00	0.23	0.12	0.00		0.10	0.00	0.09
Avail Cap(c_a), veh/h	435	0	0	950	0	423	1113	0		938	0	1025
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	0.00	0.00	1.00	0.00	1.00	1.00	0.00	0.00	1.00	0.00	1.00
Uniform Delay (d), s/veh	35.2	0.0	0.0	28.6	0.0	25.9	6.4	0.0	0.0	6.2	0.0	6.2
Incr Delay (d2), s/veh	26.3	0.0	0.0	3.0	0.0	0.8	0.2	0.0	0.0	0.2	0.0	0.2
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	1.7	0.0	0.0	4.1	0.0	1.0	0.8	0.0	0.0	0.6	0.0	0.5
Unsig. Movement Delay, s/veh												
LnGrp Delay(d), s/veh	61.5	0.0	0.0	31.6	0.0	26.7	6.6	0.0	0.0	6.4	0.0	6.4
LnGrp LOS	E			C		C	A			A		A
Approach Vol, veh/h	62			541			133			182		
Approach Delay, s/veh	61.5			31.0			6.6			6.4		
Approach LOS	E			C			A			A		
Timer - Assigned Phs	2			4			6			8		
Phs Duration (G+Y+Rc), s	49.3			7.7			49.3			18.0		
Change Period (Y+Rc), s	4.0			4.0			4.0			4.0		
Max Green Setting (Gmax), s	23.0			20.0			23.0			20.0		
Max Q Clear Time (g_c+I1), s	4.3			4.8			3.6			11.4		
Green Ext Time (p_c), s	1.1			0.3			1.7			2.6		
Intersection Summary												
HCM 7th Control Delay, s/veh				24.7								
HCM 7th LOS				C								
Notes												
User approved volume balancing among the lanes for turning movement.												
Unsignalized Delay for [NBR] is excluded from calculations of the approach delay and intersection delay.												

6: N Broadway & Gladstone Bowl Drive

Existing + Proposed Development AM Peak Hour

Intersection						
Int Delay, s/veh	0					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	0	0	164	0	1	169
Future Vol, veh/h	0	0	164	0	1	169
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	50	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	79	79	79	79	79	79
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	0	208	0	1	214
Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	317	208	0	0	208	0
Stage 1	208	-	-	-	-	-
Stage 2	109	-	-	-	-	-
Critical Hdwy	6.63	6.23	-	-	4.13	-
Critical Hdwy Stg 1	5.43	-	-	-	-	-
Critical Hdwy Stg 2	5.83	-	-	-	-	-
Follow-up Hdwy	3.519	3.319	-	-	2.219	-
Pot Cap-1 Maneuver	663	832	-	-	1362	-
Stage 1	826	-	-	-	-	-
Stage 2	903	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	663	832	-	-	1362	-
Mov Cap-2 Maneuver	663	-	-	-	-	-
Stage 1	826	-	-	-	-	-
Stage 2	903	-	-	-	-	-
Approach	WB	NB		SB		
HCM Control Delay, s/v	0	0		0.05		
HCM LOS	A					
Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT		
Capacity (veh/h)	-	-	-	21	-	
HCM Lane V/C Ratio	-	-	-	0.001	-	
HCM Control Delay (s/veh)	-	-	0	7.6	0	
HCM Lane LOS	-	-	A	A	A	
HCM 95th %tile Q(veh)	-	-	-	0	-	





8: West Post Office Drive/West Drive & 72nd Street

Existing + Proposed Development AM Peak Hour

Intersection												
Int Delay, s/veh	3.4											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕					↕	↕	
Traffic Vol, veh/h	5	10	2	4	12	26	0	0	0	27	0	4
Future Vol, veh/h	5	10	2	4	12	26	0	0	0	27	0	4
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	92	61	61	61	61	92	61	92	61	92	92	92
Heavy Vehicles, %	2	15	2	2	14	2	2	2	2	2	2	2
Mvmt Flow	5	16	3	7	20	28	0	0	0	29	0	4
Major/Minor	Major1			Major2			Minor2					
Conflicting Flow All	48	0	0	20	0	0				74	77	34
Stage 1	-	-	-	-	-	-				47	47	-
Stage 2	-	-	-	-	-	-				27	31	-
Critical Hdwy	4.12	-	-	4.12	-	-				6.42	6.52	6.22
Critical Hdwy Stg 1	-	-	-	-	-	-				5.42	5.52	-
Critical Hdwy Stg 2	-	-	-	-	-	-				5.42	5.52	-
Follow-up Hdwy	2.218	-	-	2.218	-	-				3.518	4.018	3.318
Pot Cap-1 Maneuver	1559	-	-	1597	-	-				929	813	1039
Stage 1	-	-	-	-	-	-				976	856	-
Stage 2	-	-	-	-	-	-				995	870	-
Platoon blocked, %		-	-		-	-						
Mov Cap-1 Maneuver	1559	-	-	1597	-	-				922	0	1039
Mov Cap-2 Maneuver	-	-	-	-	-	-				922	0	-
Stage 1	-	-	-	-	-	-				972	0	-
Stage 2	-	-	-	-	-	-				991	0	-
Approach	EB			WB			SB					
HCM Control Delay, s/v	1.58			0.87			8.96					
HCM LOS							A					
Minor Lane/Major Mvmt	EBL	EBT	EBR	WBL	WBT	WBR	SBLn1	SBLn2				
Capacity (veh/h)	377	-	-	194	-	-	922	1039				
HCM Lane V/C Ratio	0.003	-	-	0.004	-	-	0.032	0.004				
HCM Control Delay (s/veh)	7.3	0	-	7.3	0	-	9	8.5				
HCM Lane LOS	A	A	-	A	A	-	A	A				
HCM 95th %tile Q(veh)	0	-	-	0	-	-	0.1	0				

10: N Broadway & North Drive

Existing + Proposed Development AM Peak Hour

Intersection						
Int Delay, s/veh	5					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Vol, veh/h	12	99	99	65	71	11
Future Vol, veh/h	12	99	99	65	71	11
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	-	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	13	108	108	71	77	12
Major/Minor	Minor2	Major1		Major2		
Conflicting Flow All	369	83	89	0	-	0
Stage 1	83	-	-	-	-	-
Stage 2	286	-	-	-	-	-
Critical Hdwy	6.42	6.22	4.12	-	-	-
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-	-
Follow-up Hdwy	3.518	3.318	2.218	-	-	-
Pot Cap-1 Maneuver	631	976	1506	-	-	-
Stage 1	940	-	-	-	-	-
Stage 2	763	-	-	-	-	-
Platoon blocked, %				-	-	-
Mov Cap-1 Maneuver	584	976	1506	-	-	-
Mov Cap-2 Maneuver	584	-	-	-	-	-
Stage 1	870	-	-	-	-	-
Stage 2	763	-	-	-	-	-
Approach	EB	NB		SB		
HCM Control Delay, s/v	9.38	4.57		0		
HCM LOS	A					
Minor Lane/Major Mvmt	NBL	NBT	EBLn1	EBLn2	SBT	SBR
Capacity (veh/h)	1087	-	584	976	-	-
HCM Lane V/C Ratio	0.071	-	0.022	0.11	-	-
HCM Control Delay (s/veh)	7.6	0	11.3	9.1	-	-
HCM Lane LOS	A	A	B	A	-	-
HCM 95th %tile Q(veh)	0.2	-	0.1	0.4	-	-

3: N Broadway & 72nd Street

Existing + Proposed Development PM Peak Hour























Lane Group	EBT	WBL	WBT	WBR	NBT	NBR	SBT
Lane Group Flow (vph)	110	327	329	123	213	809	241
v/c Ratio	0.77	0.70	0.70	0.25	0.29	0.72	0.21
Control Delay (s/veh)	53.8	33.8	33.6	11.2	20.0	6.2	18.0
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay (s/veh)	53.8	33.8	33.6	11.2	20.0	6.2	18.0
Queue Length 50th (ft)	33	129	130	16	77	0	43
Queue Length 95th (ft)	#99	#265	#266	57	135	96	72
Internal Link Dist (ft)	204		604		384		28
Turn Bay Length (ft)				25			
Base Capacity (vph)	187	488	492	511	712	1123	1104
Starvation Cap Reductn	0	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0	0
Reduced v/c Ratio	0.59	0.67	0.67	0.24	0.30	0.72	0.22

Intersection Summary

95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

3: N Broadway & 72nd Street

Existing + Proposed Development PM Peak Hour

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (veh/h)	14	55	36	582	48	118	28	177	777	93	131	8
Future Volume (veh/h)	14	55	36	582	48	118	28	177	777	93	131	8
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Lane Width Adj.	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach	No			No			No			No		
Adj Sat Flow, veh/h/ln	1870	1870	1841	1870	1856	1870	1870	1870	1870	1870	1856	1870
Adj Flow Rate, veh/h	15	57	38	642	0	123	29	184	0	97	136	8
Peak Hour Factor	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Percent Heavy Veh, %	2	2	4	2	3	2	2	2	2	2	3	2
Cap, veh/h	21	79	53	820	0	365	141	847		631	964	58
Arrive On Green	0.09	0.09	0.09	0.23	0.00	0.23	0.52	0.52	0.00	0.52	0.52	0.52
Sat Flow, veh/h	239	907	604	3563	0	1585	166	1622	1585	1043	1846	112
Grp Volume(v), veh/h	110	0	0	642	0	123	213	0	0	122	0	119
Grp Sat Flow(s),veh/h/ln	1750	0	0	1781	0	1585	1787	0	1585	1333	0	1668
Q Serve(g_s), s	4.6	0.0	0.0	12.7	0.0	4.9	0.0	0.0	0.0	0.0	0.0	2.8
Cycle Q Clear(g_c), s	4.6	0.0	0.0	12.7	0.0	4.9	4.6	0.0	0.0	2.7	0.0	2.8
Prop In Lane	0.14		0.35	1.00		1.00	0.14		1.00	0.80		0.07
Lane Grp Cap(c), veh/h	153	0	0	820	0	365	988	0		783	0	872
V/C Ratio(X)	0.72	0.00	0.00	0.78	0.00	0.34	0.22	0.00		0.16	0.00	0.14
Avail Cap(c_a), veh/h	467	0	0	950	0	423	988	0		783	0	872
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	0.00	0.00	1.00	0.00	1.00	1.00	0.00	0.00	1.00	0.00	1.00
Uniform Delay (d), s/veh	33.3	0.0	0.0	27.1	0.0	24.1	9.7	0.0	0.0	9.2	0.0	9.2
Incr Delay (d2), s/veh	12.7	0.0	0.0	4.9	0.0	1.2	0.5	0.0	0.0	0.4	0.0	0.3
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	2.4	0.0	0.0	5.6	0.0	1.8	1.8	0.0	0.0	1.0	0.0	1.0
Unsig. Movement Delay, s/veh												
LnGrp Delay(d), s/veh	46.0	0.0	0.0	32.0	0.0	25.2	10.2	0.0	0.0	9.6	0.0	9.5
LnGrp LOS	D			C		C	B			A		A
Approach Vol, veh/h	110			765			213			241		
Approach Delay, s/veh	46.0			30.9			10.2			9.6		
Approach LOS	D			C			B			A		
Timer - Assigned Phs	2			4			6			8		
Phs Duration (G+Y+Rc), s	43.2			10.6			43.2			21.3		
Change Period (Y+Rc), s	4.0			4.0			4.0			4.0		
Max Green Setting (Gmax), s	23.0			20.0			23.0			20.0		
Max Q Clear Time (g_c+I1), s	6.6			6.6			4.8			14.7		
Green Ext Time (p_c), s	1.8			0.7			2.3			2.6		

Intersection Summary

HCM 7th Control Delay, s/veh	25.0
HCM 7th LOS	C




Notes

User approved volume balancing among the lanes for turning movement.

Unsignalized Delay for [NBR] is excluded from calculations of the approach delay and intersection delay.

6: N Broadway & Gladstone Bowl Drive

Existing + Proposed Development PM Peak Hour

Intersection						
Int Delay, s/veh	0.6					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	13	9	301	8	10	219
Future Vol, veh/h	13	9	301	8	10	219
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	50	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	82	82	82	82	82	82
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	16	11	367	10	12	267
Major/Minor	Minor1	Major1		Major2		
Conflicting Flow All	530	372	0	0	377	0
Stage 1	372	-	-	-	-	-
Stage 2	158	-	-	-	-	-
Critical Hdwy	6.63	6.23	-	-	4.13	-
Critical Hdwy Stg 1	5.43	-	-	-	-	-
Critical Hdwy Stg 2	5.83	-	-	-	-	-
Follow-up Hdwy	3.519	3.319	-	-	2.219	-
Pot Cap-1 Maneuver	494	673	-	-	1180	-
Stage 1	696	-	-	-	-	-
Stage 2	855	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	489	673	-	-	1180	-
Mov Cap-2 Maneuver	489	-	-	-	-	-
Stage 1	696	-	-	-	-	-
Stage 2	846	-	-	-	-	-
Approach	WB	NB		SB		
HCM Control Delay, s/v11.87		0		0.43		
HCM LOS	B					
Minor Lane/Major Mvmt	NBT	NBRWBLn1		SBL	SBT	
Capacity (veh/h)	-	-	551	157	-	
HCM Lane V/C Ratio	-	-	0.049	0.01	-	
HCM Control Delay (s/veh)	-	-	11.9	8.1	0.1	
HCM Lane LOS	-	-	B	A	A	
HCM 95th %tile Q(veh)	-	-	0.2	0	-	

8: West Post Office Drive & 72nd Street

Existing + Proposed Development PM Peak Hour

Intersection												
Int Delay, s/veh	3.3											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕					↕	↕	
Traffic Vol, veh/h	6	24	0	16	29	24	0	0	0	25	0	5
Future Vol, veh/h	6	24	0	16	29	24	0	0	0	25	0	5
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	92	81	81	81	81	92	81	92	81	92	92	92
Heavy Vehicles, %	2	4	2	2	3	2	2	2	2	2	2	2
Mvmt Flow	7	30	0	20	36	26	0	0	0	27	0	5
Major/Minor	Major1			Major2			Minor2					
Conflicting Flow All	62	0	0	30	0	0				131	131	49
Stage 1	-	-	-	-	-	-				88	88	-
Stage 2	-	-	-	-	-	-				43	43	-
Critical Hdwy	4.12	-	-	4.12	-	-				6.42	6.52	6.22
Critical Hdwy Stg 1	-	-	-	-	-	-				5.42	5.52	-
Critical Hdwy Stg 2	-	-	-	-	-	-				5.42	5.52	-
Follow-up Hdwy	2.218	-	-	2.218	-	-				3.518	4.018	3.318
Pot Cap-1 Maneuver	1541	-	-	1583	-	-				863	760	1020
Stage 1	-	-	-	-	-	-				935	822	-
Stage 2	-	-	-	-	-	-				980	859	-
Platoon blocked, %		-	-		-	-						
Mov Cap-1 Maneuver	1541	-	-	1583	-	-				848	0	1020
Mov Cap-2 Maneuver	-	-	-	-	-	-				848	0	-
Stage 1	-	-	-	-	-	-				931	0	-
Stage 2	-	-	-	-	-	-				967	0	-
Approach	EB			WB			SB					
HCM Control Delay, s/v	1.33			1.77			9.25					
HCM LOS							A					
Minor Lane/Major Mvmt	EBL	EBT	EBR	WBL	WBT	WBR	SBLn1	SBLn2				
Capacity (veh/h)	325	-	-	402	-	-	848	1020				
HCM Lane V/C Ratio	0.004	-	-	0.012	-	-	0.032	0.005				
HCM Control Delay (s/veh)	7.3	0	-	7.3	0	-	9.4	8.5				
HCM Lane LOS	A	A	-	A	A	-	A	A				
HCM 95th %tile Q(veh)	0	-	-	0	-	-	0.1	0				

10: N Broadway & North Drive

Existing + Proposed Development PM Peak Hour

Intersection

Int Delay, s/veh 3.2

Movement	EBL	EBR	NBL	NBT	SBT	SBR
----------	-----	-----	-----	-----	-----	-----

Lane Configurations						
---------------------	---	---	--	---	---	--

Traffic Vol, veh/h	18	89	93	217	140	13
--------------------	----	----	----	-----	-----	----

Future Vol, veh/h	18	89	93	217	140	13
-------------------	----	----	----	-----	-----	----

Conflicting Peds, #/hr	0	0	0	0	0	0
------------------------	---	---	---	---	---	---

Sign Control	Stop	Stop	Free	Free	Free	Free
--------------	------	------	------	------	------	------

RT Channelized	-	None	-	None	-	None
----------------	---	------	---	------	---	------

Storage Length	-	-	-	-	-	-
----------------	---	---	---	---	---	---

Veh in Median Storage, #	0	-	-	0	0	-
--------------------------	---	---	---	---	---	---

Grade, %	0	-	-	0	0	-
----------	---	---	---	---	---	---

Peak Hour Factor	92	92	92	92	92	92
------------------	----	----	----	----	----	----

Heavy Vehicles, %	2	2	2	2	2	2
-------------------	---	---	---	---	---	---

Mvmt Flow	20	97	101	236	152	14
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Major/Minor	Minor2	Major1	Major2
-------------	--------	--------	--------

Conflicting Flow All	597	159	166	0	-	0
----------------------	-----	-----	-----	---	---	---

Stage 1	159	-	-	-	-	-
---------	-----	---	---	---	---	---

Stage 2	438	-	-	-	-	-
---------	-----	---	---	---	---	---

Critical Hdwy	6.42	6.22	4.12	-	-	-
---------------	------	------	------	---	---	---

Critical Hdwy Stg 1	5.42	-	-	-	-	-
---------------------	------	---	---	---	---	---

Critical Hdwy Stg 2	5.42	-	-	-	-	-
---------------------	------	---	---	---	---	---

Follow-up Hdwy	3.518	3.318	2.218	-	-	-
----------------	-------	-------	-------	---	---	---

Pot Cap-1 Maneuver	466	886	1412	-	-	-
--------------------	-----	-----	------	---	---	---

Stage 1	869	-	-	-	-	-
---------	-----	---	---	---	---	---

Stage 2	650	-	-	-	-	-
---------	-----	---	---	---	---	---

Platoon blocked, %				-	-	-
--------------------	--	--	--	---	---	---

Mov Cap-1 Maneuver	427	886	1412	-	-	-
--------------------	-----	-----	------	---	---	---

Mov Cap-2 Maneuver	427	-	-	-	-	-
--------------------	-----	---	---	---	---	---

Stage 1	798	-	-	-	-	-
---------	-----	---	---	---	---	---

Stage 2	650	-	-	-	-	-
---------	-----	---	---	---	---	---

Approach	EB	NB	SB
----------	----	----	----

HCM Control Delay, s/v10.28		2.32	0
-----------------------------	--	------	---

HCM LOS	B		
---------	---	--	--

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	EBLn2	SBT	SBR
-----------------------	-----	-----	-------	-------	-----	-----

Capacity (veh/h)	540	-	427	886	-	-
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HCM Lane V/C Ratio	0.072	-	0.046	0.109	-	-
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HCM Control Delay (s/veh)	7.7	0	13.8	9.6	-	-
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HCM Lane LOS	A	A	B	A	-	-
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HCM 95th %tile Q(veh)	0.2	-	0.1	0.4	-	-
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Drainage Report
For
400 NW 72nd Street
Gladstone, Missouri

April 01, 2024

By:
Gerald W. Menefee, PE
KAM Design LLC
9000 Bannister Road
Kansas City, Missouri 64134

menefeegerald@gmail.com



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Section 1 General

The proposed site for a new convenience store with gasoline pumps is just northwest corner of the intersection of N Broadway and NW 72nd Street in Gladstone, Missouri. The tract of land is currently covered by grassland. The developed portion of the site is expected to cover approximately the south two thirds of the site.

Section 2 Methodology

HydroCAD 10.00 was utilized for the drainage calculations developed for this project. The Water Quality solution was developed utilizing Manual of Best Management Practices for Stormwater Quality, October 2012 edition.

Section 3 Existing Drainage Patterns

From the peak elevation of the site located near the southeast corner of the site, there are three basins radiating out from it. Reference Maps Section. Basins E1 generally exhibits flow toward the west side of the property; Basin E2 drains to the east part of the property; while Basin E3 drains toward the west side of the site. Table 1 shows the amounts of existing runoff from each of the basins for the 1-year, 10-year and 100-year storms are as follows:

**Table 1
Existing Site Runoff**

Storm Year	Basin E1 (cfs)	Basin E2 (cfs)	Basin E3 (cfs)	Total Site (cfs)
1	0.66	0.03	1.53	2.22
10	2.04	0.08	4.62	6.74
100	3.65	0.15	8.24	12.04

Proposed Drainage Patterns Section 4

The proposed drainage patterns are consolidated into six basins. Reference the Maps Section. The north or 1P Basin allows for runoff to flow toward the north edge of the property and thence to the Bioretention Bed located to its immediate north. Basins 2P and 3P are much smaller basins

draining to the west. The Basin 4P Generally drains that portion of the east property. The P5 Basin is the water quality Bioretention Area and land immediately around. It drains excess runoff to the sites underground detention system. The area surrounding P5 is comprised of P6 land which is uncontrolled drainage to the west side of the property. A summary of the proposed runoff expected from the site for the 1-year, 10-year and 100-year storms are noted in Table 2. The calculated detention depth and storage are noted in Table 3 as follows:

Table 2
Proposed Site Runoff

Storm Year	Basin 1P (cfs)	Basin 1P And 5P w/ Detention (cfs)	Basin 2P (cfs)	Basin 3P (cfs)	Basin 4P (cfs)	Basin 5P (cfs)	Basin 6P (cfs)	Total Site w/ Detention (cfs)
1	4.33	1.70	0.01	0.01	0.27	0.23	0.23	2.06
10	8.53	5.20	0.03	0.03	0.82	0.70	0.61	5.38
100	12.83	8.78	0.06	0.06	1.45	1.23	1.23	10.81

Table 3
Detention Depth and Storage

Storm Year	Detained Depth (ft)	Detained Volume (ac-ft)
1	1.02	0.064
10	1.71	0.126
100	5.98	0.177

Table 4
Final Detention Volume Minus the WQv Volume

	Calculated Detention Volume	WQv Volume Stored	Final Detention Volume
Acre-Feet Volumes	0.211 ac-ft	0.081 ac-ft	0.13 ac- ft
Linear Feet of Pipe	1300.00 Lf	499.00 Lf	801.00 Lf

As a part of this analysis, it was assumed that the outflow pipe of the detention basin would consist of a 12-inch diameter PVC pipe. As can be seen in the Tables 1 that at all storm levels

the 12-inch PVC pipe provides an adequate release of water so that the discharge in the post developed situation results in the sites runoff being less than the existing runoff.

As for an emergency spillover, it shall be incorporated as a part of the discharge of the 12-inch PVC pipe. The pipe can handle the excess flow by allowing the water in the inlet structure to exceed the height of the orifice plate and travel down through the 12-inch discharge pipe.

The total detention utilized for the site incorporates a reduction in volume. See Table 4. This reduction is predicated on the assumption that the runoff stored in the Bioretention area is effectively detained water and therefore extra volume was left in the detention system pipes.

Section 5 Water Quality

Water quality goals for the site will be achieved through the use Bioretention Area. The area is located to immediate north of drainage basin P1. Runoff water will fill the Area with runoff to a depth of 1 foot. Once this volume is achieved, excess water over the maximum depth of the subsurface storage area flows in an into an inlet structure located at the southwest portion of the Area corner of the property and then into the detention piping.

Water in the Bioretention Area is to drain down the through a 3- inch cover of hardwood wood chips and thence through a 4-foot-thick layer of porous soil. Runoff will be removed from the Area utilizing a system of perforated 4-inch PVC pipes to allow water to leave and travel to a point of daylight. The Area is constructed to allow for the minimum drawdown of one foot per day.

Section 6 Summary

The proposed new improvements on will increase impervious cover necessitating the need for a detention facility to control the additional runoff generated. Since there is insufficient area to construct a detention pond on the surface, it was determined that a subsurface pipe system should be constructed on the north side of the developed portion of the site. A bio retention pond is too be constructed just before the runoff is directed to the detention system in order to allow for the treatment of the first flush of rain water.

Section 7

Conclusions and Recommendations

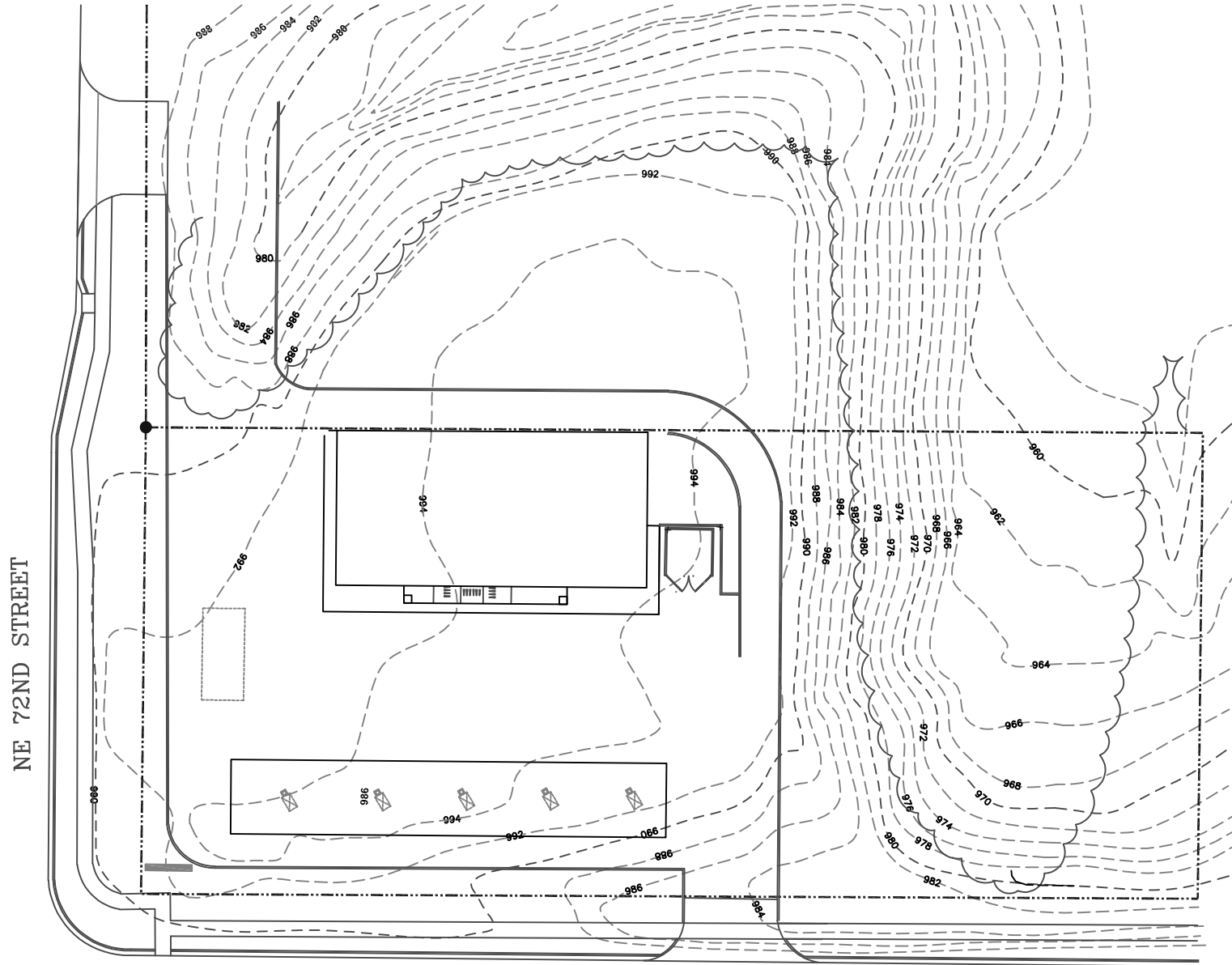
Based upon review of the site involving existing and proposed conditions, conclusions and recommendations are provided as follows:

1. Installation of the Bioretention Area will increase the quality of water exiting the site by filtering water leaving the proposed parking areas.
2. Detention will be provided to mitigate the increasing runoff due to the additional impervious cover added to the site.
3. The detention volume was reduced by the storage volume of the water quality storage. Since not doing this would result in the site being penalized by the extra water stored in the water quality structure.
4. Over flow runoff will be incorporated within the discharge piping of the detention control structure.

Section 8
Drainage Area Maps

SHORT STOP GAS STATION

400 N 72ND STREET, GLADSTONE, MISSOURI



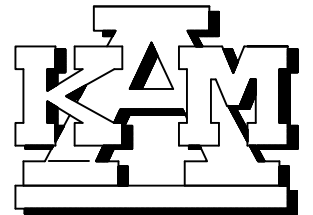
LEGEND

EXISTING CONTOURS

N BROADWAY

EXISTING DRAINAGE AREA MAP

SCALE 1" = 50'



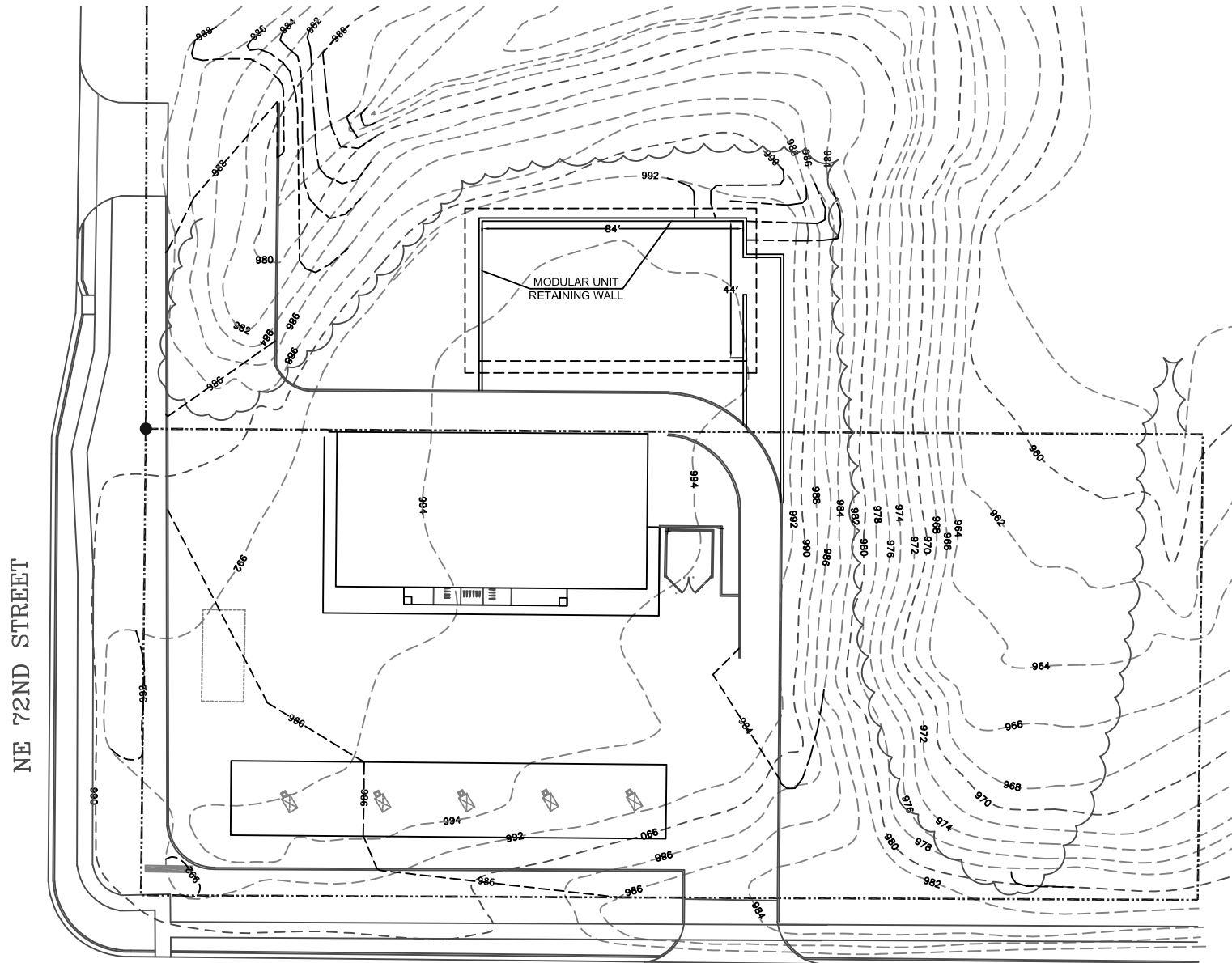
Design Group LLC.

9264 Blue Ridge Blvd.
Suite A

Kansas City, Missouri 64138
(816) 797-2065

SHORT STOP GAS STATION

400 N 72ND STREET, GLADSTONE, MISSOURI



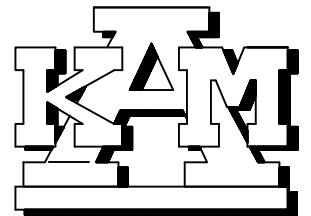
LEGEND

- EXISTING CONTOURS
- PROPOSED CONTOURS

N BROADWAY

PROPOSED DRAINAGE AREA MAP

SCALE 1' = 50'



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Section 9

Supporting Calculations

Exhibit 1

Water Quality Equations

$$WQ_v = P \cdot R_v \cdot A / 12$$

$$P = 1.37$$

$$I = 68 \%$$

$$R_v = 0.05 + 0.009 \cdot I = 0.05 + 0.009 \cdot 68 =$$

$$A = 0.87$$

$$= 1.37 \cdot 0.62 \cdot 0.87 / 12 = 0.062 \text{ a-ft} = 2665.87 \text{ cf}$$

Refer to Bioretention Worksheet that follows:

Design Procedure Form: Bioretention
Main Worksheet

Designer: GERALD MENEZES
Checked By: GERALD MENEZES
Company: KAM DESIGN LLC
Date: 2/21/23
Project: SHORE STOP GAS STATION
Location: 400 NW 72ND STREET

I. Water Quality Volume

Step 1) Tributary area to bioretention area, A_T (ac)

A_T (ac) = 1.207

Step 2) Calculate WQv using methodology in Section 6

WQv (cu-ft) = 0.91

Ila. Pretreatment

Step 1) Specify type of inflow to Bioretention facility:

Type 1 = sheet flow

Type 2 = concentrated or channelized

Inflow type = TYPE 1

Step 2) Pretreatment

Step 3) Proceed to Part IIb, IIc, or IId for design guidance on different pretreatment options

IIb. Vegetated Pretreatment Strip

Step 1) Type of land cover of contributing area:

Type 1 = Impervious (i.e., parking lot)

Type 2 = Pervious (i.e., residential lawn)

Land cover type = TYPE 1

Step 2) Maximum inflow approach length, L_{approach} (ft)

L_{approach} (ft) = 30

Step 3) Average slope of pretreatment strip, S_{fs} (%)

(Maximum slope of 6%)

S_{fs} (%) = 2%

Step 4) Vegetated pretreatment strip minimum length, L_{fs} (ft), from Table 8.2

L_{fs} (ft) = 30

IIc. Vegetated Pretreatment Channel

Step 1) Percent imperviousness of contributing area, % imp

% imp = 68

Step 2) Average slope of vegetated channel, S_{vc} (%)

(Maximum slope of 6%)

S_{vc} (%) = 2%

Step 3) Vegetated pretreatment channel minimum length, L_{vc} (ft), from Table 8.3

L_{vc} (ft) = 30

IId. Other Pretreatment Devices

Other methods of pretreatment may be utilized upstream of a bioretention facility to settle out suspended solids and reduce runoff velocity. Several proprietary devices are available that will achieve these results. Most such devices install below ground and accept inflow from a piped stormwater management system or from surface sheet flow via drop inlets. These devices should be selected and sized based on site-specific conditions for each project.

Design Procedure Form: Bioretention
Main Worksheet

Designer: GERALD MENERES
Checked By: GERALD MENERES
Company: KAM DESIGN LLC
Date: 7/21/23
Project: SHORT STOP GAS STATION
Location: 400 NW 72ND STREET

III. Planting Soil Bed and Ponding Area

- Step 1) Planting bed soil depth, d_f (ft)
(d_f should be between 2.5 feet and 4 feet). d_f (ft) = 4
- Step 2) Coefficient of permeability for planting soil bed, k (ft/day)
(k should be at least 1 ft/day) k (ft/day) = 1
- Step 3) Maximum ponding depth, h_{max} (ft)
(h_{max} should be between 0.25 ft and 1.0 ft). h_{max} (ft) = 1
- Step 4) Average height of water above bioretention bed, h_{avg} (ft)
 $h_{avg} = h_{max}/2$ h_{avg} (ft) = 0.5
- Step 5) Time required for WQv to filter through the planting soil bed, t_f (days)
(t_f of 1 to 3 days is recommended) t_f (days) = 1
- Step 6) Required filter bed surface area, A_f (ft²)
 $A_f = (WQv * d_f) / [k * t_f * (h_{avg} + d_f)]$ A_f (ft²) = 2370
- Step 7) Approximate filter bed length, L_f (ft), assuming a length to width ratio of 2:1
(L_f should be at least 40 ft) L_f (ft) = 84
- Step 8) Approximate filter bed width, W_f (ft), assuming a length to width ratio of 2:1
(W_f should be at least 15 feet, and optimally half of L_f) W_f (ft) = 42
- Step 9) Required Ponding Area, A_p (sf)
 $A_p = WQv / h_{max}$ A_p (ft²) = 266.00

Design Procedure Form: Bioretention
Main Worksheet

Designer: GERALD MONEPREG
 Checked By: GERALD MONEPREG
 Company: KAM DESIGN LLC
 Date: 7/21/23
 Project: SHORT STOP GAS STATION
 Location: 400 NW 72ND STREET

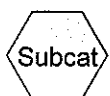
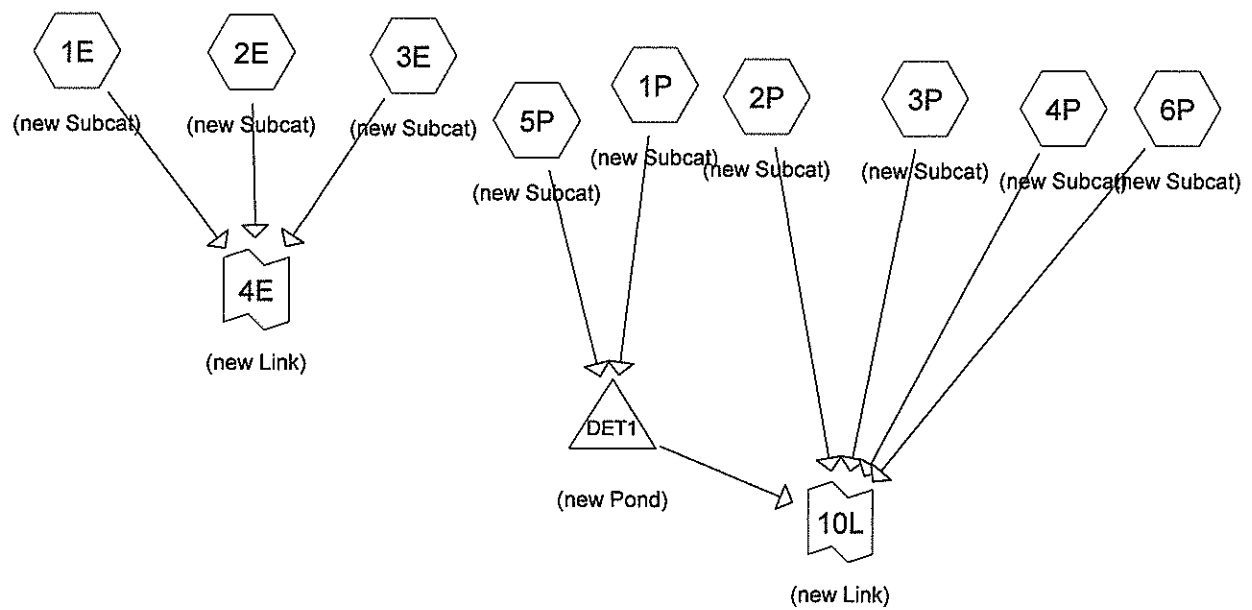
IV. Underdrain

Step 1) Underdrain pipe diameter, D_U (in) (D_U should be at least 4 inches)	D_U (in) = <u>4</u>
Step 2) Depth of gravel blanket, Z_{gravel} (in.) (Z_{gravel} should be at least 8 inches, and at least 2 inches greater than D_U)	Z_{gravel} (in) = <u>12</u>
Step 3) Set underdrain perforation diameters to 0.375 inches.	D_{perf} (in) = <u>0.375</u>
Step 4) Longitudinal center-to-center underdrain perforation spacing, S_{perf} (in)	S_{perf} (in) = <u>14</u>
Step 5) Number of perforations per row (around circumference of underdrain), n_{perf} (n_{perf} should be at least 4)	n_{perf} = <u>4</u>
Step 6) Underdrain collector spacing (approximately 20') S_U (ft)	S_U (ft) = <u>14</u>
Step 7) Pipe grade, G_{pipe} (%), for main pipe and transverse collector pipes (G_{pipe} should be at least 0.5%)	G_{pipe} (%) = <u>0</u>
Step 8) Providing at least one cleanout per pipe run? (Yes or No)	<u>YES</u>
Step 9) Determine design head (h_o) on orifice, $h_o = (d_f + h_{max})/2$	h_o (ft) = <u>2.5</u>
Step 10) Determine Average flow rate, $Q_{avg} = WQ_v/144,000$	Q_{avg} (cfs) = <u>0.019</u>
Step 11) Determine orifice area $A_o = Q_{avg}/(0.6 \cdot (2 \cdot g \cdot h_o)^{0.5})$	A_o (ft ²) = <u>0.0025</u> A_o (in ²) = <u>0.36</u>

V. Overflow

The bioretention overflow shall be designed to safely pass runoff flows from events up to and including the 1 percent event unless the facility is designed with a bypass around the facility for larger storm events. If the 1-percent event is to pass through the facility, the maximum velocity shall be kept below 3 feet per second to avoid erosion of the soil matrix. If facilities are designed with a bypass, it shall be designed to safely pass runoff flows from events up to and including the 1 percent event. The overflow shall be designed as a vegetated or stabilized channel of a yard inlet catch basin. Vegetated or stabilized channels shall be designed using one of the methods presented in APWA Section 5603 and shall conform to the design criteria presented in APWA Section 5607. Methods presented in APWA Section 5604 shall be used for inlet design.

Exhibit 2
1-Year Storm Calculations



Subcat



Reach



Pond



Link

Routing Diagram for 400 NW 72 Street

Prepared by HP, Printed 7/21/2023

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Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
2.354	74	>75% Grass cover, Good, HSG C (1E, 1P, 2E, 2P, 3E, 3P, 4P, 5P, 6P)
0.874	98	Paved parking, HSG C (1P)
3.228	80	TOTAL AREA

Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
3.228	HSG C	1E, 1P, 2E, 2P, 3E, 3P, 4P, 5P, 6P
0.000	HSG D	
0.000	Other	
3.228		TOTAL AREA

400 NW 72 Street

Prepared by HP

Printed 7/21/2023

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Page 4

Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	2.354	0.000	0.000	2.354	>75% Grass cover, Good	1E, 1P, 2E, 2P, 3E, 3P, 4P, 5P, 6P
0.000	0.000	0.874	0.000	0.000	0.874	Paved parking	1P
0.000	0.000	3.228	0.000	0.000	3.228	TOTAL AREA	

Time span=2.00-30.00 hrs, dt=0.05 hrs, 561 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1E: (new Subcat)	Runoff Area=0.544 ac 0.00% Impervious Runoff Depth=0.85"
	Flow Length=81' Slope=0.0247 '/' Tc=10.6 min CN=74 Runoff=0.66 cfs 0.038 af
Subcatchment 1P: (new Subcat)	Runoff Area=1.145 ac 76.33% Impervious Runoff Depth=2.07"
	Flow Length=249' Tc=2.8 min CN=92 Runoff=4.33 cfs 0.197 af
Subcatchment 2E: (new Subcat)	Runoff Area=0.017 ac 0.00% Impervious Runoff Depth=0.85"
	Flow Length=30' Slope=0.0732 '/' Tc=3.1 min CN=74 Runoff=0.03 cfs 0.001 af
Subcatchment 2P: (new Subcat)	Runoff Area=0.007 ac 0.00% Impervious Runoff Depth=0.85"
	Flow Length=33' Slope=0.0758 '/' Tc=3.3 min CN=74 Runoff=0.01 cfs 0.000 af
Subcatchment 3E: (new Subcat)	Runoff Area=1.053 ac 0.00% Impervious Runoff Depth=0.85"
	Flow Length=237' Tc=5.8 min CN=74 Runoff=1.53 cfs 0.074 af
Subcatchment 3P: (new Subcat)	Runoff Area=0.007 ac 0.00% Impervious Runoff Depth=0.85"
	Flow Length=43' Slope=0.5116 '/' Tc=1.9 min CN=74 Runoff=0.01 cfs 0.000 af
Subcatchment 4P: (new Subcat)	Runoff Area=0.167 ac 0.00% Impervious Runoff Depth=0.85"
	Flow Length=83' Tc=2.6 min CN=74 Runoff=0.27 cfs 0.012 af
Subcatchment 5P: (new Subcat)	Runoff Area=0.142 ac 0.00% Impervious Runoff Depth=0.85"
	Flow Length=13' Slope=0.0176 '/' Tc=2.8 min CN=74 Runoff=0.23 cfs 0.010 af
Subcatchment 6P: (new Subcat)	Runoff Area=0.146 ac 0.00% Impervious Runoff Depth=0.85"
	Flow Length=222' Tc=7.5 min CN=74 Runoff=0.20 cfs 0.010 af
Pond DET1: (new Pond)	Peak Elev=983.05' Storage=0.064 af Inflow=4.56 cfs 0.207 af
	Outflow=1.70 cfs 0.207 af
Link 4E: (new Link)	Inflow=2.13 cfs 0.114 af
	Primary=2.13 cfs 0.114 af
Link 10L: (new Link)	Inflow=2.06 cfs 0.230 af
	Primary=2.06 cfs 0.230 af
Total Runoff Area = 3.228 ac Runoff Volume = 0.344 af Average Runoff Depth = 1.28"	
72.92% Pervious = 2.354 ac 27.08% Impervious = 0.874 ac	

Summary for Subcatchment 1E: (new Subcat)

Runoff = 0.66 cfs @ 12.04 hrs, Volume= 0.038 af, Depth= 0.85"

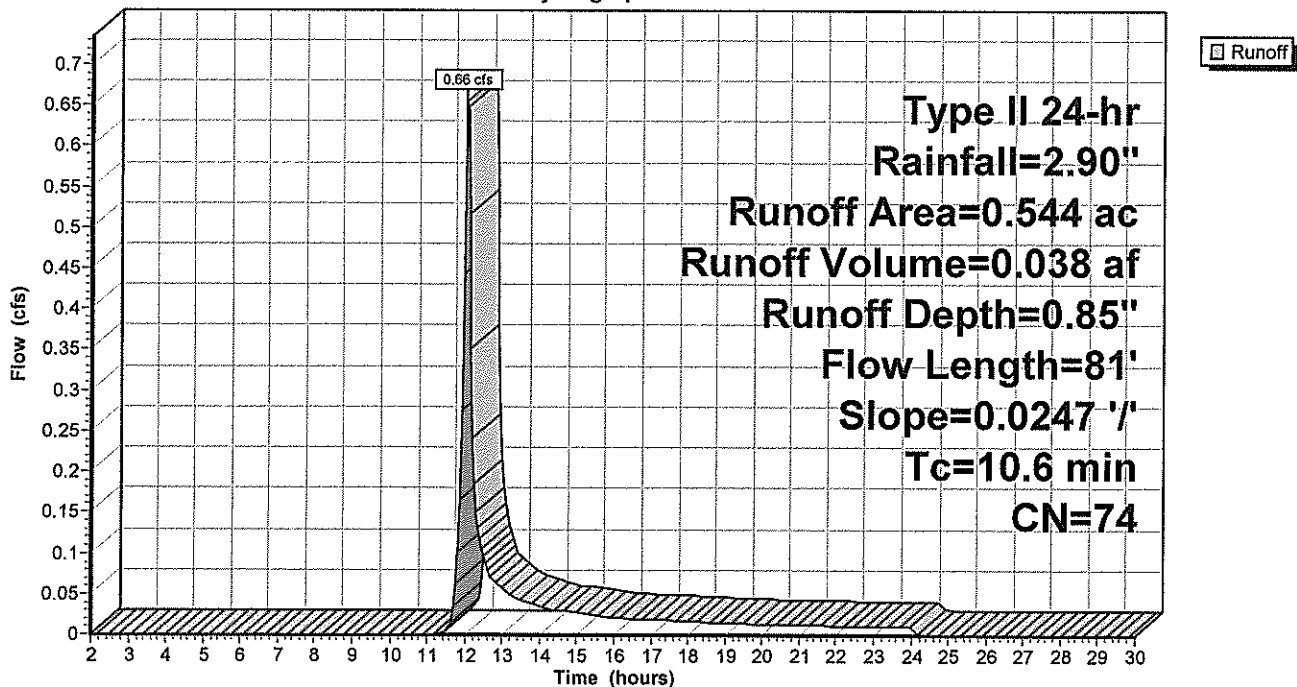
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs
Type II 24-hr Rainfall=2.90"

Area (ac)	CN	Description
0.544	74	>75% Grass cover, Good, HSG C
0.544		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.6	81	0.0247	0.13		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 1E: (new Subcat)

Hydrograph



Summary for Subcatchment 1P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 4.33 cfs @ 11.93 hrs, Volume= 0.197 af, Depth= 2.07"

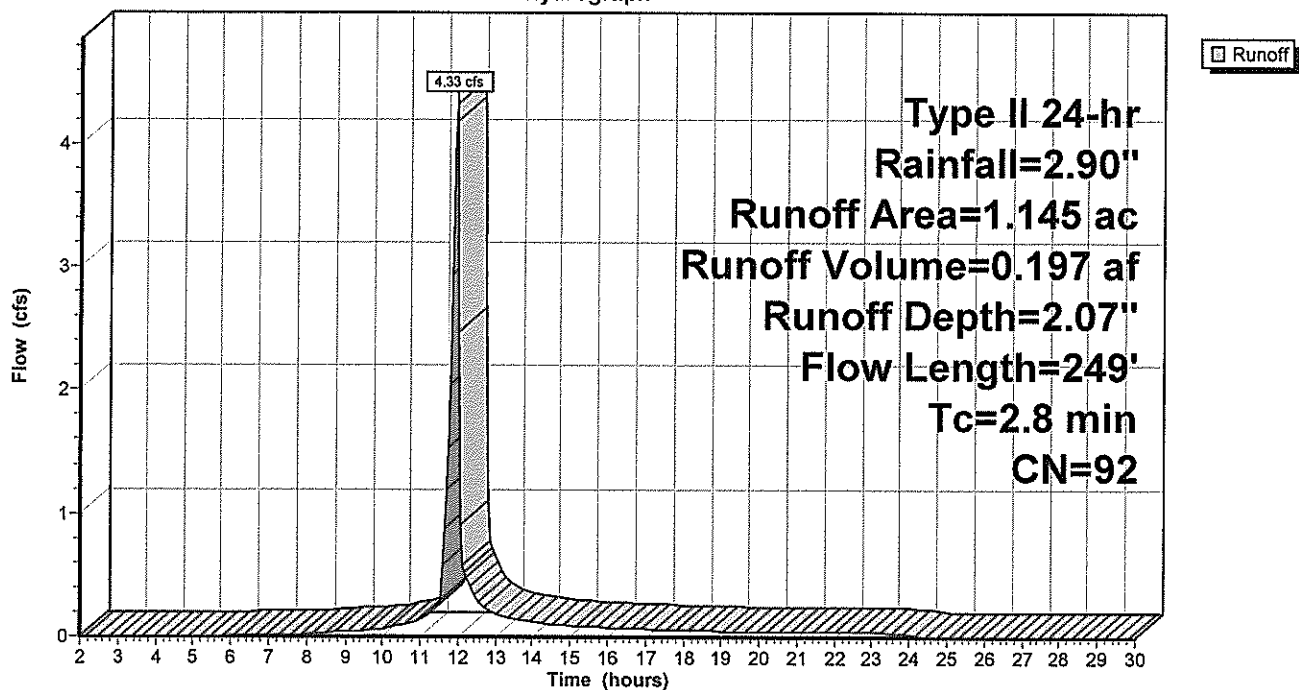
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=2.90"

Area (ac)	CN	Description
0.271	74	>75% Grass cover, Good, HSG C
0.874	98	Paved parking, HSG C
1.145	92	Weighted Average
0.271		23.67% Pervious Area
0.874		76.33% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0065	0.92		Sheet Flow, Smooth surfaces n= 0.011 P2= 3.50"
1.0	149	0.0151	2.49		Shallow Concentrated Flow, Paved Kv= 20.3 fps
2.8	249	Total			

Subcatchment 1P: (new Subcat)

Hydrograph



Summary for Subcatchment 2E: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.03 cfs @ 11.94 hrs, Volume= 0.001 af, Depth= 0.85"

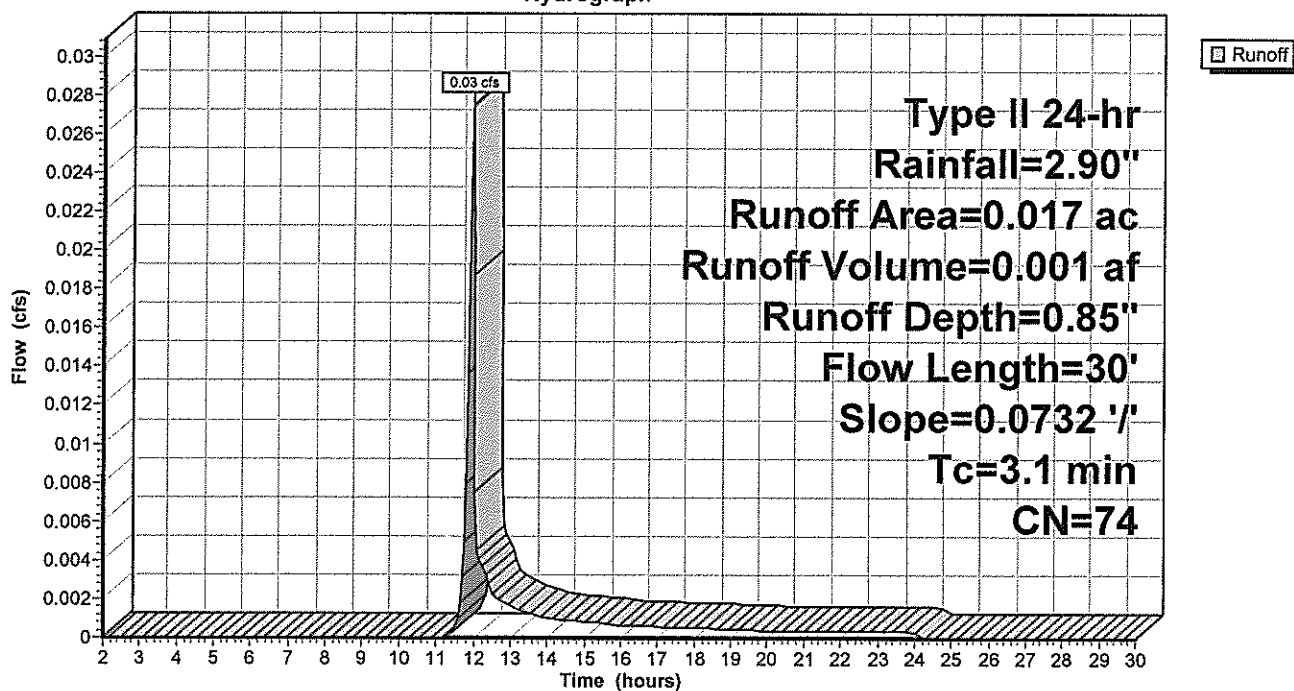
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=2.90"

Area (ac)	CN	Description
0.017	74	>75% Grass cover, Good, HSG C
0.017		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	30	0.0732	0.16		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 2E: (new Subcat)

Hydrograph



Summary for Subcatchment 2P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.01 cfs @ 11.95 hrs, Volume= 0.000 af, Depth= 0.85"

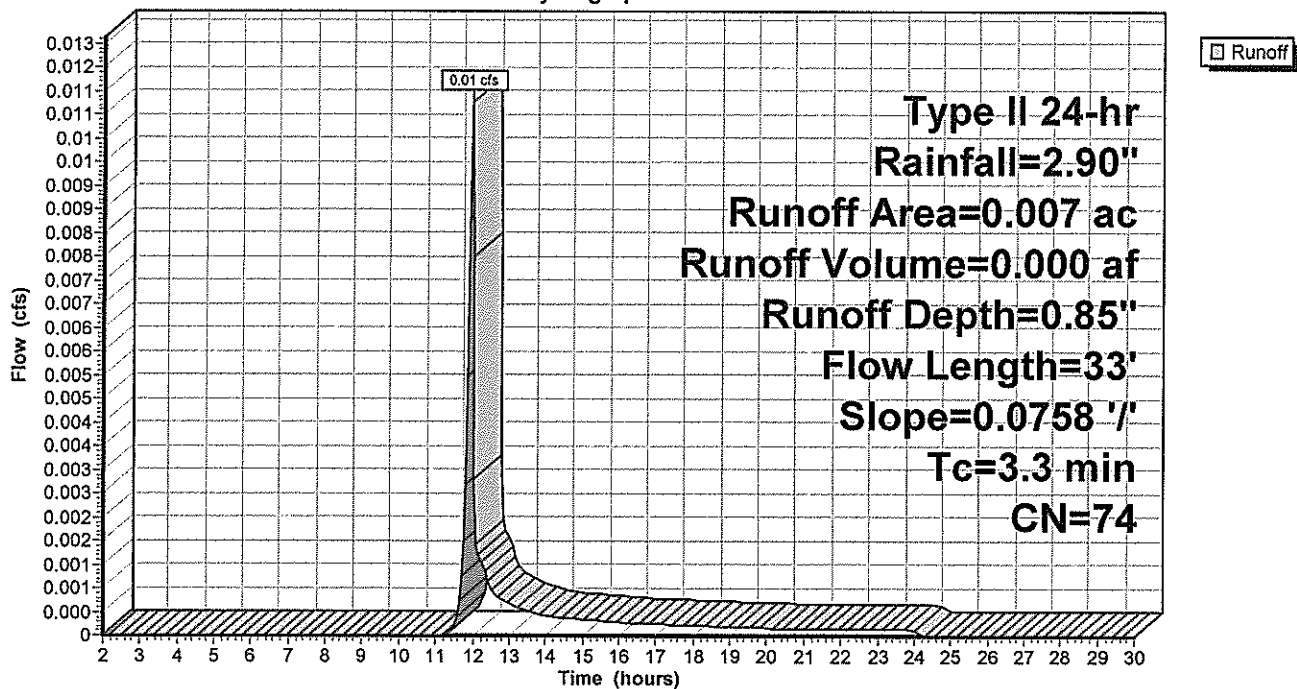
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=2.90"

Area (ac)	CN	Description
0.007	74	>75% Grass cover, Good, HSG C
0.007		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	33	0.0758	0.17		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 2P: (new Subcat)

Hydrograph



Summary for Subcatchment 3E: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 1.53 cfs @ 11.98 hrs, Volume= 0.074 af, Depth= 0.85"

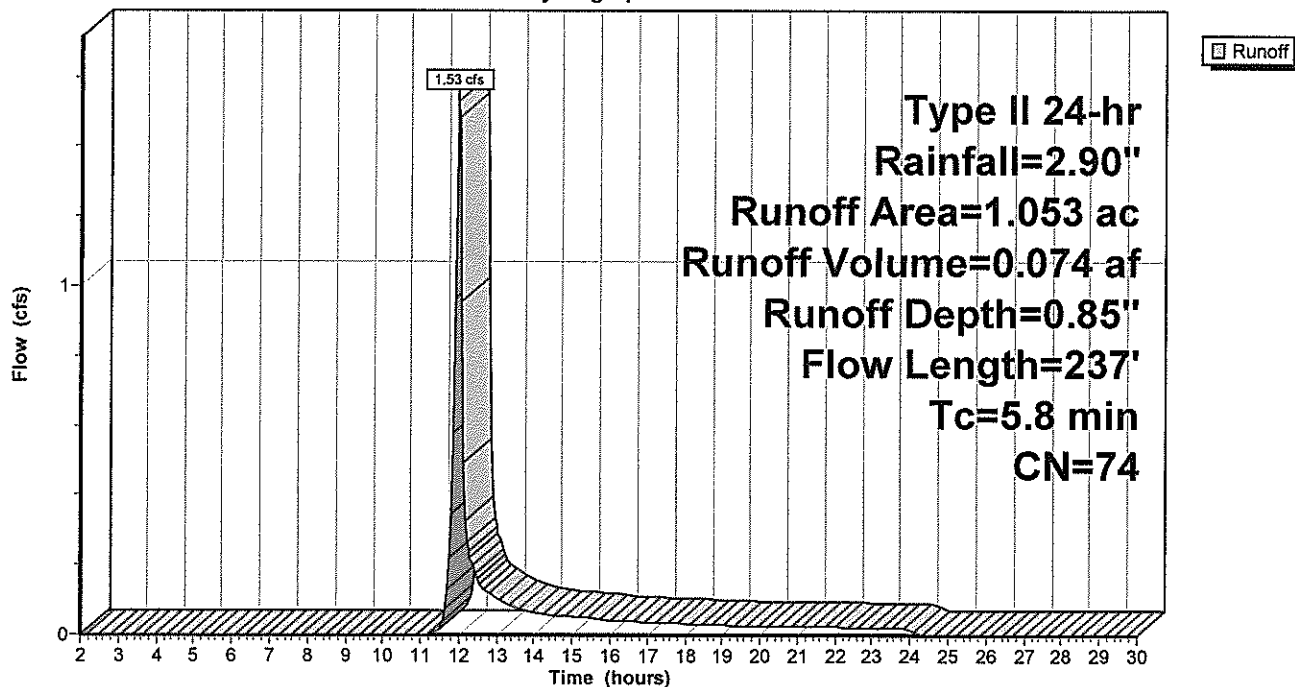
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=2.90"

Area (ac)	CN	Description
1.053	74	>75% Grass cover, Good, HSG C
1.053		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.4	100	0.2000	0.31		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$
0.4	137	0.1339	5.49		Shallow Concentrated Flow, Grassed Waterway $K_v=15.0$ fps
5.8	237	Total			

Subcatchment 3E: (new Subcat)

Hydrograph



Summary for Subcatchment 3P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.01 cfs @ 11.93 hrs, Volume= 0.000 af, Depth= 0.85"

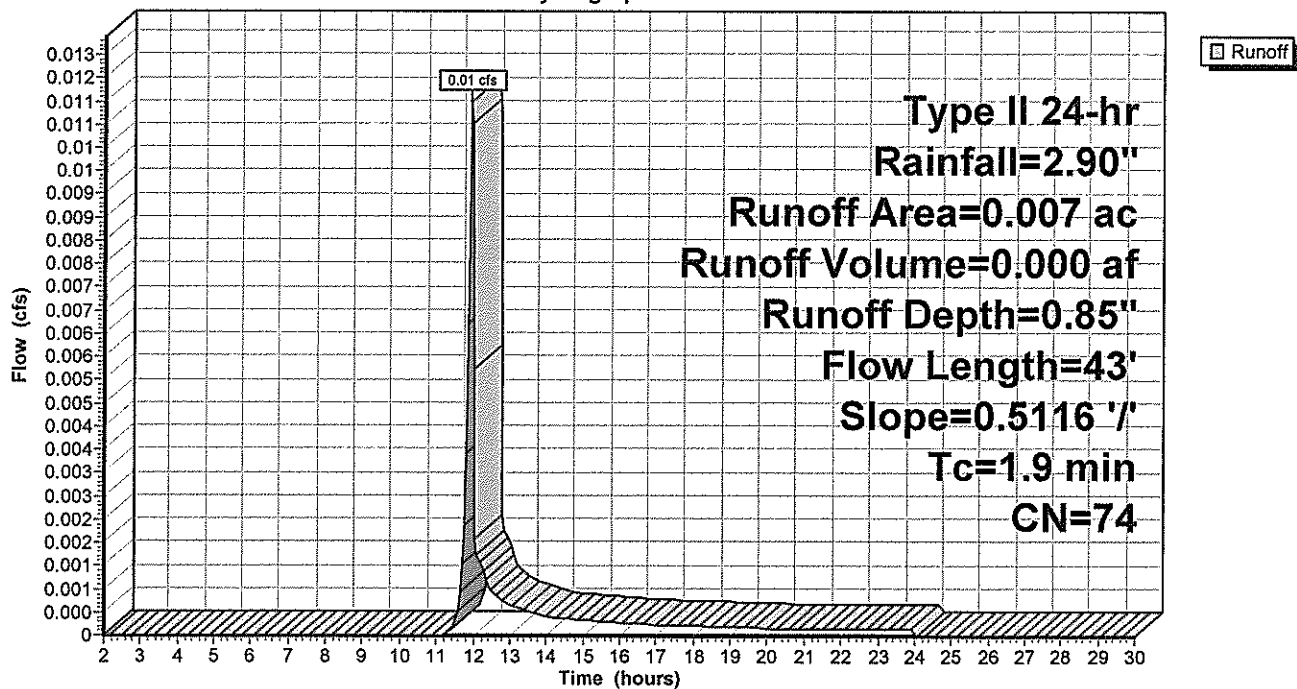
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=2.90"

Area (ac)	CN	Description
0.007	74	>75% Grass cover, Good, HSG C
0.007		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	43	0.5116	0.38		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 3P: (new Subcat)

Hydrograph



Summary for Subcatchment 4P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.27 cfs @ 11.94 hrs, Volume= 0.012 af, Depth= 0.85"

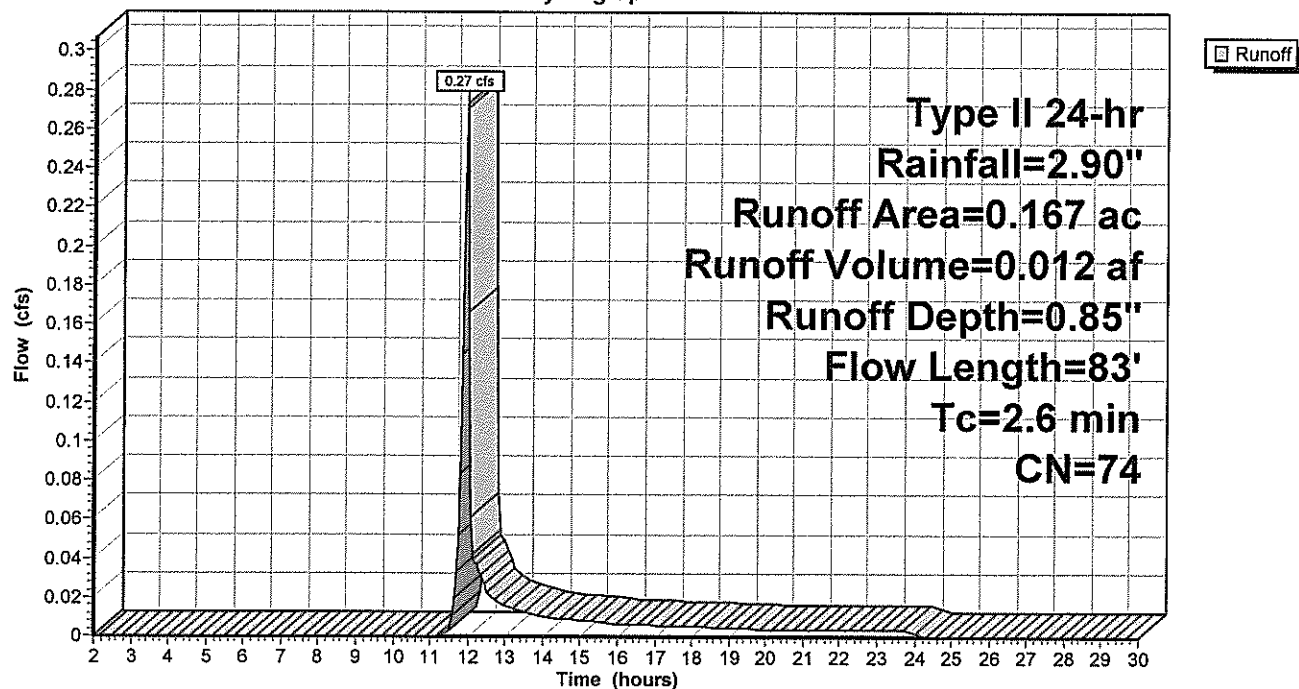
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=2.90"

Area (ac)	CN	Description
0.167	74	>75% Grass cover, Good, HSG C
0.167		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	30	0.1453	0.21		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$
0.2	53	0.0967	5.01		Shallow Concentrated Flow, Unpaved $K_v=16.1$ fps
2.6	83	Total			

Subcatchment 4P: (new Subcat)

Hydrograph



Summary for Subcatchment 5P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.23 cfs @ 11.94 hrs, Volume= 0.010 af, Depth= 0.85"

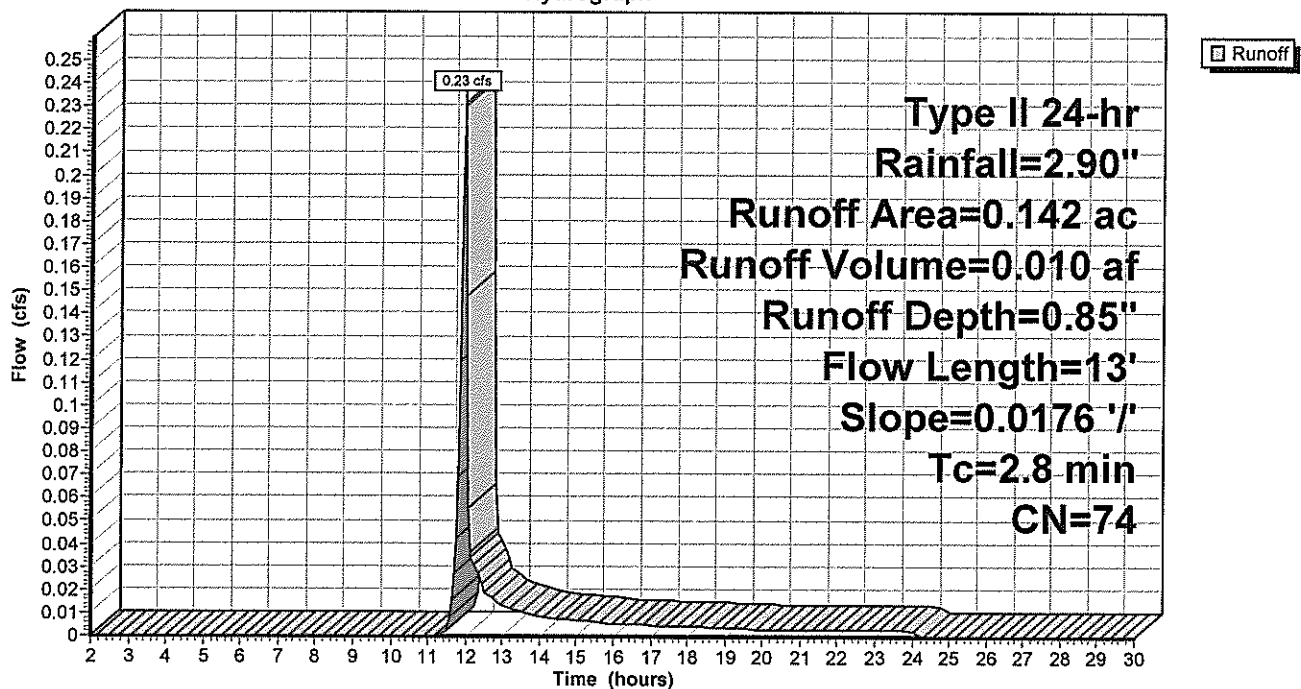
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=2.90"

Area (ac)	CN	Description
0.142	74	>75% Grass cover, Good, HSG C
0.142		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.8	13	0.0176	0.08		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$

Subcatchment 5P: (new Subcat)

Hydrograph



Summary for Subcatchment 6P: (new Subcat)

Runoff = 0.20 cfs @ 12.00 hrs, Volume= 0.010 af, Depth= 0.85"

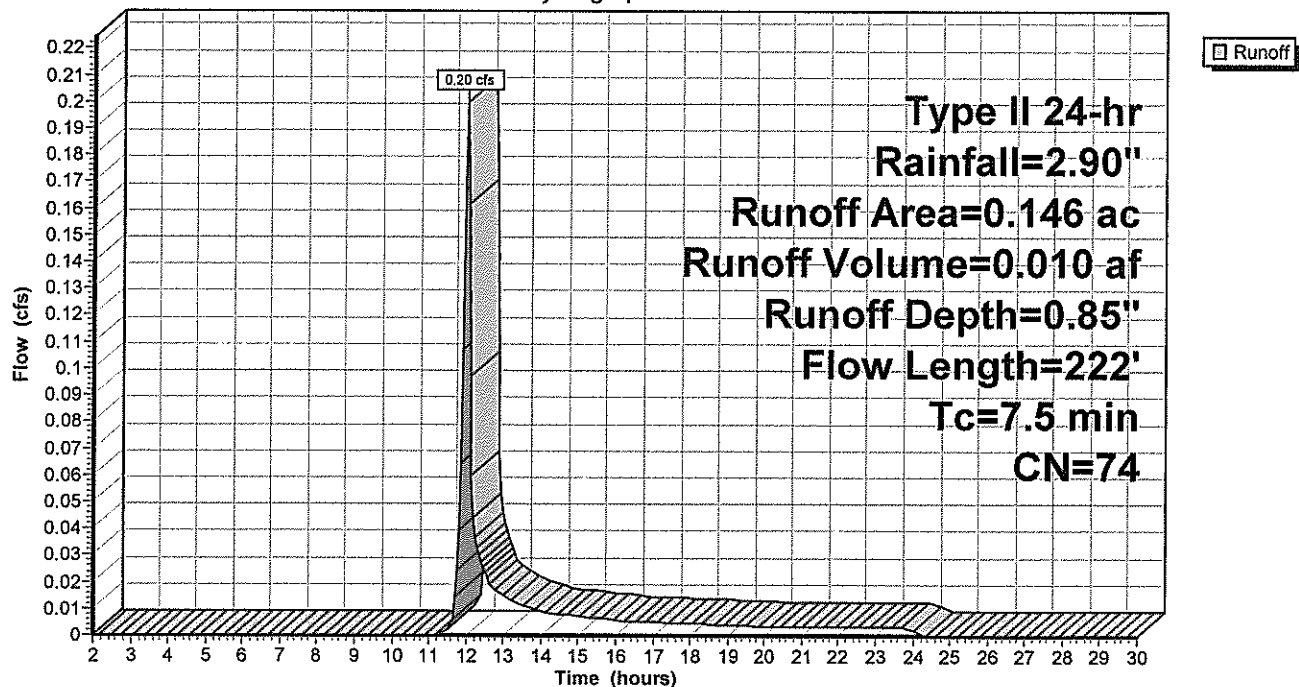
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs
Type II 24-hr Rainfall=2.90"

Area (ac)	CN	Description
0.146	74	>75% Grass cover, Good, HSG C
0.146		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.9	60	0.0400	0.15		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"
0.6	162	0.0775	4.18		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
7.5	222	Total			

Subcatchment 6P: (new Subcat)

Hydrograph



Summary for Pond DET1: (new Pond)

Inflow Area = 1.287 ac, 67.91% Impervious, Inflow Depth = 1.93"
 Inflow = 4.56 cfs @ 11.93 hrs, Volume= 0.207 af
 Outflow = 1.70 cfs @ 12.03 hrs, Volume= 0.207 af, Atten= 63%, Lag= 6.0 min
 Primary = 1.70 cfs @ 12.03 hrs, Volume= 0.207 af

Routing by Stor-Ind method, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs
 Peak Elev= 983.05' @ 12.03 hrs Surf.Area= 0.085 ac Storage= 0.064 af

Plug-Flow detention time= 29.3 min calculated for 0.207 af (100% of inflow)
 Center-of-Mass det. time= 29.1 min (827.6 - 798.5)

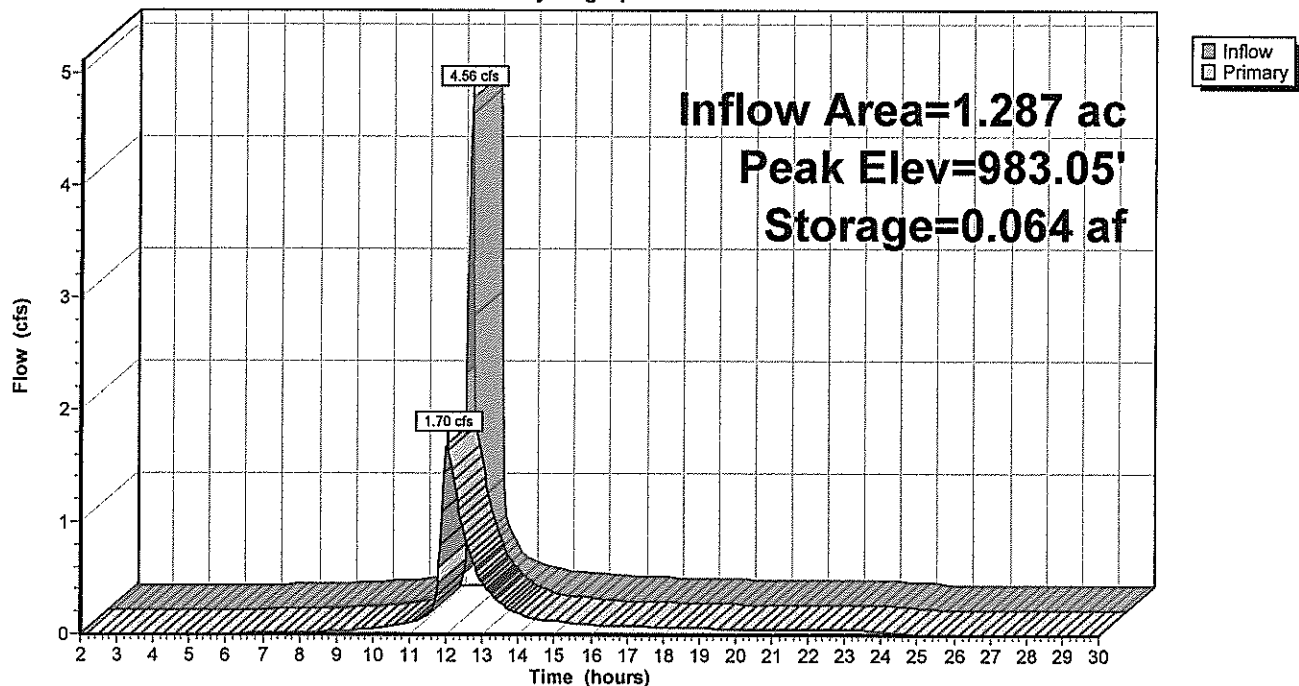
Volume	Invert	Avail.Storage	Storage Description
#1	982.03'	0.211 af	36.0" Round Pipe Storage L= 1,300.0'

Device	Routing	Invert	Outlet Devices
#1	Primary	982.03'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28) Head (feet) 0.00 1.03 1.03 1.93 1.93 3.00 Width (feet) 0.50 0.50 0.79 0.79 2.50 2.50

Primary OutFlow Max=1.68 cfs @ 12.03 hrs HW=983.05' (Free Discharge)
 ←1=Custom Weir/Orifice (Weir Controls 1.68 cfs @ 3.31 fps)

Pond DET1: (new Pond)

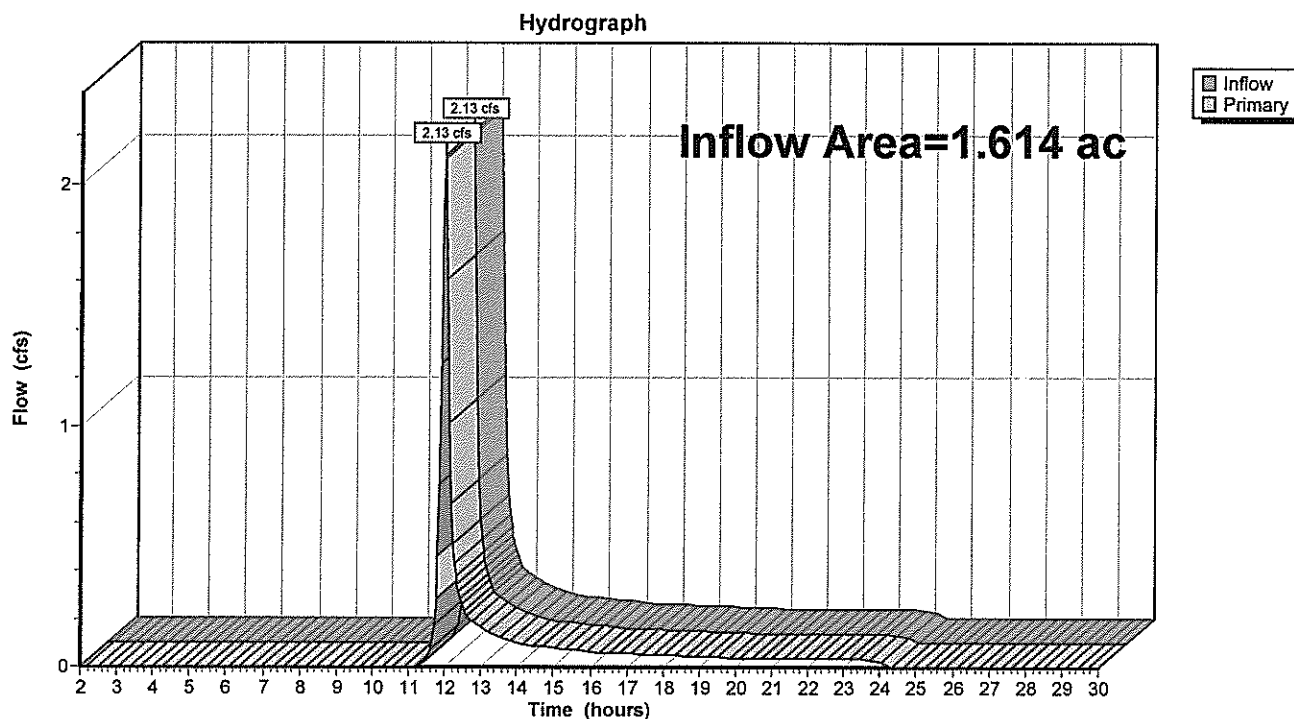
Hydrograph



Summary for Link 4E: (new Link)

Inflow Area = 1.614 ac, 0.00% Impervious, Inflow Depth = 0.85"
Inflow = 2.13 cfs @ 11.99 hrs, Volume= 0.114 af
Primary = 2.13 cfs @ 11.99 hrs, Volume= 0.114 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs

Link 4E: (new Link)

Summary for Link 10L: (new Link)

Inflow Area = 1.614 ac, 54.15% Impervious, Inflow Depth = 1.71"
Inflow = 2.06 cfs @ 12.00 hrs, Volume= 0.230 af
Primary = 2.06 cfs @ 12.00 hrs, Volume= 0.230 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs

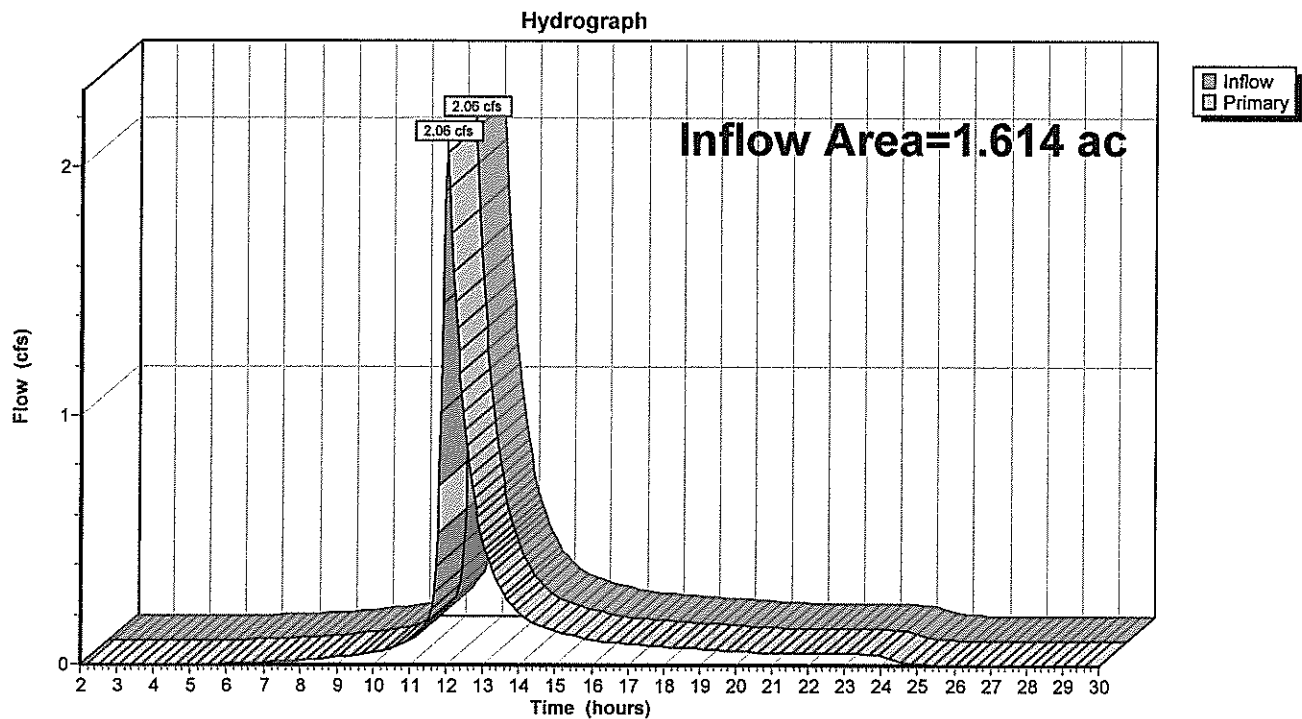
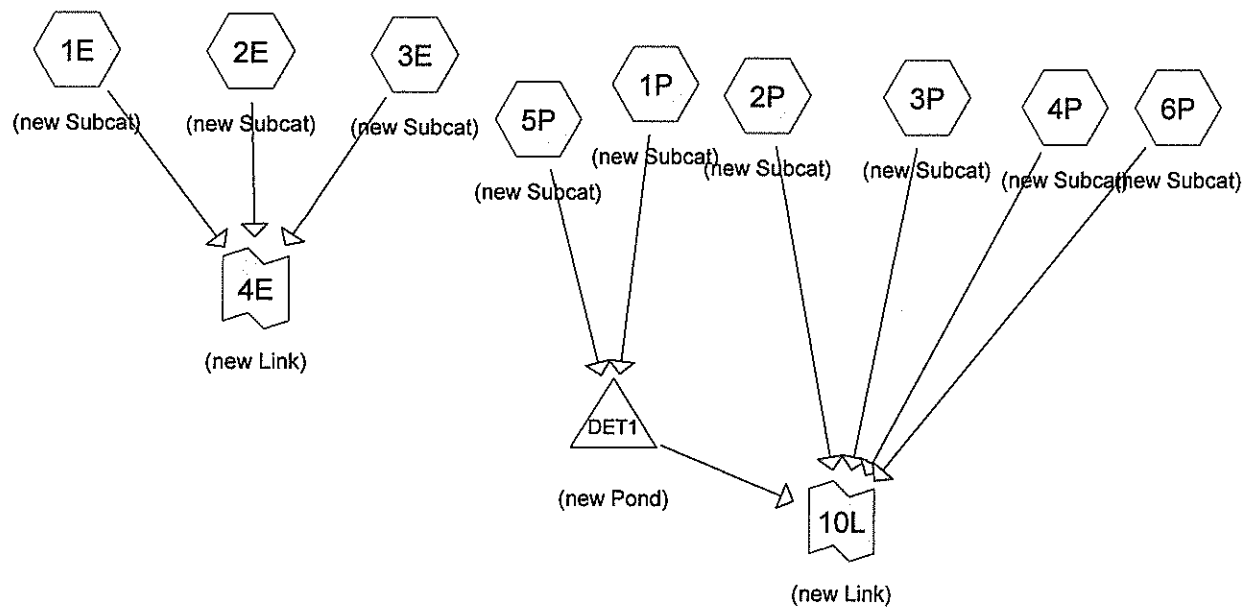
Link 10L: (new Link)

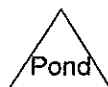
Exhibit 3
10-year Storm Calculations



Subcat



Reach



Pond



Link

Routing Diagram for 400 NW 72 Street

Prepared by HP, Printed 7/20/2023

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400 NW 72 Street

Prepared by HP

Printed 7/20/2023

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Page 2

Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
2.354	74	>75% Grass cover, Good, HSG C (1E, 1P, 2E, 2P, 3E, 3P, 4P, 5P, 6P)
0.874	98	Paved parking, HSG C (1P)
3.228	80	TOTAL AREA

Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
3.228	HSG C	1E, 1P, 2E, 2P, 3E, 3P, 4P, 5P, 6P
0.000	HSG D	
0.000	Other	
3.228		TOTAL AREA

400 NW 72 Street

Prepared by HP

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Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	2.354	0.000	0.000	2.354	>75% Grass cover, Good	1E, 1P, 2E, 2P, 3E, 3P, 4P, 5P, 6P
0.000	0.000	0.874	0.000	0.000	0.874	Paved parking	1P
0.000	0.000	3.228	0.000	0.000	3.228	TOTAL AREA	

Time span=2.00-30.00 hrs, dt=0.05 hrs, 561 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1E: (new Subcat) Runoff Area=0.544 ac 0.00% Impervious Runoff Depth=2.52"
 Flow Length=81' Slope=0.0247 '/ Tc=10.6 min CN=74 Runoff=2.04 cfs 0.114 af

Subcatchment 1P: (new Subcat) Runoff Area=1.145 ac 76.33% Impervious Runoff Depth=4.28"
 Flow Length=249' Tc=2.8 min CN=92 Runoff=8.53 cfs 0.409 af

Subcatchment 2E: (new Subcat) Runoff Area=0.017 ac 0.00% Impervious Runoff Depth=2.52"
 Flow Length=30' Slope=0.0732 '/ Tc=3.1 min CN=74 Runoff=0.08 cfs 0.004 af

Subcatchment 2P: (new Subcat) Runoff Area=0.007 ac 0.00% Impervious Runoff Depth=2.52"
 Flow Length=33' Slope=0.0758 '/ Tc=3.3 min CN=74 Runoff=0.03 cfs 0.001 af

Subcatchment 3E: (new Subcat) Runoff Area=1.053 ac 0.00% Impervious Runoff Depth=2.52"
 Flow Length=237' Tc=5.8 min CN=74 Runoff=4.62 cfs 0.222 af

Subcatchment 3P: (new Subcat) Runoff Area=0.007 ac 0.00% Impervious Runoff Depth=2.52"
 Flow Length=43' Slope=0.5116 '/ Tc=1.9 min CN=74 Runoff=0.03 cfs 0.001 af

Subcatchment 4P: (new Subcat) Runoff Area=0.167 ac 0.00% Impervious Runoff Depth=2.52"
 Flow Length=83' Tc=2.6 min CN=74 Runoff=0.82 cfs 0.035 af

Subcatchment 5P: (new Subcat) Runoff Area=0.142 ac 0.00% Impervious Runoff Depth=2.52"
 Flow Length=13' Slope=0.0176 '/ Tc=2.8 min CN=74 Runoff=0.70 cfs 0.030 af

Subcatchment 6P: (new Subcat) Runoff Area=0.146 ac 0.00% Impervious Runoff Depth=2.52"
 Flow Length=222' Tc=7.5 min CN=74 Runoff=0.61 cfs 0.031 af

Pond DET1: (new Pond) Peak Elev=983.76' Storage=0.126 af Inflow=9.22 cfs 0.439 af
 Outflow=4.30 cfs 0.439 af

Link 4E: (new Link) Inflow=6.54 cfs 0.340 af
 Primary=6.54 cfs 0.340 af

Link 10L: (new Link) Inflow=5.38 cfs 0.508 af
 Primary=5.38 cfs 0.508 af

Total Runoff Area = 3.228 ac Runoff Volume = 0.847 af Average Runoff Depth = 3.15"
72.92% Pervious = 2.354 ac 27.08% Impervious = 0.874 ac

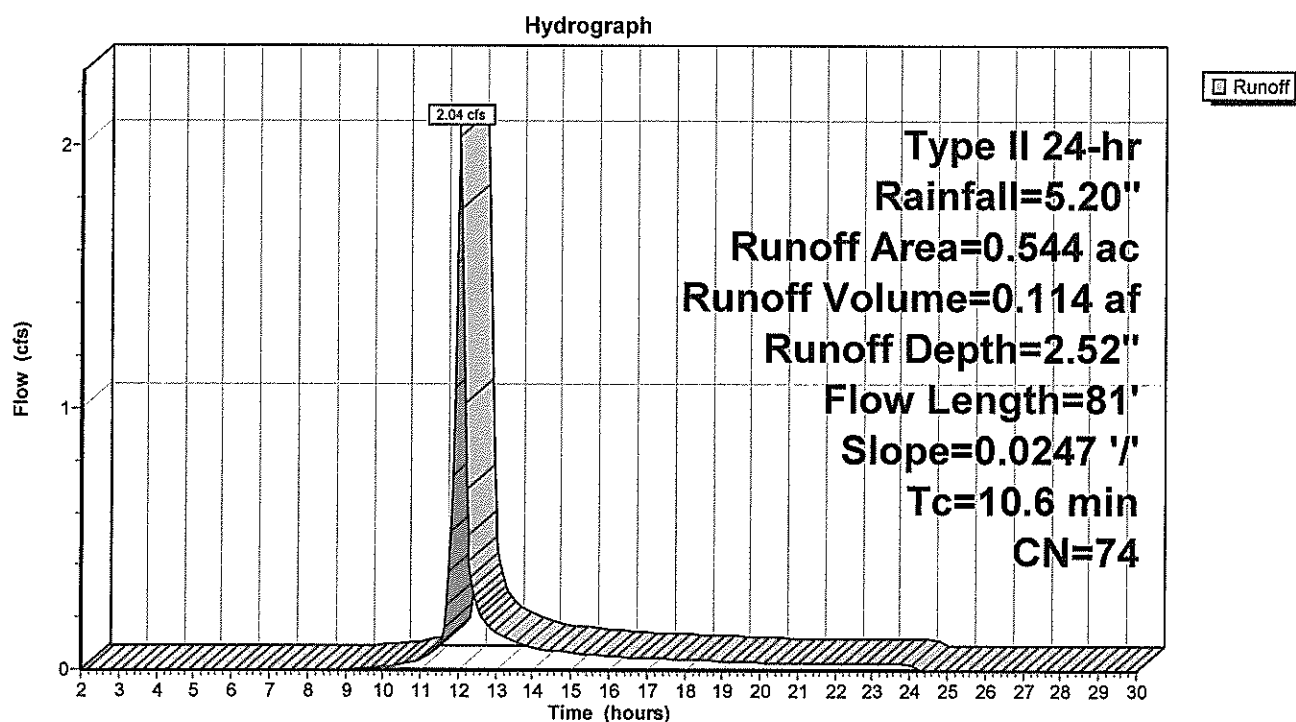
Summary for Subcatchment 1E: (new Subcat)

Runoff = 2.04 cfs @ 12.03 hrs, Volume= 0.114 af, Depth= 2.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs
Type II 24-hr Rainfall=5.20"

Area (ac)	CN	Description
0.544	74	>75% Grass cover, Good, HSG C
0.544		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.6	81	0.0247	0.13		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 1E: (new Subcat)

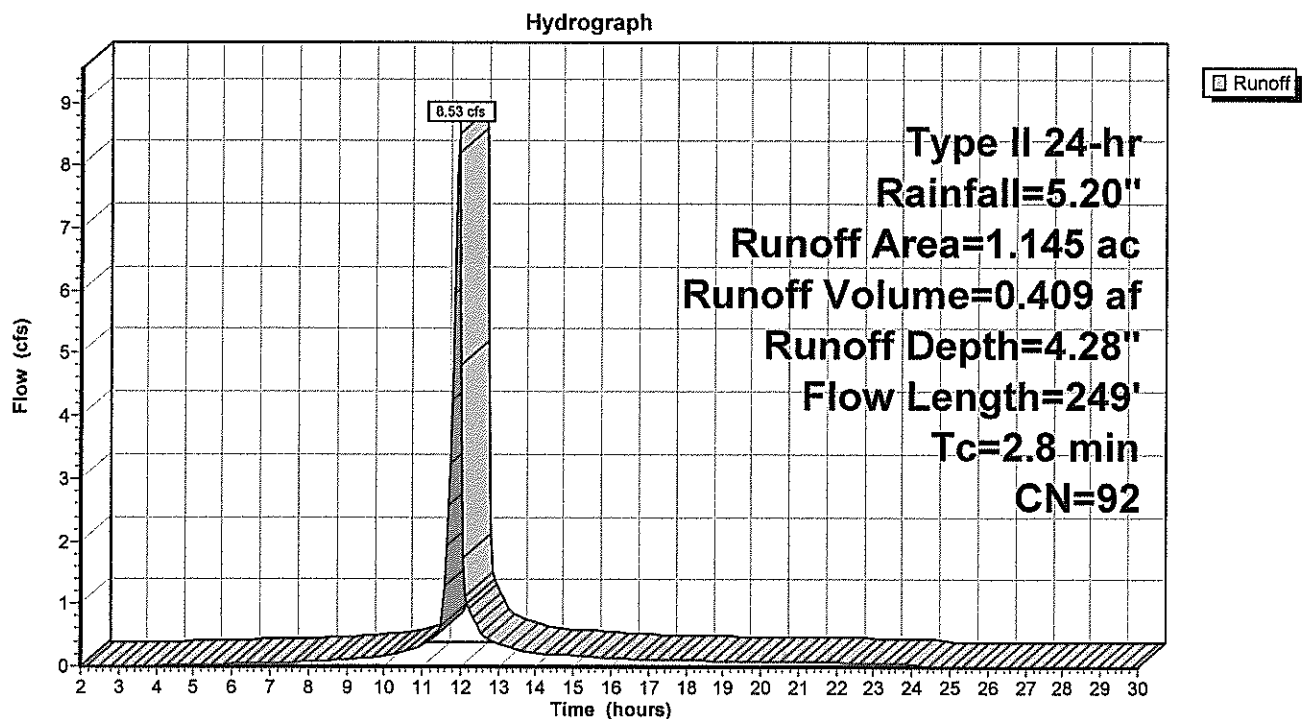
Summary for Subcatchment 1P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 8.53 cfs @ 11.93 hrs, Volume= 0.409 af, Depth= 4.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=5.20"

Area (ac)	CN	Description
0.271	74	>75% Grass cover, Good, HSG C
0.874	98	Paved parking, HSG C
1.145	92	Weighted Average
0.271		23.67% Pervious Area
0.874		76.33% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0065	0.92		Sheet Flow, Smooth surfaces $n=0.011$ $P_2=3.50"$
1.0	149	0.0151	2.49		Shallow Concentrated Flow, Paved $K_v=20.3$ fps
2.8	249	Total			

Subcatchment 1P: (new Subcat)

Summary for Subcatchment 2E: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.08 cfs @ 11.94 hrs, Volume= 0.004 af, Depth= 2.52"

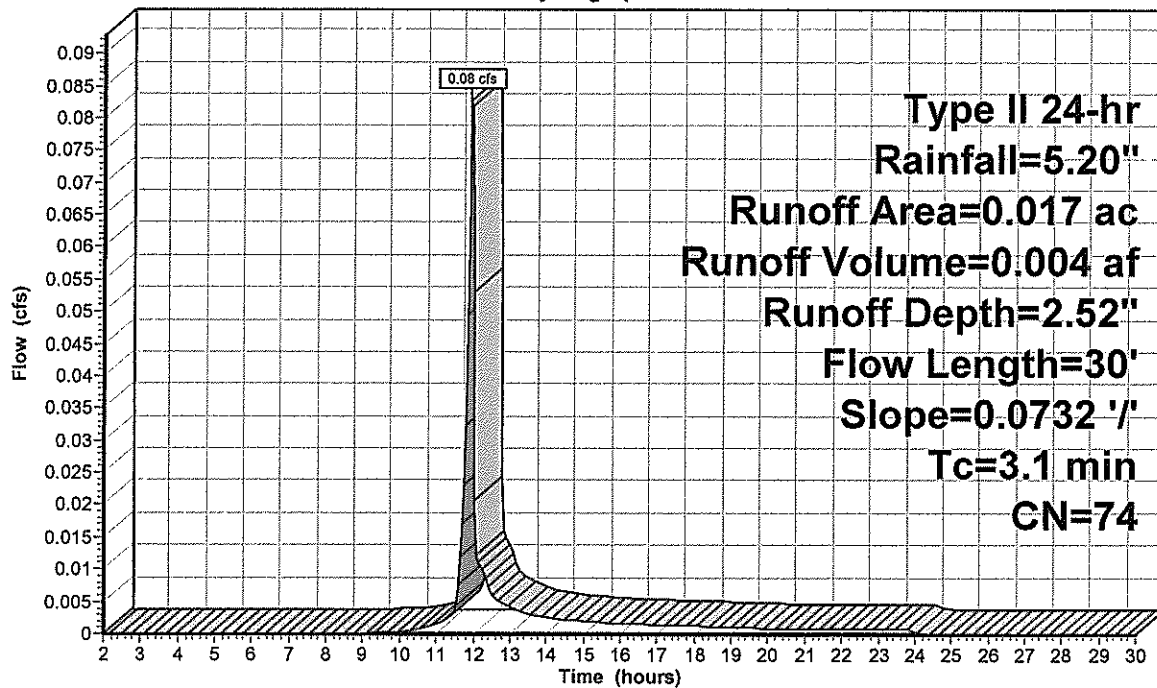
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=5.20"

Area (ac)	CN	Description
0.017	74	>75% Grass cover, Good, HSG C
0.017		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	30	0.0732	0.16		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 2E: (new Subcat)

Hydrograph



Runoff

Summary for Subcatchment 2P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.03 cfs @ 11.94 hrs, Volume= 0.001 af, Depth= 2.52"

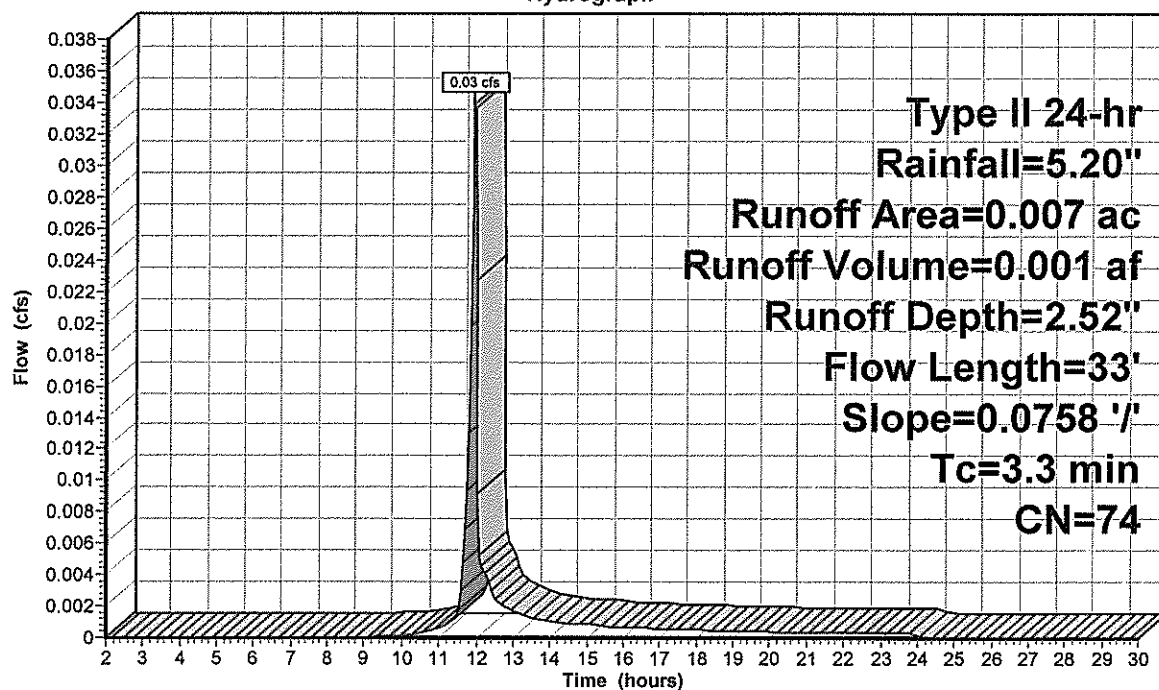
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=5.20"

Area (ac)	CN	Description
0.007	74	>75% Grass cover, Good, HSG C
0.007		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	33	0.0758	0.17		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$

Subcatchment 2P: (new Subcat)

Hydrograph



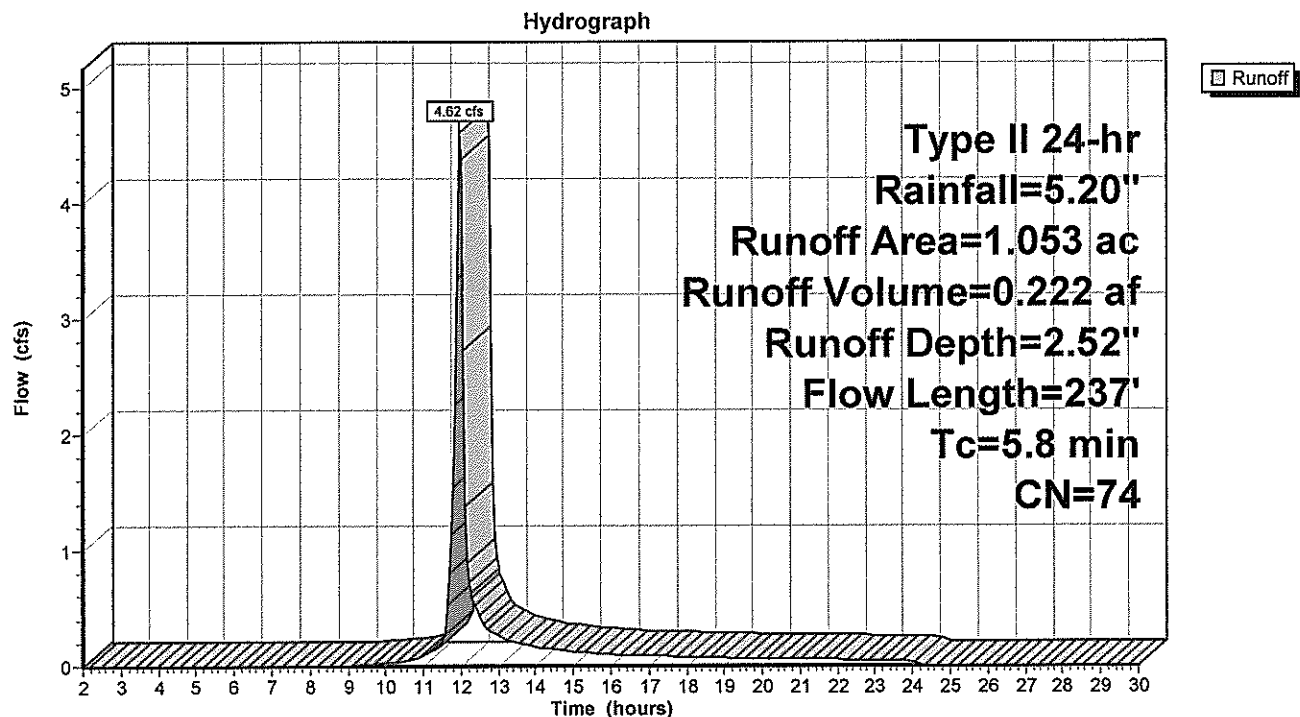
Summary for Subcatchment 3E: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 4.62 cfs @ 11.97 hrs, Volume= 0.222 af, Depth= 2.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=5.20"

Area (ac)	CN	Description
1.053	74	>75% Grass cover, Good, HSG C
1.053		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.4	100	0.2000	0.31		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$
0.4	137	0.1339	5.49		Shallow Concentrated Flow, Grassed Waterway $K_v=15.0$ fps
5.8	237	Total			

Subcatchment 3E: (new Subcat)

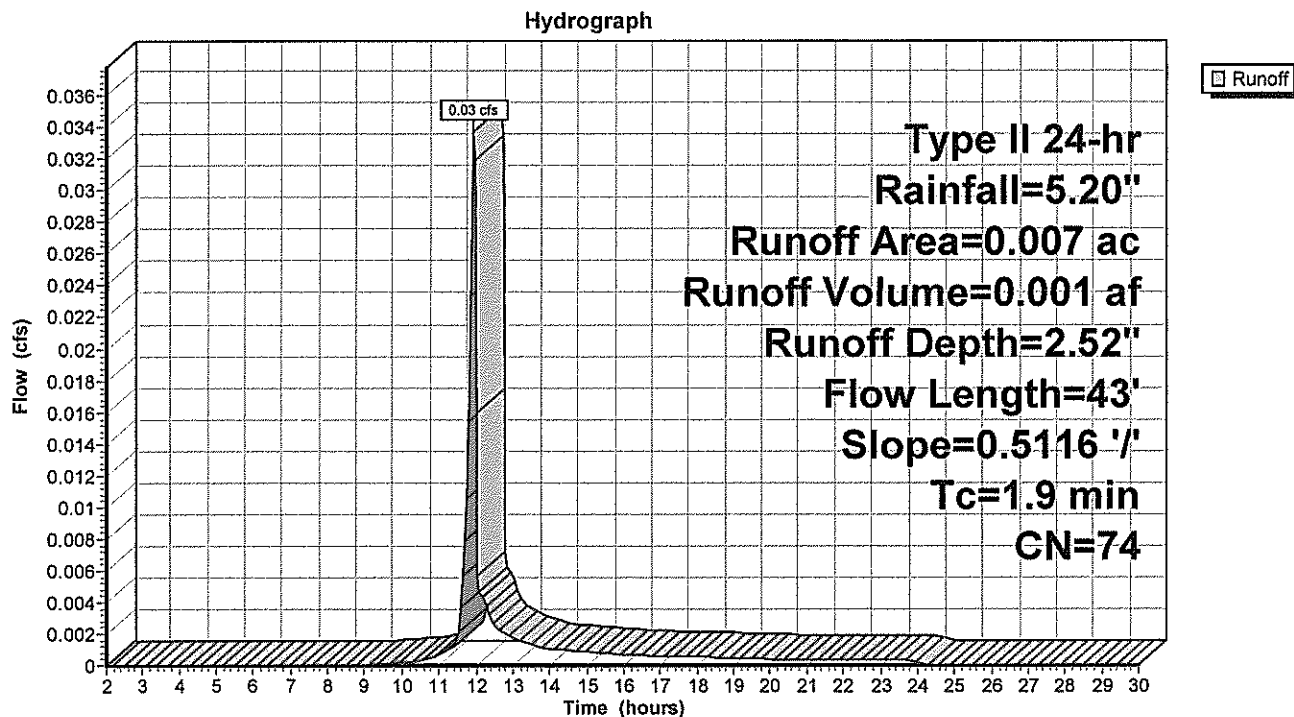
Summary for Subcatchment 3P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.03 cfs @ 11.92 hrs, Volume= 0.001 af, Depth= 2.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=5.20"

Area (ac)	CN	Description
0.007	74	>75% Grass cover, Good, HSG C
0.007		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	43	0.5116	0.38		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$

Subcatchment 3P: (new Subcat)

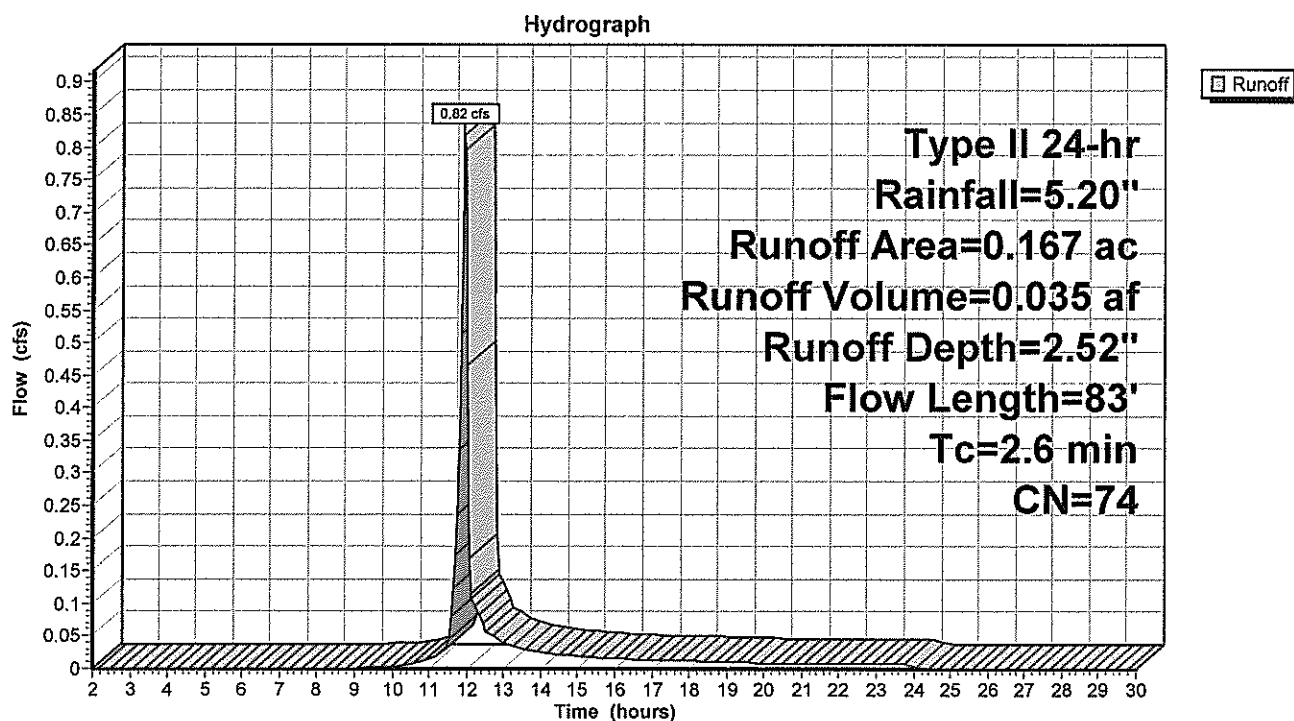
Summary for Subcatchment 4P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.82 cfs @ 11.93 hrs, Volume= 0.035 af, Depth= 2.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=5.20"

Area (ac)	CN	Description
0.167	74	>75% Grass cover, Good, HSG C
0.167		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	30	0.1453	0.21		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$
0.2	53	0.0967	5.01		Shallow Concentrated Flow, Unpaved $K_v=16.1$ fps
2.6	83	Total			

Subcatchment 4P: (new Subcat)

Summary for Subcatchment 5P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.70 cfs @ 11.94 hrs, Volume= 0.030 af, Depth= 2.52"

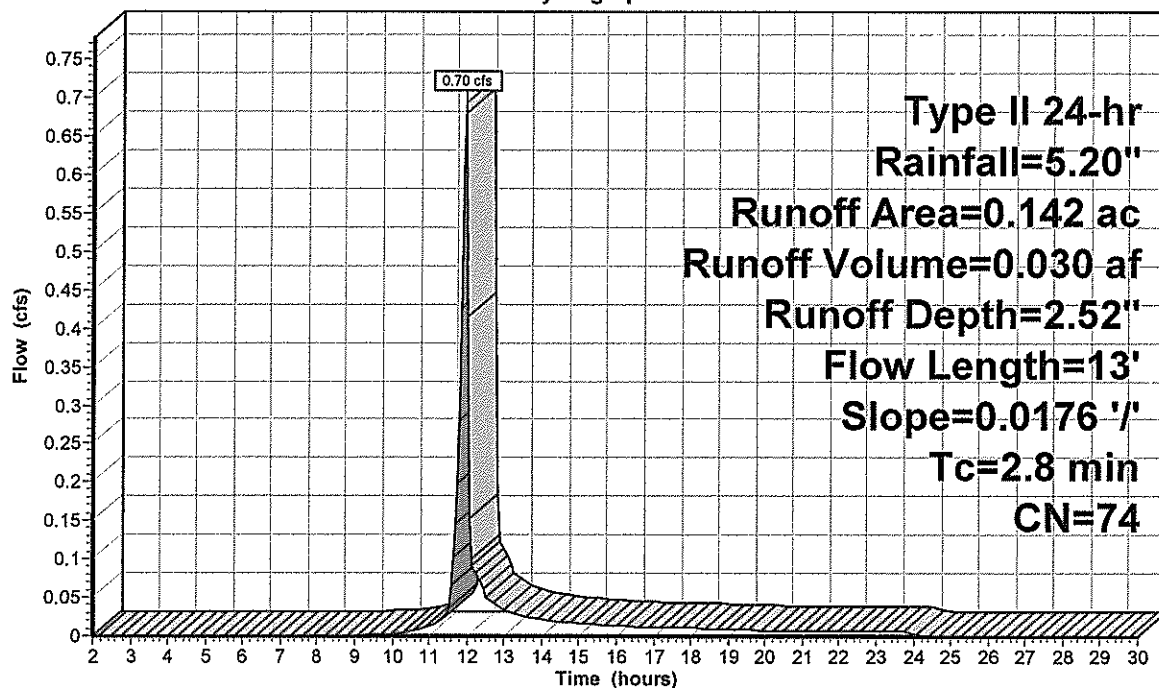
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=5.20"

Area (ac)	CN	Description
0.142	74	>75% Grass cover, Good, HSG C
0.142		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.8	13	0.0176	0.08		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 5P: (new Subcat)

Hydrograph



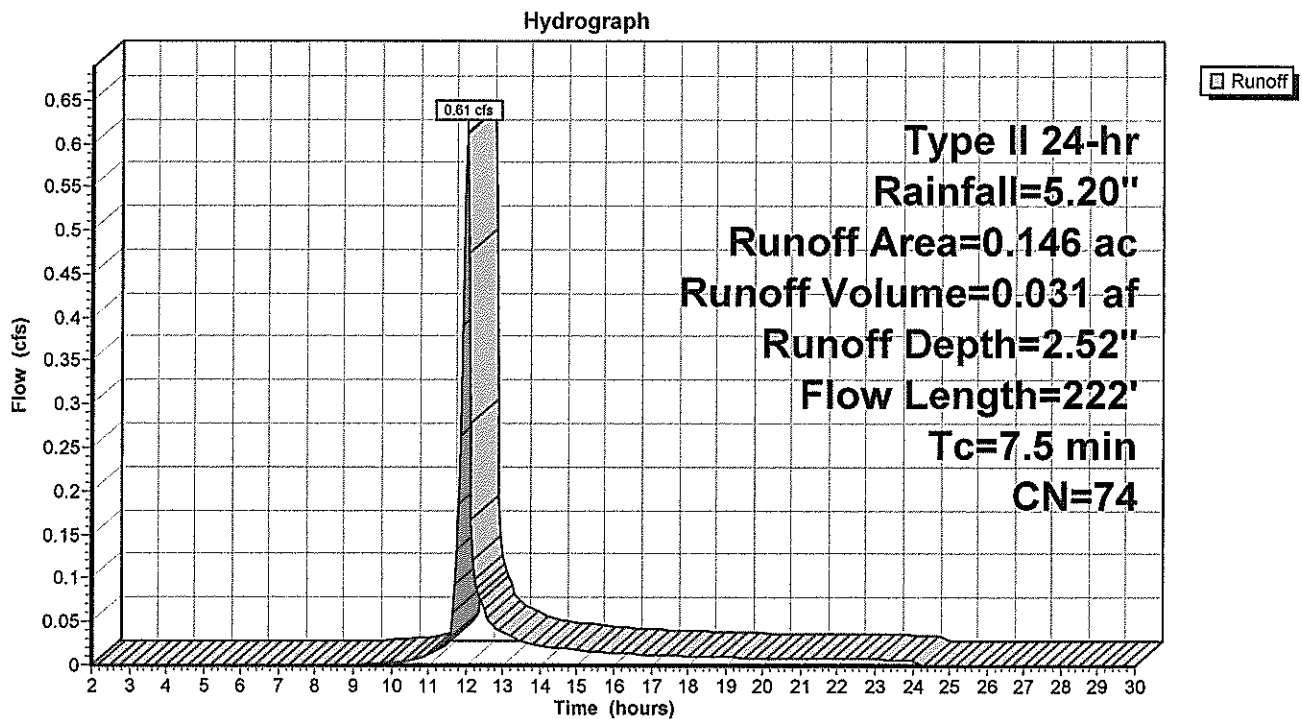
Summary for Subcatchment 6P: (new Subcat)

Runoff = 0.61 cfs @ 11.99 hrs, Volume= 0.031 af, Depth= 2.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs
Type II 24-hr Rainfall=5.20"

Area (ac)	CN	Description
0.146	74	>75% Grass cover, Good, HSG C
0.146		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.9	60	0.0400	0.15		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"
0.6	162	0.0775	4.18		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
7.5	222	Total			

Subcatchment 6P: (new Subcat)

Summary for Pond DET1: (new Pond)

Inflow Area = 1.287 ac, 67.91% Impervious, Inflow Depth = 4.09"
 Inflow = 9.22 cfs @ 11.93 hrs, Volume= 0.439 af
 Outflow = 4.30 cfs @ 12.02 hrs, Volume= 0.439 af, Atten= 53%, Lag= 5.2 min
 Primary = 4.30 cfs @ 12.02 hrs, Volume= 0.439 af

Routing by Stor-Ind method, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs
 Peak Elev= 983.76' @ 12.02 hrs Surf.Area= 0.088 ac Storage= 0.126 af

Plug-Flow detention time= 27.3 min calculated for 0.438 af (100% of inflow)
 Center-of-Mass det. time= 27.4 min (806.2 - 778.8)

Volume	Invert	Avail.Storage	Storage Description
#1	982.03'	0.211 af	36.0" Round Pipe Storage L= 1,300.0'

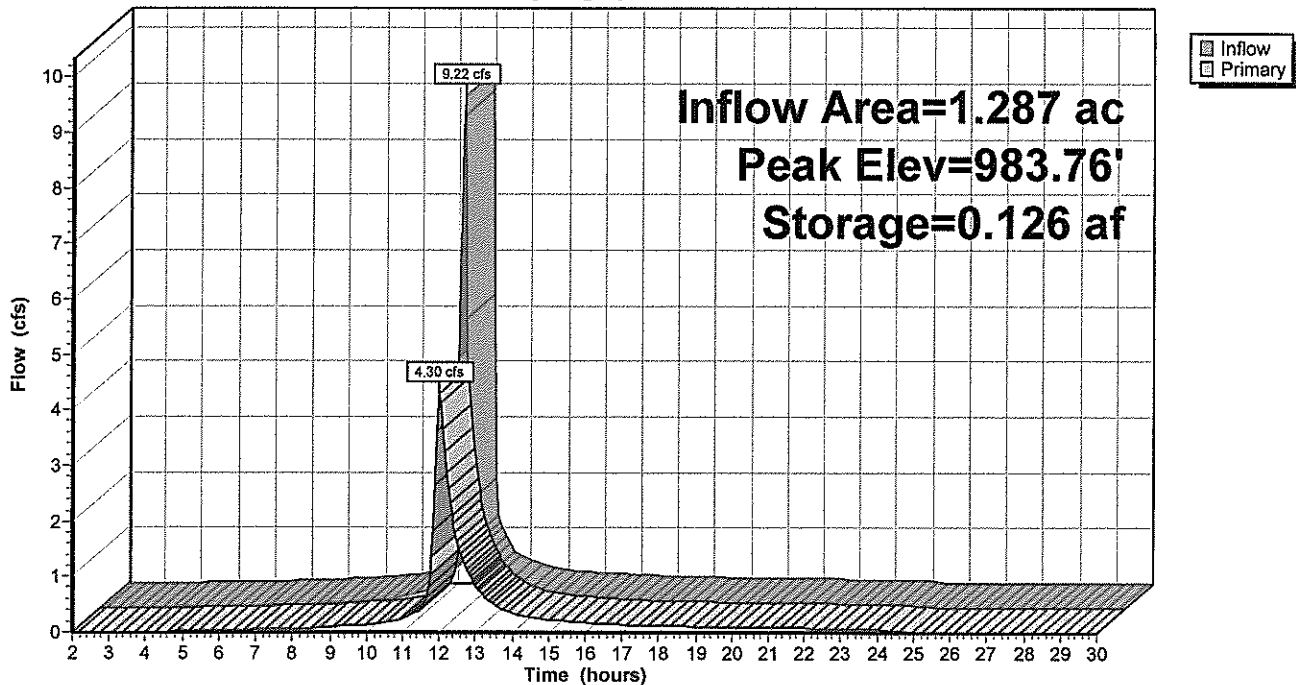
Device	Routing	Invert	Outlet Devices
#1	Primary	982.03'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28) Head (feet) 0.00 1.03 1.03 1.93 1.93 3.00 Width (feet) 0.50 0.50 0.79 0.79 2.50 2.50

Primary OutFlow Max=4.21 cfs @ 12.02 hrs HW=983.74' (Free Discharge)

↑1=Custom Weir/Orifice (Weir Controls 4.21 cfs @ 3.99 fps)

Pond DET1: (new Pond)

Hydrograph



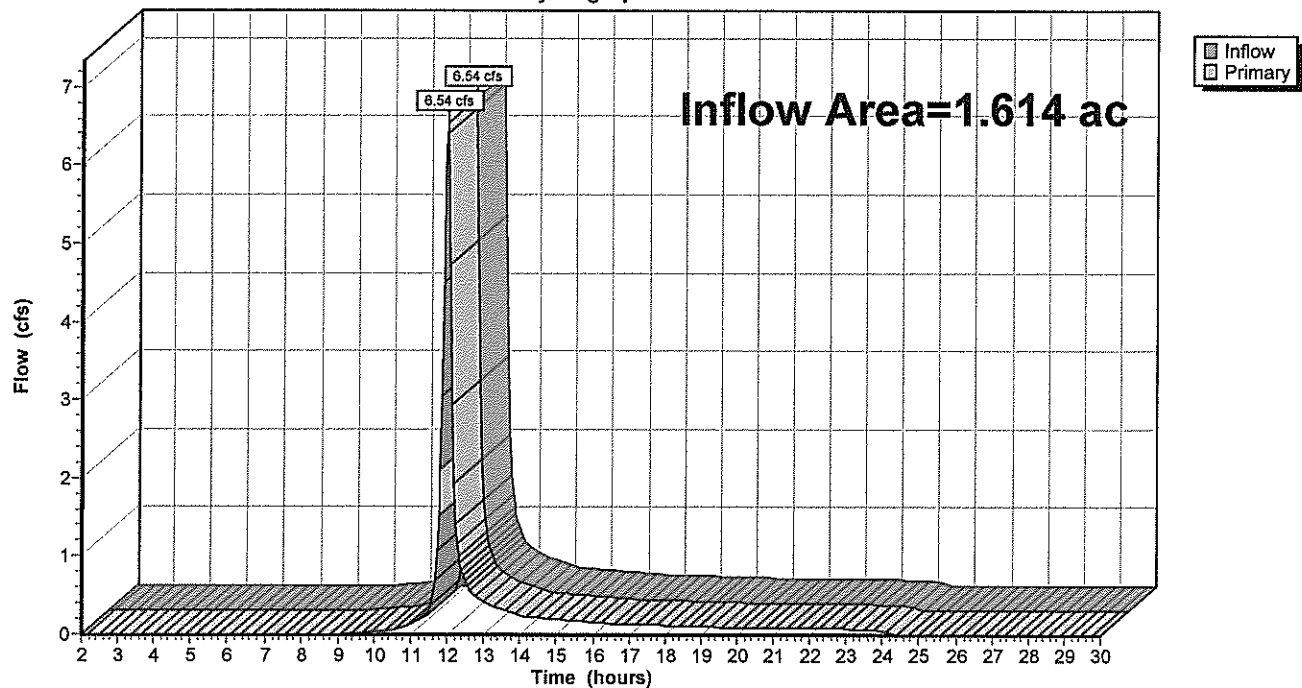
Summary for Link 4E: (new Link)

Inflow Area = 1.614 ac, 0.00% Impervious, Inflow Depth = 2.52"
Inflow = 6.54 cfs @ 11.98 hrs, Volume= 0.340 af
Primary = 6.54 cfs @ 11.98 hrs, Volume= 0.340 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs

Link 4E: (new Link)

Hydrograph



Summary for Link 10L: (new Link)

Inflow Area = 1.614 ac, 54.15% Impervious, Inflow Depth = 3.77"
Inflow = 5.38 cfs @ 11.99 hrs, Volume= 0.508 af
Primary = 5.38 cfs @ 11.99 hrs, Volume= 0.508 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs

Link 10L: (new Link)

Hydrograph

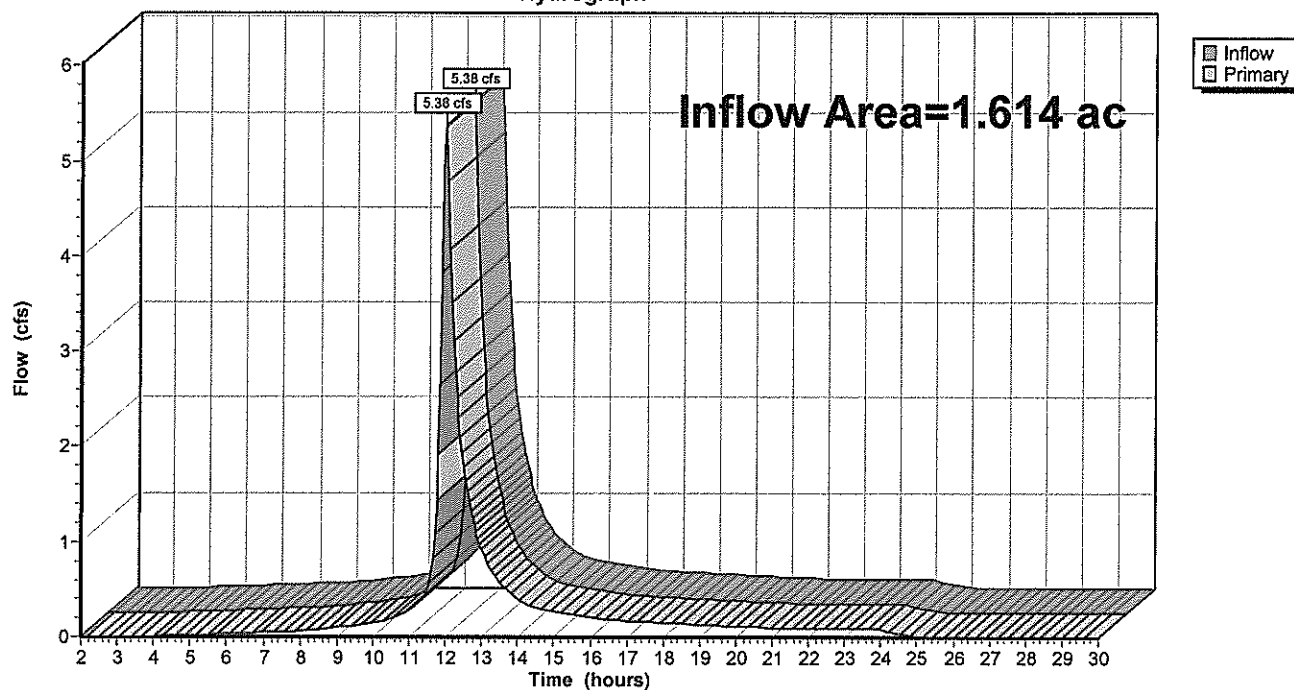
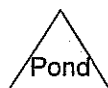
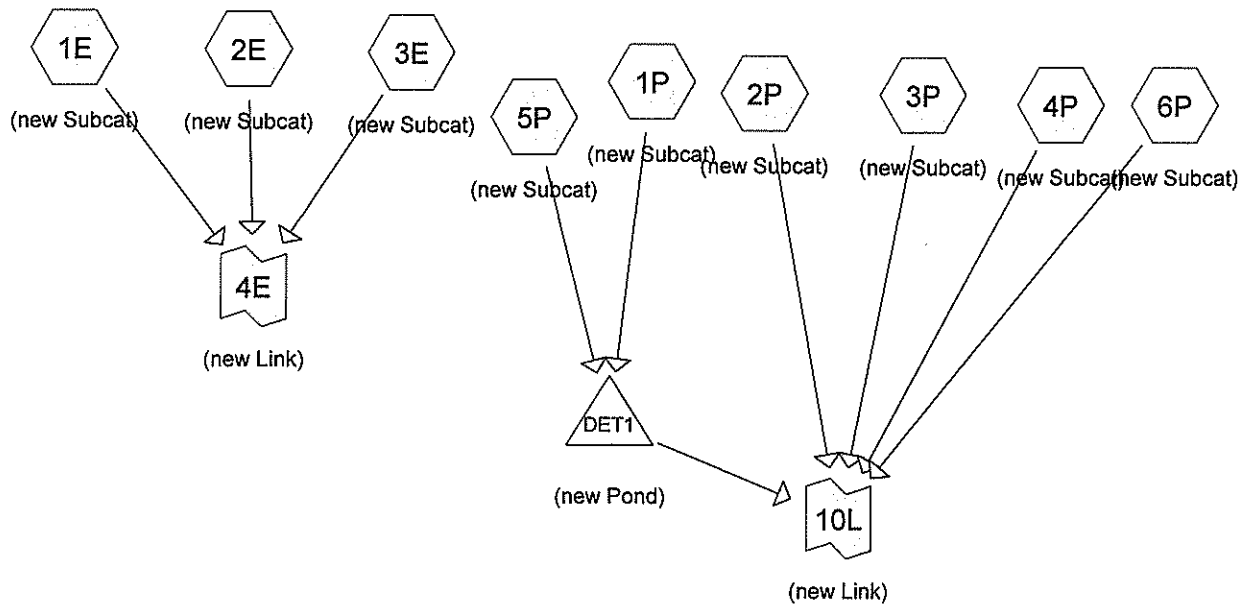


Exhibit 4
100-year Storm Calculations



Routing Diagram for 400 NW 72 Street

Prepared by HP, Printed 7/20/2023

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400 NW 72 Street

Prepared by HP

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Page 2

Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
2.354	74	>75% Grass cover, Good, HSG C (1E, 1P, 2E, 2P, 3E, 3P, 4P, 5P, 6P)
0.874	98	Paved parking, HSG C (1P)
3.228	80	TOTAL AREA

Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
3.228	HSG C	1E, 1P, 2E, 2P, 3E, 3P, 4P, 5P, 6P
0.000	HSG D	
0.000	Other	
3.228		TOTAL AREA

400 NW 72 Street

Prepared by HP

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Page 4

Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	2.354	0.000	0.000	2.354	>75% Grass cover, Good	1E, 1P, 2E, 2P, 3E, 3P, 4P, 5P, 6P
0.000	0.000	0.874	0.000	0.000	0.874	Paved parking	1P
0.000	0.000	3.228	0.000	0.000	3.228	TOTAL AREA	

Time span=2.00-30.00 hrs, dt=0.05 hrs, 561 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1E: (new Subcat) Runoff Area=0.544 ac 0.00% Impervious Runoff Depth=4.57"
 Flow Length=81' Slope=0.0247 '/' Tc=10.6 min CN=74 Runoff=3.65 cfs 0.207 af

Subcatchment 1P: (new Subcat) Runoff Area=1.145 ac 76.33% Impervious Runoff Depth=6.65"
 Flow Length=249' Tc=2.8 min CN=92 Runoff=12.83 cfs 0.634 af

Subcatchment 2E: (new Subcat) Runoff Area=0.017 ac 0.00% Impervious Runoff Depth=4.57"
 Flow Length=30' Slope=0.0732 '/' Tc=3.1 min CN=74 Runoff=0.15 cfs 0.006 af

Subcatchment 2P: (new Subcat) Runoff Area=0.007 ac 0.00% Impervious Runoff Depth=4.57"
 Flow Length=33' Slope=0.0758 '/' Tc=3.3 min CN=74 Runoff=0.06 cfs 0.003 af

Subcatchment 3E: (new Subcat) Runoff Area=1.053 ac 0.00% Impervious Runoff Depth=4.57"
 Flow Length=237' Tc=5.8 min CN=74 Runoff=8.24 cfs 0.401 af

Subcatchment 3P: (new Subcat) Runoff Area=0.007 ac 0.00% Impervious Runoff Depth=4.57"
 Flow Length=43' Slope=0.5116 '/' Tc=1.9 min CN=74 Runoff=0.06 cfs 0.003 af

Subcatchment 4P: (new Subcat) Runoff Area=0.167 ac 0.00% Impervious Runoff Depth=4.57"
 Flow Length=83' Tc=2.6 min CN=74 Runoff=1.45 cfs 0.064 af

Subcatchment 5P: (new Subcat) Runoff Area=0.142 ac 0.00% Impervious Runoff Depth=4.57"
 Flow Length=13' Slope=0.0176 '/' Tc=2.8 min CN=74 Runoff=1.23 cfs 0.054 af

Subcatchment 6P: (new Subcat) Runoff Area=0.146 ac 0.00% Impervious Runoff Depth=4.57"
 Flow Length=222' Tc=7.5 min CN=74 Runoff=1.10 cfs 0.056 af

Pond DET1: (new Pond) Peak Elev=984.37' Storage=0.177 af Inflow=14.06 cfs 0.688 af
 Outflow=8.78 cfs 0.688 af

Link 4E: (new Link) Inflow=11.69 cfs 0.615 af
 Primary=11.69 cfs 0.615 af

Link 10L: (new Link) Inflow=10.81 cfs 0.813 af
 Primary=10.81 cfs 0.813 af

Total Runoff Area = 3.228 ac Runoff Volume = 1.427 af Average Runoff Depth = 5.31"
72.92% Pervious = 2.354 ac 27.08% Impervious = 0.874 ac

Summary for Subcatchment 1E: (new Subcat)

Runoff = 3.65 cfs @ 12.02 hrs, Volume= 0.207 af, Depth= 4.57"

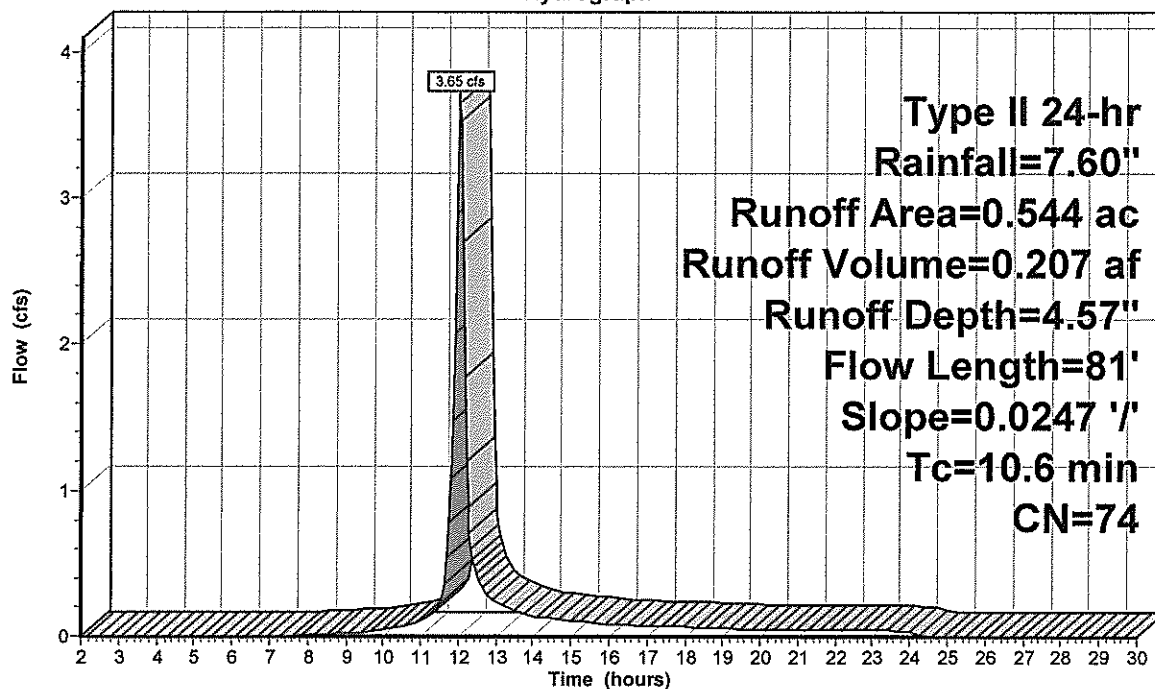
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs
Type II 24-hr Rainfall=7.60"

Area (ac)	CN	Description
0.544	74	>75% Grass cover, Good, HSG C
0.544		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.6	81	0.0247	0.13		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 1E: (new Subcat)

Hydrograph



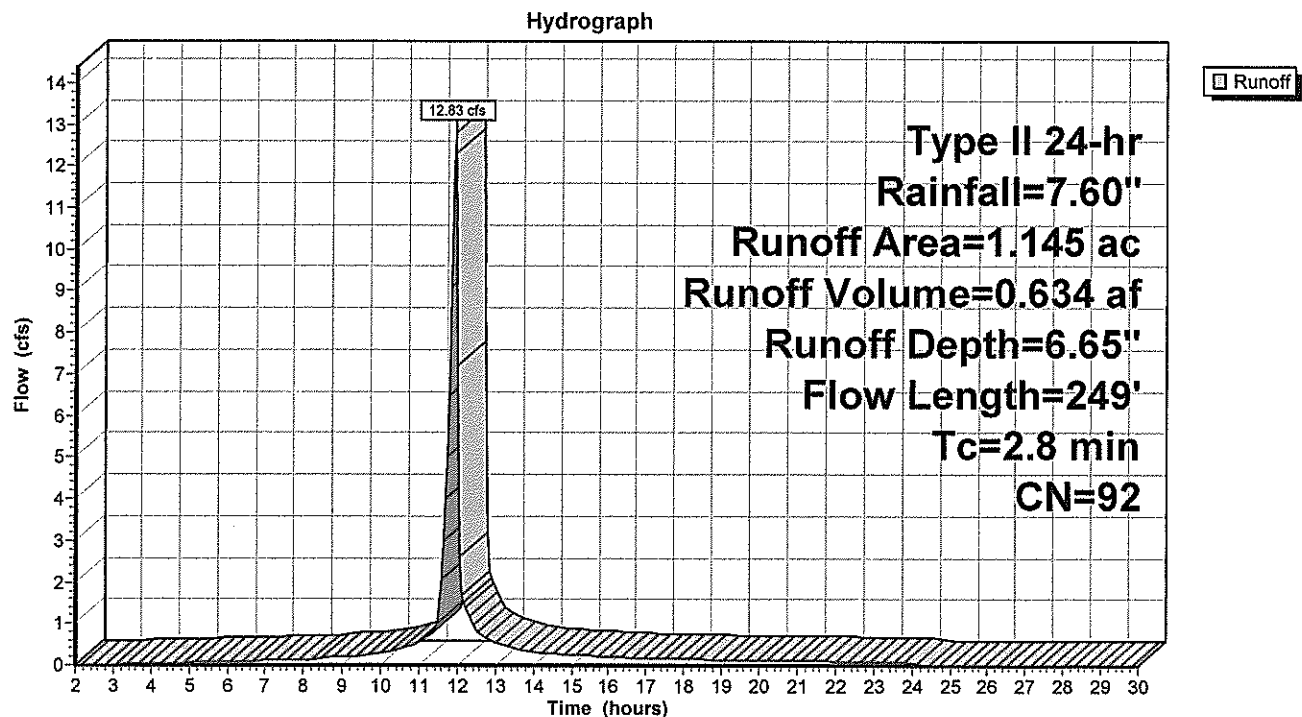
Summary for Subcatchment 1P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 12.83 cfs @ 11.93 hrs, Volume= 0.634 af, Depth= 6.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=7.60"

Area (ac)	CN	Description
0.271	74	>75% Grass cover, Good, HSG C
0.874	98	Paved parking, HSG C
1.145	92	Weighted Average
0.271		23.67% Pervious Area
0.874		76.33% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0065	0.92		Sheet Flow, Smooth surfaces n= 0.011 P2= 3.50"
1.0	149	0.0151	2.49		Shallow Concentrated Flow, Paved Kv= 20.3 fps
2.8	249	Total			

Subcatchment 1P: (new Subcat)

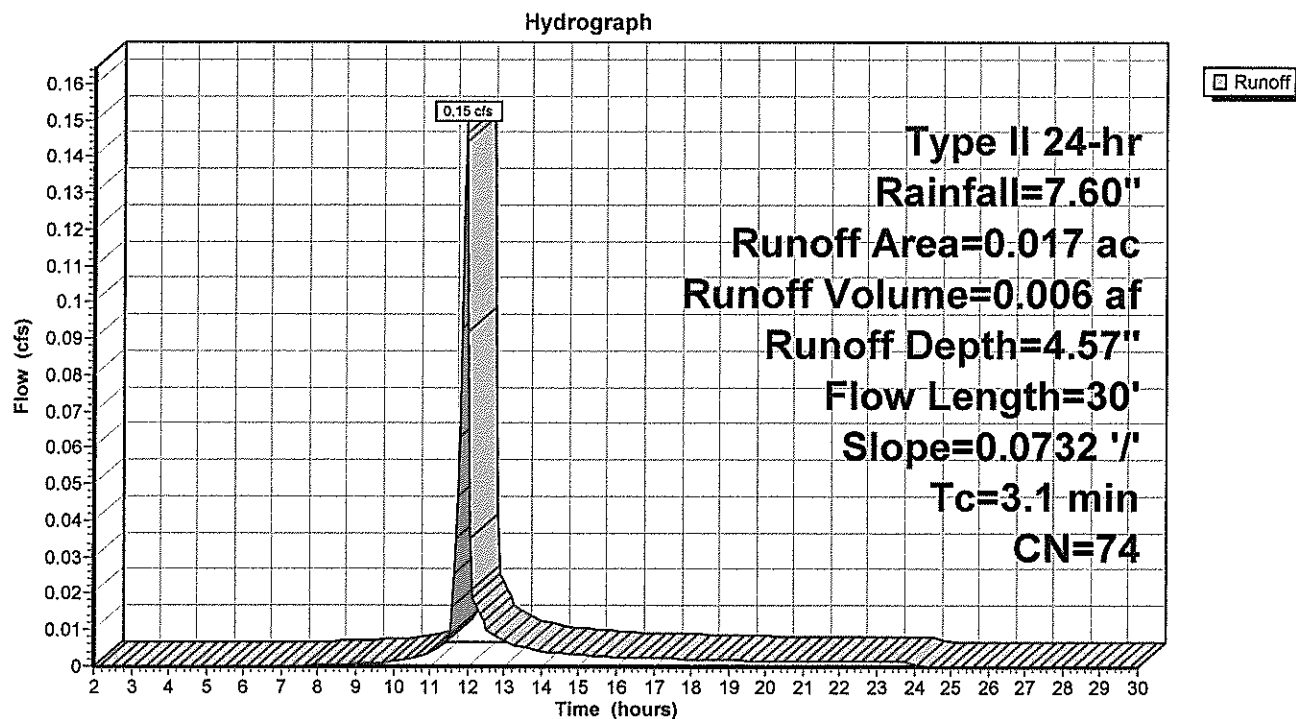
Summary for Subcatchment 2E: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.15 cfs @ 11.94 hrs, Volume= 0.006 af, Depth= 4.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=7.60"

Area (ac)	CN	Description
0.017	74	>75% Grass cover, Good, HSG C
0.017		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	30	0.0732	0.16		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 2E: (new Subcat)

Summary for Subcatchment 2P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.06 cfs @ 11.94 hrs, Volume= 0.003 af, Depth= 4.57"

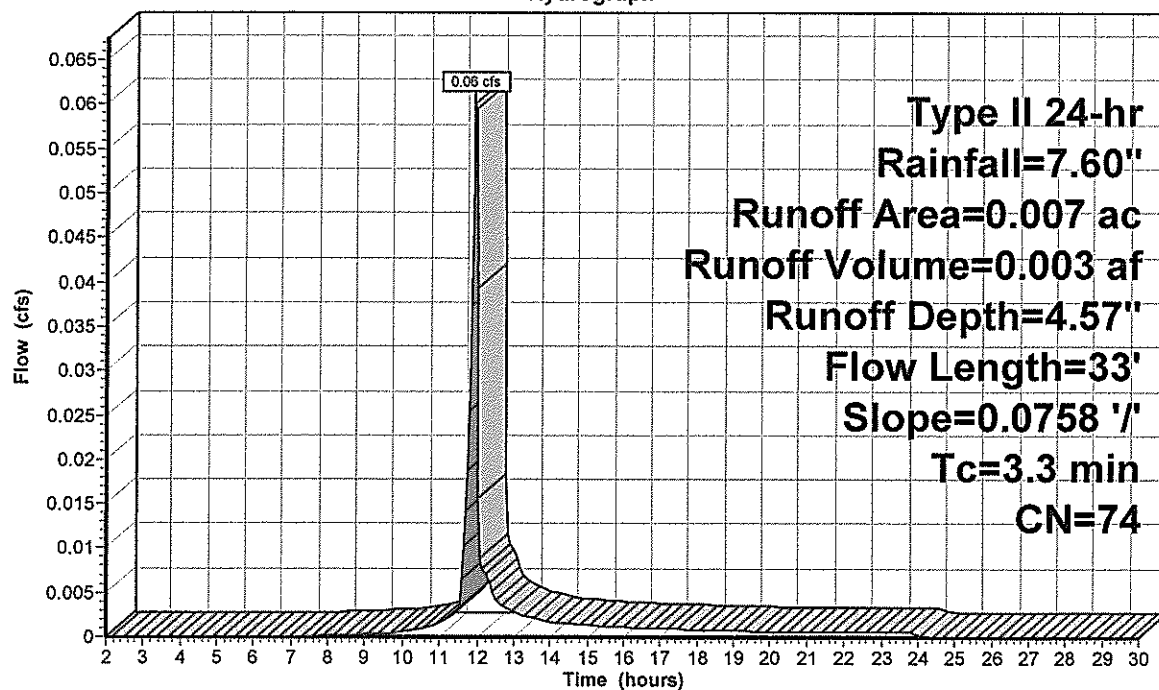
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=7.60"

Area (ac)	CN	Description
0.007	74	>75% Grass cover, Good, HSG C
0.007		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	33	0.0758	0.17		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$

Subcatchment 2P: (new Subcat)

Hydrograph



Runoff

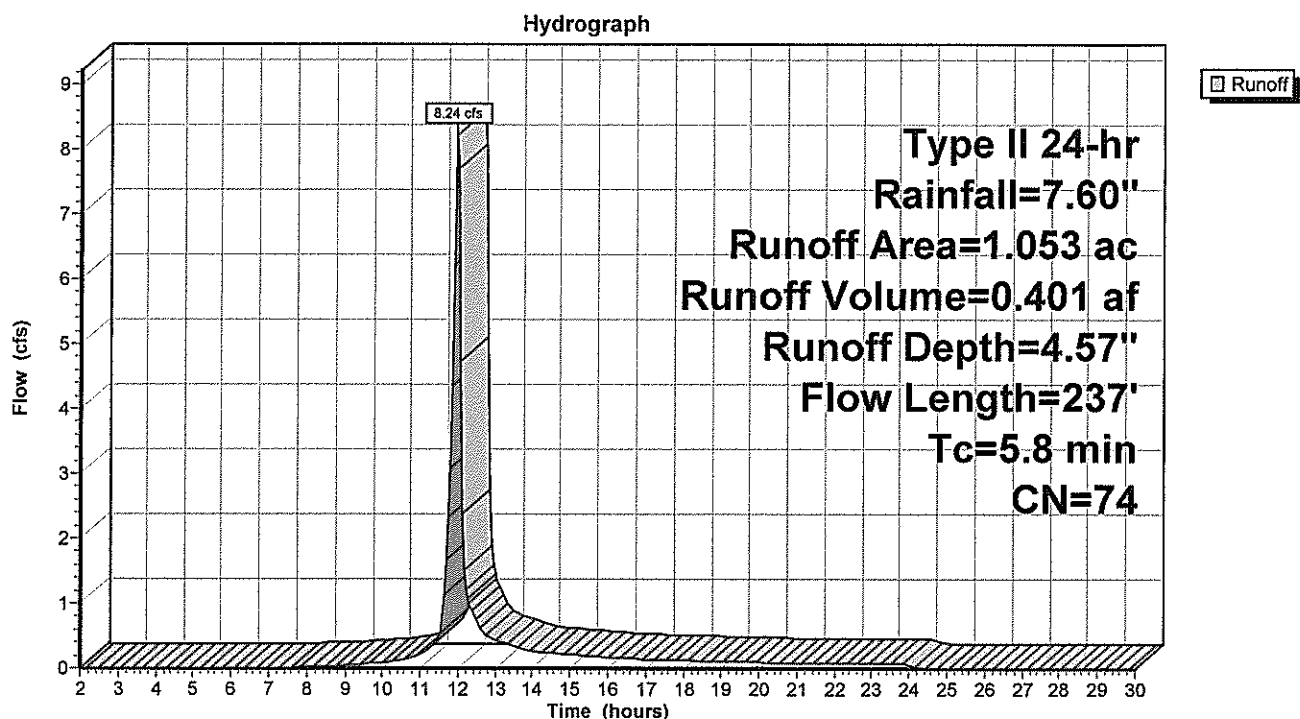
Summary for Subcatchment 3E: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 8.24 cfs @ 11.97 hrs, Volume= 0.401 af, Depth= 4.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=7.60"

Area (ac)	CN	Description
1.053	74	>75% Grass cover, Good, HSG C
1.053		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.4	100	0.2000	0.31		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$
0.4	137	0.1339	5.49		Shallow Concentrated Flow, Grassed Waterway $K_v=15.0$ fps
5.8	237	Total			

Subcatchment 3E: (new Subcat)

Summary for Subcatchment 3P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.06 cfs @ 11.92 hrs, Volume= 0.003 af, Depth= 4.57"

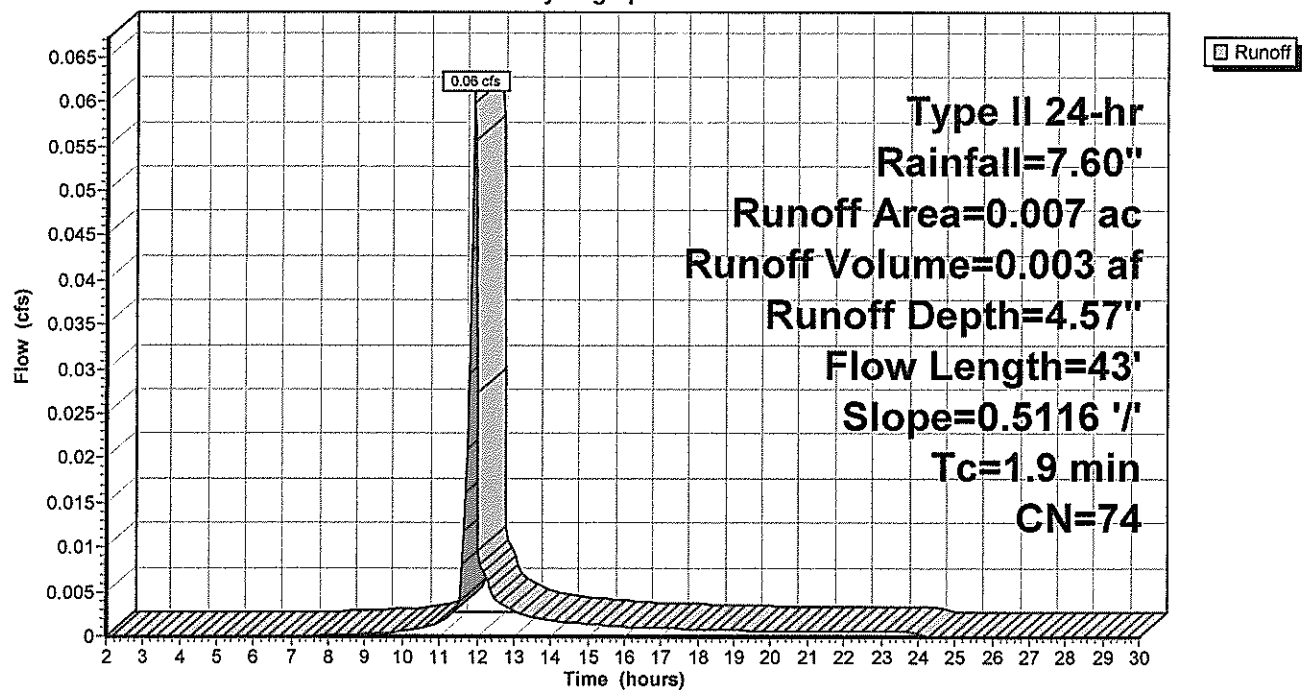
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=7.60"

Area (ac)	CN	Description
0.007	74	>75% Grass cover, Good, HSG C
0.007		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	43	0.5116	0.38		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 3P: (new Subcat)

Hydrograph



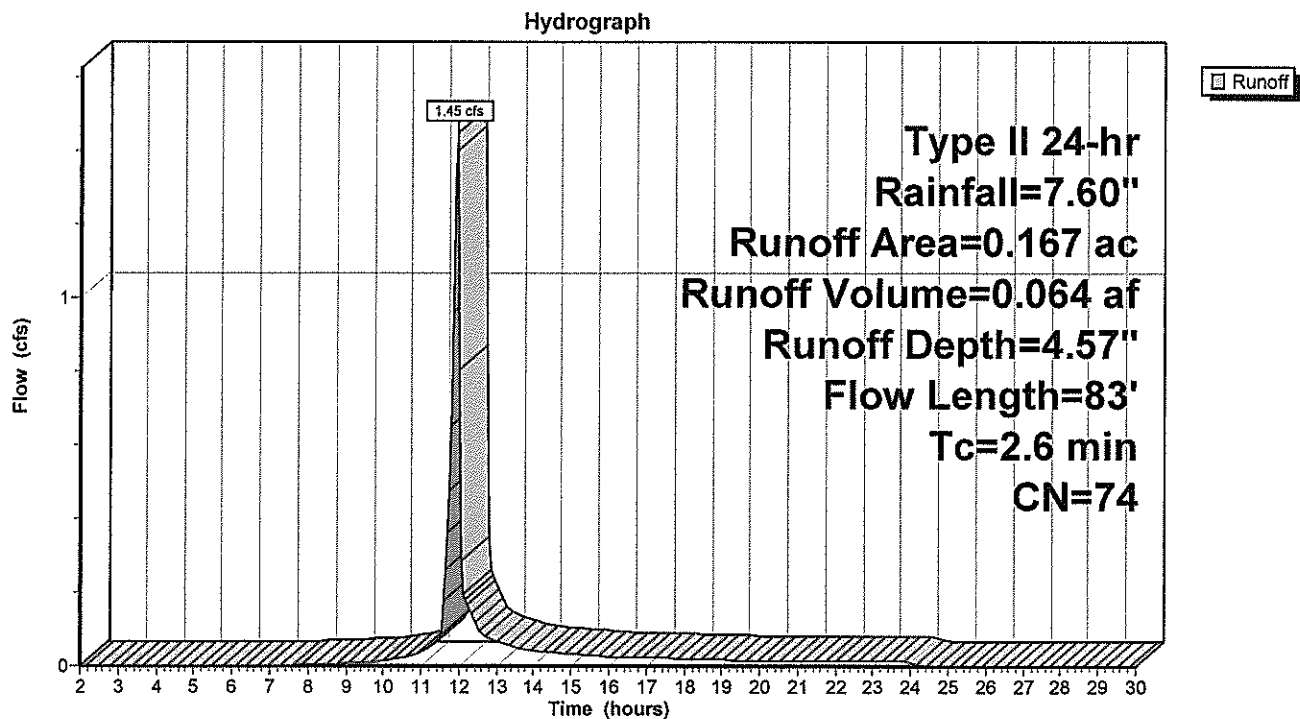
Summary for Subcatchment 4P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 1.45 cfs @ 11.93 hrs, Volume= 0.064 af, Depth= 4.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=7.60"

Area (ac)	CN	Description
0.167	74	>75% Grass cover, Good, HSG C
0.167		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	30	0.1453	0.21		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$
0.2	53	0.0967	5.01		Shallow Concentrated Flow, Unpaved $K_v=16.1$ fps
2.6	83	Total			

Subcatchment 4P: (new Subcat)

Summary for Subcatchment 5P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 1.23 cfs @ 11.93 hrs, Volume= 0.054 af, Depth= 4.57"

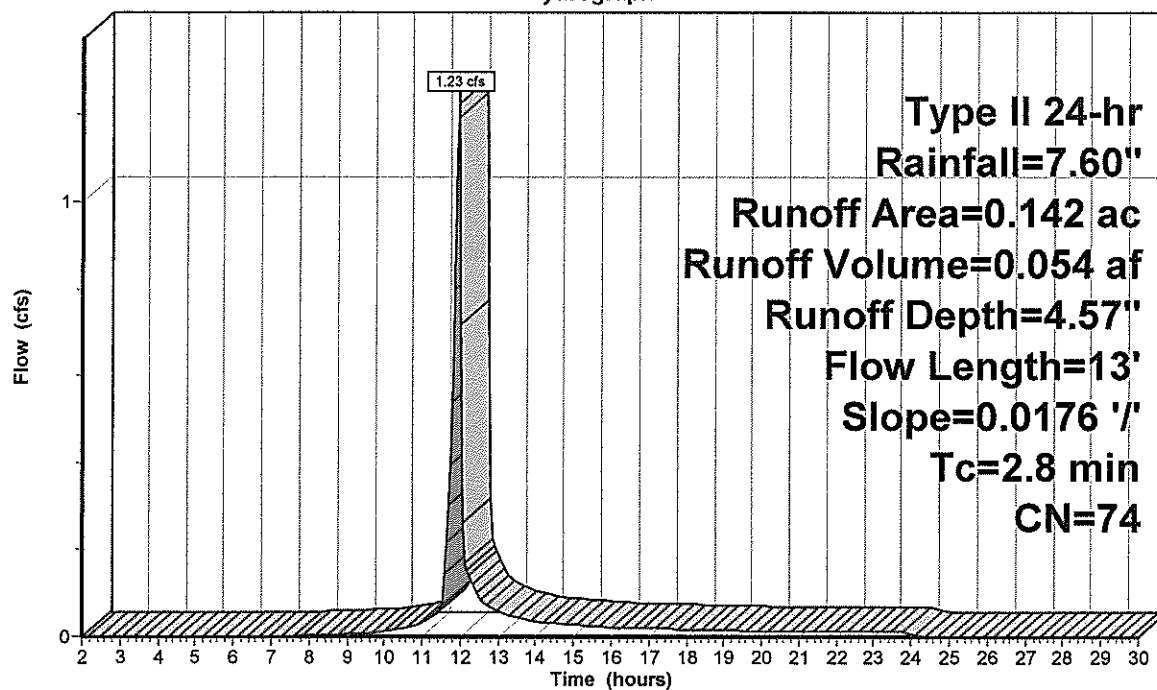
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=7.60"

Area (ac)	CN	Description
0.142	74	>75% Grass cover, Good, HSG C
0.142		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.8	13	0.0176	0.08		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 5P: (new Subcat)

Hydrograph



Summary for Subcatchment 6P: (new Subcat)

Runoff = 1.10 cfs @ 11.99 hrs, Volume= 0.056 af, Depth= 4.57"

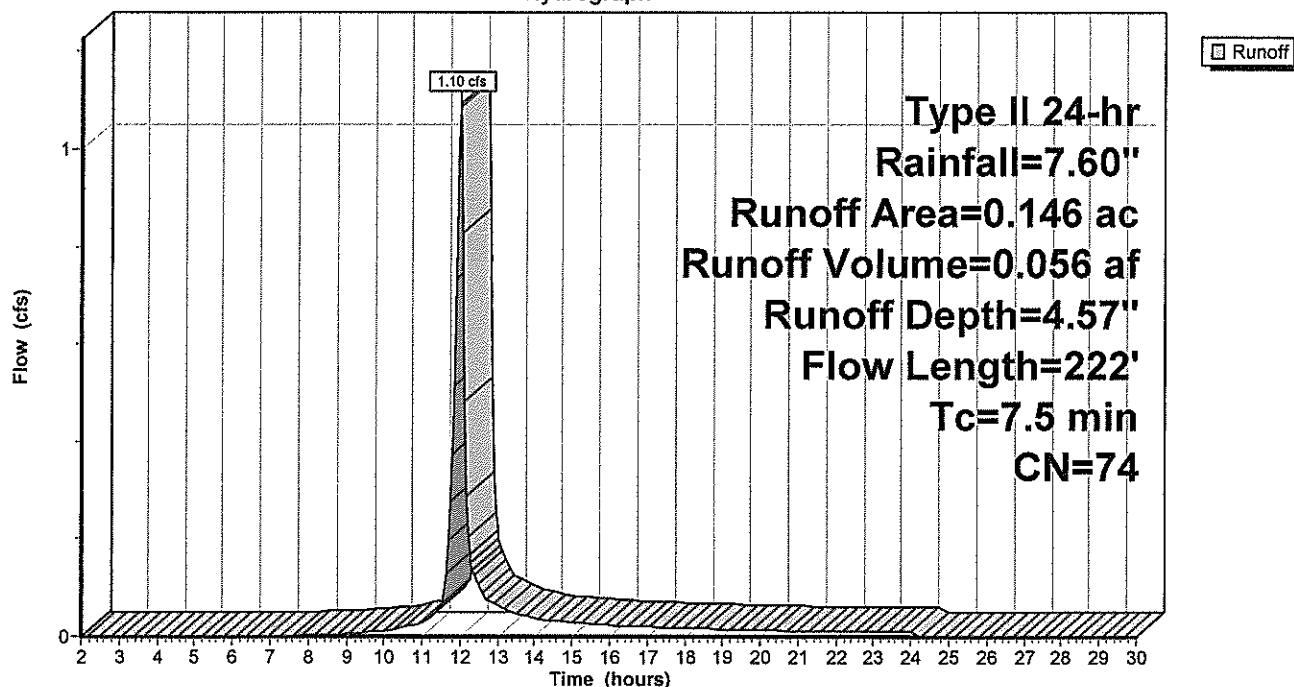
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs
Type II 24-hr Rainfall=7.60"

Area (ac)	CN	Description
0.146	74	>75% Grass cover, Good, HSG C
0.146		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.9	60	0.0400	0.15		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"
0.6	162	0.0775	4.18		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
7.5	222	Total			

Subcatchment 6P: (new Subcat)

Hydrograph



Summary for Pond DET1: (new Pond)

Inflow Area = 1.287 ac, 67.91% Impervious, Inflow Depth = 6.42"
 Inflow = 14.06 cfs @ 11.93 hrs, Volume= 0.688 af
 Outflow = 8.78 cfs @ 12.00 hrs, Volume= 0.688 af, Atten= 38%, Lag= 4.3 min
 Primary = 8.78 cfs @ 12.00 hrs, Volume= 0.688 af

Routing by Stor-Ind method, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs
 Peak Elev= 984.37' @ 12.00 hrs Surf.Area= 0.074 ac Storage= 0.177 af

Plug-Flow detention time= 25.7 min calculated for 0.688 af (100% of inflow)
 Center-of-Mass det. time= 25.5 min (793.2 - 767.7)

Volume	Invert	Avail.Storage	Storage Description
#1	982.03'	0.211 af	36.0" Round Pipe Storage L= 1,300.0'

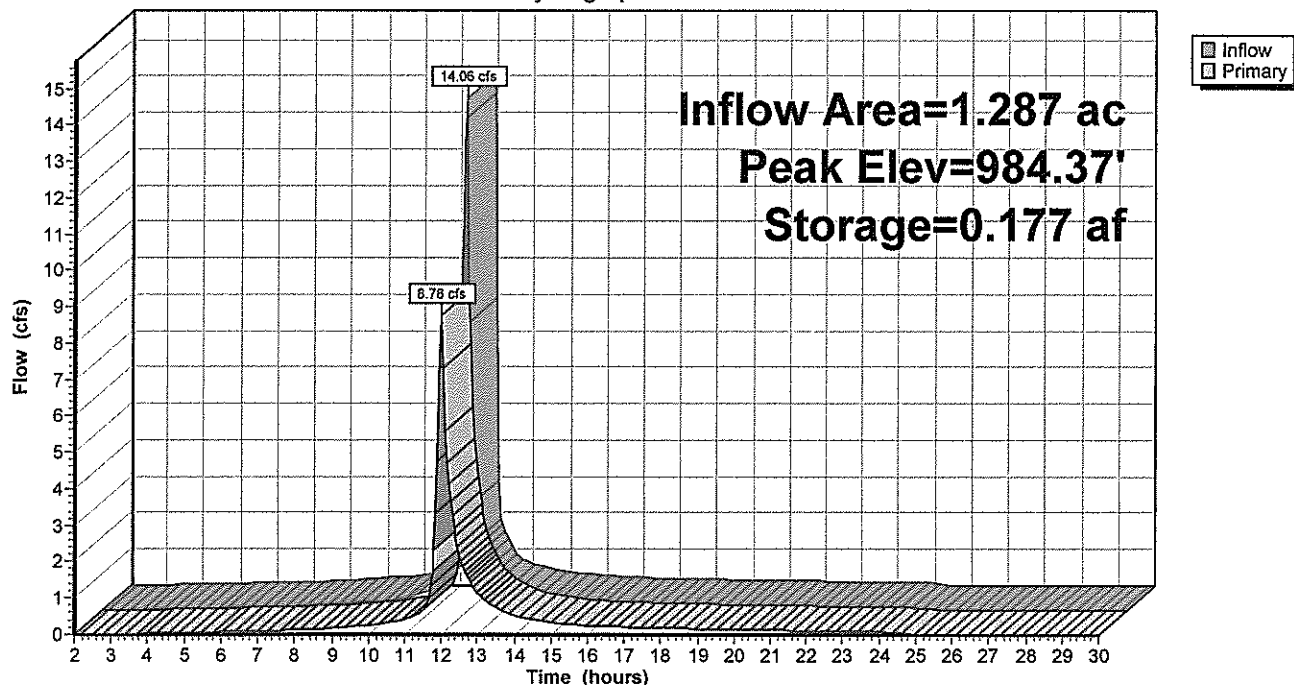
Device	Routing	Invert	Outlet Devices
#1	Primary	982.03'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28) Head (feet) 0.00 1.03 1.03 1.93 1.93 3.00 Width (feet) 0.50 0.50 0.79 0.79 2.50 2.50

Primary OutFlow Max=8.78 cfs @ 12.00 hrs HW=984.37' (Free Discharge)

↑1=Custom Weir/Orifice (Weir Controls 8.78 cfs @ 3.89 fps)

Pond DET1: (new Pond)

Hydrograph



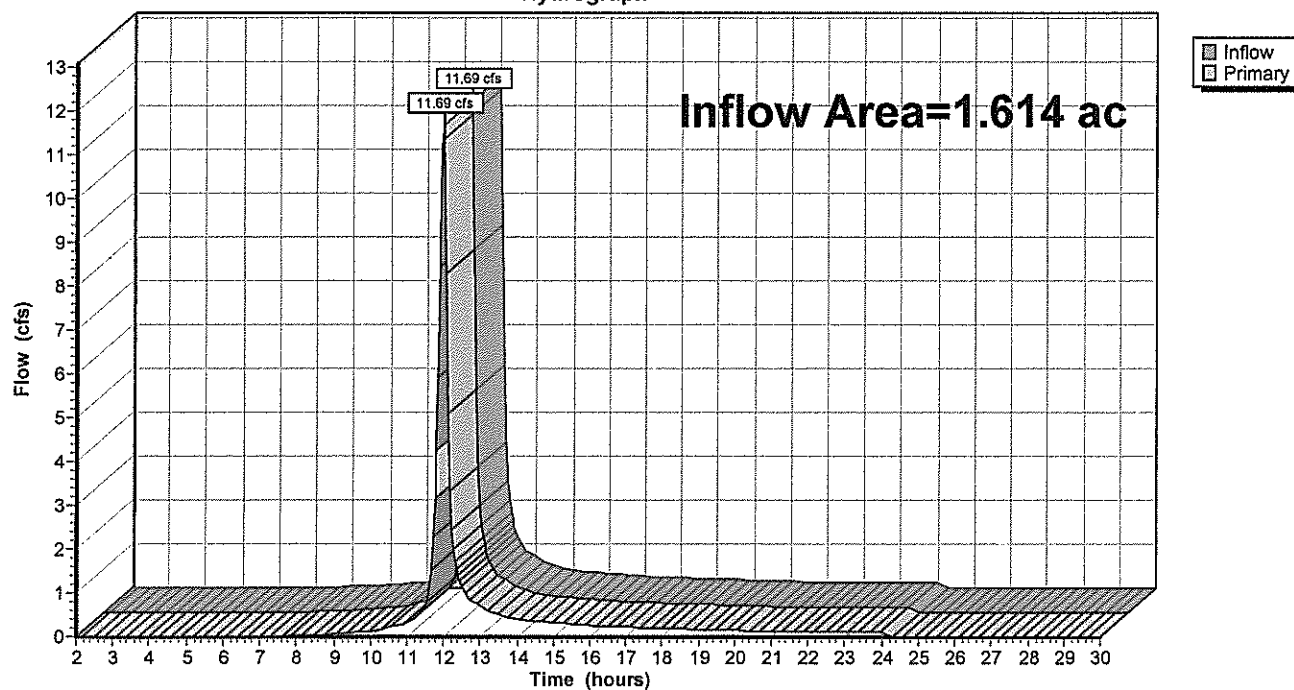
Summary for Link 4E: (new Link)

Inflow Area = 1.614 ac, 0.00% Impervious, Inflow Depth = 4.57"
Inflow = 11.69 cfs @ 11.98 hrs, Volume= 0.615 af
Primary = 11.69 cfs @ 11.98 hrs, Volume= 0.615 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs

Link 4E: (new Link)

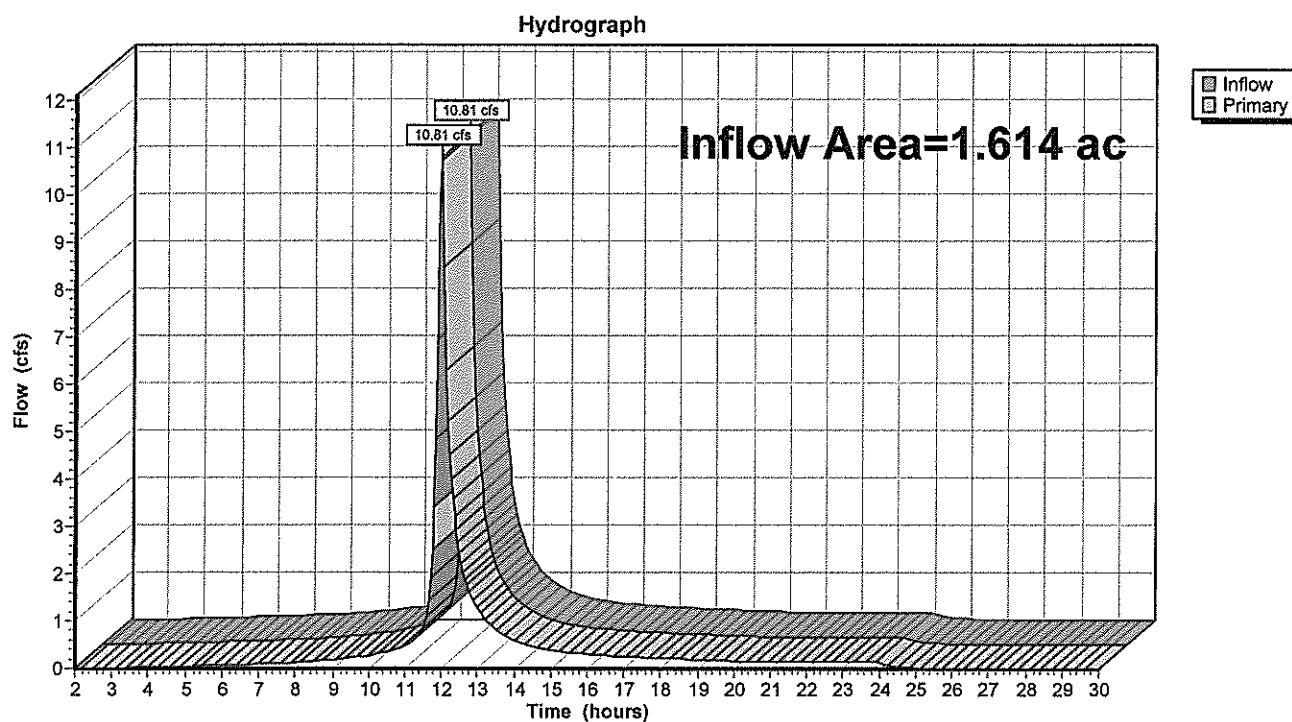
Hydrograph

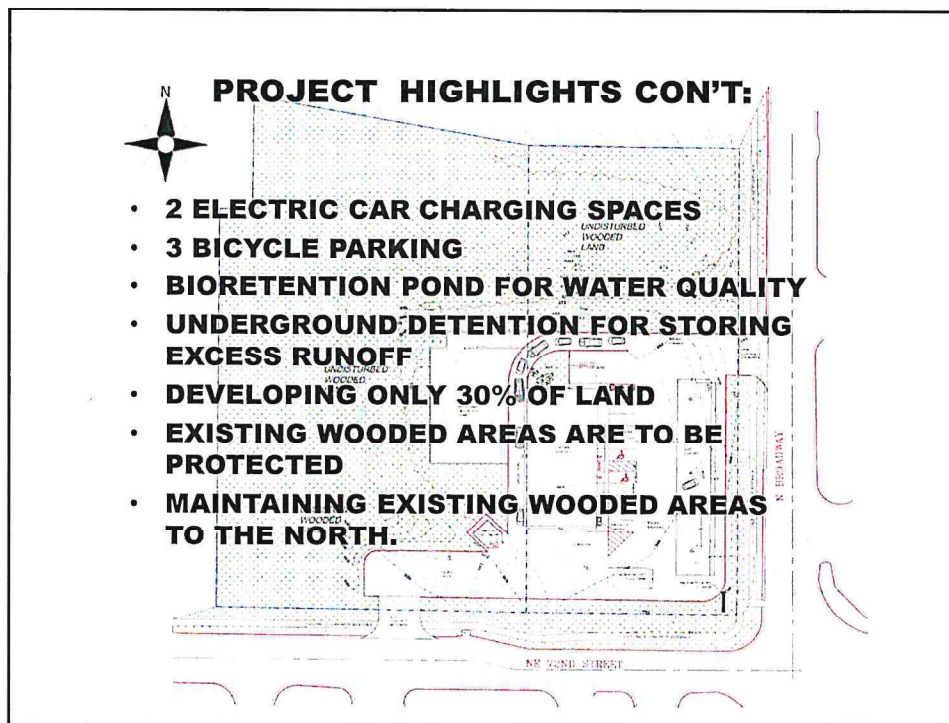
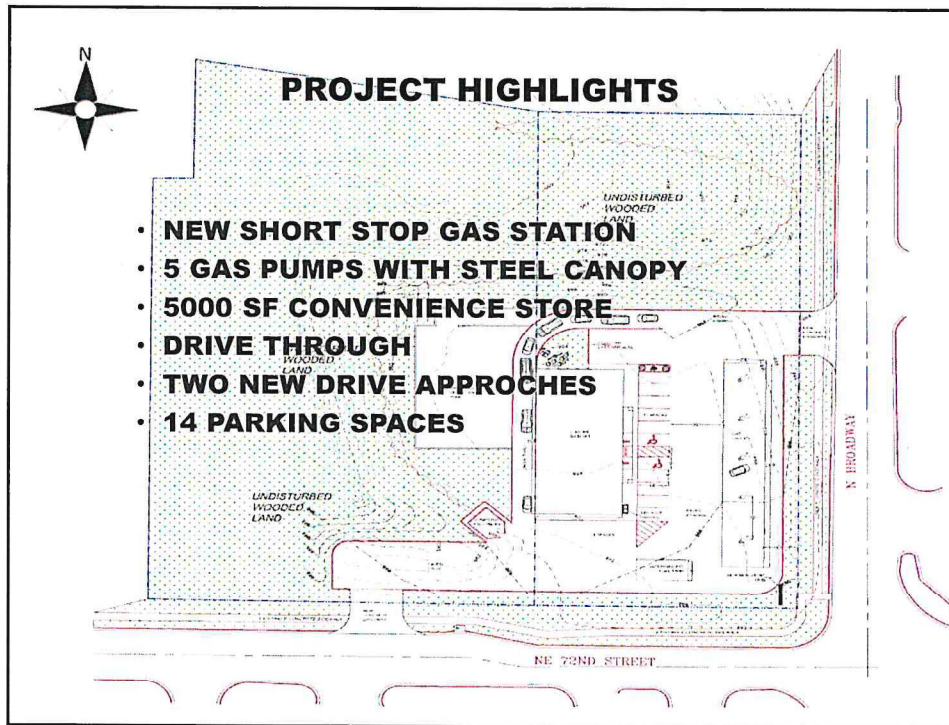


Summary for Link 10L: (new Link)

Inflow Area = 1.614 ac, 54.15% Impervious, Inflow Depth = 6.04"
Inflow = 10.81 cfs @ 11.99 hrs, Volume= 0.813 af
Primary = 10.81 cfs @ 11.99 hrs, Volume= 0.813 af, Atten= 0%, Lag= 0.0 min

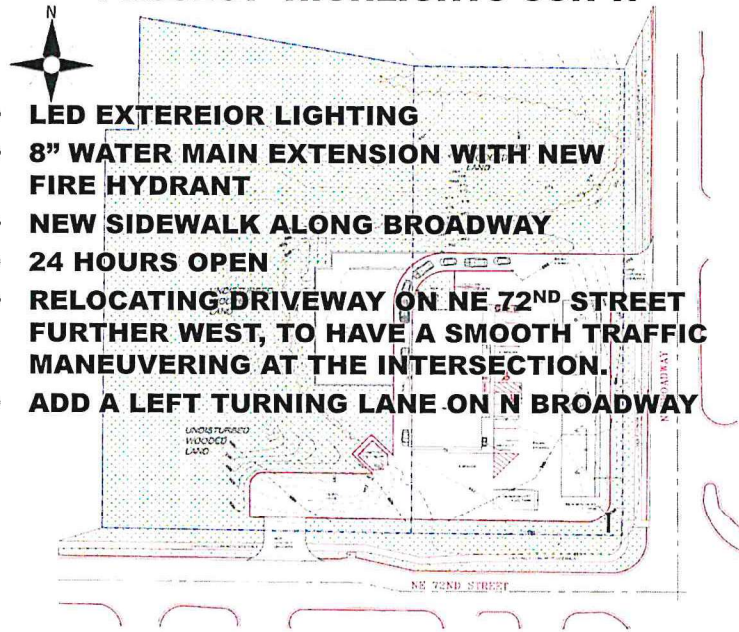
Primary outflow = Inflow, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs

Link 10L: (new Link)



PROJECT HIGHLIGHTS CON'T:

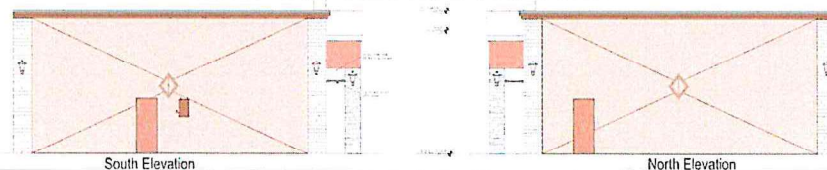
- LED EXTEREIOR LIGHTING
- 8" WATER MAIN EXTENSION WITH NEW FIRE HYDRANT
- NEW SIDEWALK ALONG BROADWAY
- 24 HOURS OPEN
- RELOCATING DRIVEWAY ON NE 72ND STREET FURTHER WEST, TO HAVE A SMOOTH TRAFFIC MANEUVERING AT THE INTERSECTION.
- ADD A LEFT TURNING LANE ON N BROADWAY



C-STORE BUILDING ELEVATIONS



- CONSTRUCTED OF CONCRETE BLOCKS
- METAL BAR JOIST ROOF SYSTEM
- BRICK AND STONE EXTERIOR
- CONCRETE STUCCO ON SIDE AND REAR
- HIGH PARAPET TO SCREEN MECHANICAL UNITS
- LESS THAN 50% GLAZING TO HAVE SIGNAGE
- MATCHING ENCLOSED TRASH DUMPSTER



SITE PLAN RENDERING



BUILDING & CANOPY RENDERING



BUILDING & CANOPY RENDERING



LANDSCAPING HIGHLIGHTS:

- **ONLY 30% AREA DEVELOPED**
- **70% AREA MOSTLY HAVING MATURE TREES TO REMAIN**
- **MAINTAINING EXISTING WOODED AREAS. NOT DISTURBING ANYTHING TO THE NORTH.**

LANDSCAPING HIGHLIGHTS CON'T:

- **BUILT IN IRRIGATION SYSTEM**
- **PLANTING TREES AND SHRUBS ALONG BROADWAY AND 72ND STREET**
- **ALL DISTURBED AREAS SODDED**
- **PLANTING NEW VEGETATION TO THE WEST**

PLANNING COMMISSION
GLADSTONE, MISSOURI
Gladstone Community Center
Monday, May 20th, 2024
7:00 pm

Item 1 on the Agenda: Roll Call.

Present: Kate Middleton
Bill Turnage
Jennifer McGee
Joseph Brancato
Cameron Nave Secretary
Robert Wilson
Steve Beamer Chair
Mike Ebenroth

Absent: Chase Cookson
Brenda Lowe, V-Chair
Kim Murch

Council & Staff Present:

Austin Greer, Assistant City Manager | Community Development Director
Alan Napoli, Community Development Administrator/Building Official
Angie Daugherty, Admin. Assistant
Jean B. Moore, Councilmember
Tina Spallo, Mayor

Item 2 on the Agenda: Pledge of Allegiance.

Chair Beamer led the group in reciting the Pledge of Allegiance to the United States of America.

Item 3 on the Agenda: Approval of the April 1st, 2024 Minutes. Chair Beamer asked if there was a motion to approve the minutes from the April 1st meeting.

Mr. Turnage moved to approve the minutes; Ms. McGee seconded. The minutes were approved, 8-0.

Item 4 on the Agenda: Consideration: On a Site Plan Revision on property located at 7200 N. Broadway.

Applicant: Gerald W. Menefee P.E.

Owner: Mohammad Hafiz

City Council consideration for this project is scheduled for Monday, June 10, 2024.

Mr. Greer read from the staff report:

The applicant is requesting site plan approval for the purpose of constructing a new 5,000 sq. ft. gas station and convenience store located at 7200 N. Broadway. This property is currently vacant and zoned CP-2 which is an appropriate zoning for the proposed use.

This project was proposed in 2023 and denied by the Gladstone City Council. The property owner has made adjustments to the site plan and those adjustments include the following:

- The access point on NW 72nd Street has been shifted west to lineup with the Post Office access point.
- The water quality pond has been moved from the northern side of the property to the western side of the property away from the residential homes located to the north. This basin will be located on the KCMO parcel.
- The wooded area on the northern side of the property will primarily remain untouched.

This project will also incorporate a drive thru lane and window as well as two (2) electric vehicle (EV) charging stations and a commercial bike rack. There will be ten (10) fuel pumps covered by a canopy to serve customers.

The primary exterior building materials used will be brick and stucco.

The landscaping plans show new landscape throughout the property using various trees and shrubs. All disturbed areas will be sodded and irrigated.

A traffic study was conducted by Priority Engineers, Inc. and they provided a summary of their findings.

- "Analysis of unsignalized intersections indicate that they operate with acceptable levels of service both before and after the construction of the proposed development. The signalized intersection at NW 72nd Street and N Broadway Street has an overall level of service that is acceptable both before and after construction of the proposed development. The proposed entrance locations have sufficient sight distance. A left turn lane is warranted for the entrance on N Broadway Street in the PM Peak Hour. Due to geometric constraints of this location, the left turn lane will need to be designed so that it does not interfere with the southbound left turn lane at the signalized intersection with NW 72nd Street. No other improvements are required as a result of this development."
- Given the conclusions and recommendations made by the traffic engineers, City Staff will be requiring the installation and construction of a left turn lane or right-in/right-out for the entrance on N. Broadway at the property owner's expense.
-

City Staff recommends that the following conditions be considered if the Planning Commission and City Council choose to approve this project request:

1. Any and all disturbed areas shall be sodded.
2. All manicured grass and landscaped areas shall be irrigated and maintained in perpetuity.
3. Install a minimum of 20 new shrub plantings adjacent to N. Broadway.
4. Install a minimum of 10 new shrub plantings adjacent to NE 72nd Street.
5. All mechanical equipment on the roof shall be screened from public view by a parapet or approved screening similar in design to the rest of the structure. This must be a minimum of twelve (12) inches above the tallest piece of mechanical equipment.

6. A compliant monument sign shall be used to serve the development. The monument sign will need a minimum of 240 sq. ft. of area landscaping around the sign.
7. All exterior lighting on the site shall be LED and designed to reduce adverse impact on adjoining properties.
8. The dumpster shall be enclosed with materials consistent with the primary building. Specific colors and materials shall be submitted and approved as part of the building permit.
9. Trash service, store deliveries, and gasoline refilling (underground commercial gasoline tanks) shall occur between the hours of 7:00 a.m. to 10:00 p.m.
10. Tractor trailers, storage containers, and other commercial vehicles (including delivery trucks) shall not be parked or stored overnight on the premises.
11. No more than 50% of each glazed window area of the building shall have signage.
12. Hours of operation permitted are 24 hours seven days per week.
13. Install a commercial grade bike rack on-site.
14. Install new curb, gutter, and sidewalk along the property line adjacent to N. Broadway.
15. Preserve the northern wooded tree line as a buffer to the residential neighborhood located to the north along NW 72nd Terrace.
16. Complete a Post-Construction Maintenance Agreement for stormwater facilities.
17. Install a fire hydrant within four-hundred (400) feet of any portion of the building.
18. Extend and loop the 8-inch water main along N. Broadway.
19. Given the project location and that the development extends to property located in Kansas City, Missouri, this development is subject to Kansas City, Missouri approving the improvements on their parcel.
20. The installation and construction of a left turn lane or right-in/right-out for the entrance on N. Broadway at the property owner's expense.

City Staff recommends that the request be **APPROVED** contingent upon the conditions listed above.

Mr. Menefee who is the applicant on the project presented a PowerPoint.

Mr. Menefee stated that this will be a convenience store with five gas pumps, a drive thru, 14 parking spaces, EV charging stations, exterior lighting along the north side, the water main extension and sidewalk, and open 24 hours. They will also add an access drive off of Broadway and NE 72nd St. Only 30% of the area will be developed and the other 70% has mature trees. They will have storage pipes on the northern edge of the site and those will be connected to the water retention pond on the west side of the structure. Thank you.

Ms. Middleton asked what part of this property is in Kansas City.

Mr. Menefee stated the western parcel that has the basin and west side of the driveway.

Mr. Turnage asked who will be in charge of redesigning the drive from Broadway.

Mr. Greer stated that private sector engineers hired by the property owner will likely design the project and submit the designs to city staff for review.

Ms. McGee asked where the retaining wall was going and how tall will it be.

Mr. Menefee stated the wall will be along the tree line and around 10 to 12 feet tall at the tallest point.

Mr. Wilson asked if he could explain the difference between the basin and a sand and oil separator pit.

Mr. Menefee stated it is based on the volume of the water that comes off the site. It is a large area and with a lot of rain fall this goes into the retention pond and the sand filtration is basically the same thing. The filter is made up of primarily tree bark and peat moss.

Mr. Brancato asked how the public is supposed to gain access to the drive thru and whether or not they will have to drive around the back of the building and face N. Broadway or NW 72nd Street. Also, will the drive thru be open for 24 hours as well?

Mr. Menefee stated he isn't sure about the hours that the drive thru will be open but assumes it will be dependent on customer demand. The drive thru comes in at the north side and goes south along the building facing NW 72nd St.

Mr. Beamer asked about approval from Kansas City. Do you all have a status on this?

Mr. Menefee stated they have not brought this project to Kansas City yet as we would like to get permission from the City of Gladstone first.

Mr. Beamer asked if this property has historically been vacant or have there been other approved plans on this site.

Mr. Greer stated yes, a Casey's gas station and a dentistry has been approved on this site historically but neither pursued the actual construction of the projects.

Mr. Beamer welcomed the audience to speak in favor or against the proposed project.

Mr. and Ms. Weatherford who reside at 403 NW 72nd Terrace stated that since there is a Casey's at one end of Broadway and a QuikTrip on the other so why do we need another gas station in the middle of residential? That area is full of residential homes. Will the sales from the Short Stop be mostly gas or alcohol? This is a very dangerous intersection and we are very concerned about traffic and wrecks. Are there plans to look at this intersection?

Ms. Josie Nabavian who resides at 400 NW 72nd Terrace asked what has changed from the last meeting? What is going to be the traffic pattern? There is a lot of traffic in that area. With the exit off of Broadway into the gas station, will this make a traffic delay?

Mr. Greer stated that a traffic study has been completed and the study indicates a left turn lane is warranted traveling northbound. Staff is requiring that the property owner add a left turn lane or a right-in/right-out to help mitigate traffic.

Mr. Tyson who resides at 308 NW 76th St. asked when you mention right-in and right-out will this be right lane going into the gas station parking lot and right turn only coming out of the parking lot on N. Broadway?

Mr. Greer stated yes sir.

Mr. Tyson stated that the city cannot control the traffic off of 76th St. or 72nd St.

Mr. Greer stated that the design of the right-in and right-out will be built high enough that most people will try not to drive over it.

Mr. Tyson brought up traffic control and that he doesn't think the police department does enough to stop people from speeding on Broadway. This property has been vacant for so long and I don't understand why they want to put a gas station there.

Ms. Vicki Marshall resides at 401 NW 72nd Terrace and her concern is that she feels like this project will be in her backyard. What if they have a gas leak from the tanks? When they first moved here they were told that it was zoned for an office building and that was in 1992.

Mr. Menefee stated that it is a requirement that they have a containment system that has a double wall tank that is surrounded by a plastic liner.

Ms. Taylor Sherrill who resides at 6305 N. Bales Avenue stated that this project from an environmental perspective does not seem to be compatible with the recent comprehensive plan and that this project does not fit the location.

MOTION: By Ms. Middleton, second by Mr. Ebenroth to consider a Site Plan Revision located at 7200 N Broadway.

Vote: Mr. Wilson	Yes
Mr. Brancato	Yes
Mr. Turnage	Yes
Ms. Middleton	No
Chair Beamer	Yes
Ms. McGee	Yes
Mr. Nave	Yes
Mr. Ebenroth	Yes

The motion carried. (7-1)

Item 5 on the Agenda: Communications from the City Council

Councilmember Jean Moore wanted to welcome everyone to the new space and Mr. Bob Wilson to the Planning Commission. She also thanked the residents for their participation tonight.

Item 6 on the Agenda: Communications from the City Staff

Mr. Greer welcomed Mr. Wilson to the Commission as well. With the storms that happened last night the city will be offering free brush disposable at Public Works today through Friday. City Hall will be closed next Monday for Memorial Day and Food, Art, and Drink will be at Linden Square on June 1st. Also, there will be no Planning Commission meeting on Monday, June 3rd.

Item 7 on the Agenda: Communications from the Planning Commission Members

Mr. Beamer welcomed Mr. Wilson to the Planning Commission and asked Mr. Wilson to tell them a little about himself.

Mr. Wilson stated that he is an architect by trade and is leading an architectural firm here in Kansas City. I was also on the Capital Improvements Committee and am very excited to join the Planning Commission and help the community.

Mr. Turnage wanted to thank the Public Works Department for sponsoring the beautification event.

Item 8 on the Agenda: Adjournment

Chair Beamer adjourned the meeting at 7:39 pm.

Respectfully submitted:

Steve Beamer, Chair

Approved as submitted _____

Angie Daugherty, Recording Secretary

Approved as corrected _____

DEVELOPMENT APPLICATION



CITY OF GLADSTONE
7010 N HOLMES STREET
GLADSTONE, MISSOURI 64118
PHONE: 436-4110 FAX: 436-2228

File #:
Application Date: 04/01/2024
PC Date: _____
CC Date: _____

Application Type:

- | | |
|--|---|
| <input type="checkbox"/> (PH) Special Use Permit (\$500) | <input type="checkbox"/> (PH) Right-of-Way Vacation (\$200) |
| <input type="checkbox"/> (PH) Zoning Change (\$500) | <input type="checkbox"/> (PH) Variance – BZA (\$200) |
| <input type="checkbox"/> (PH) Site Plan Revision (\$500) | <input type="checkbox"/> Final Plat/Replat (\$75) |

Address of Action: 400 NE 72ND STREET

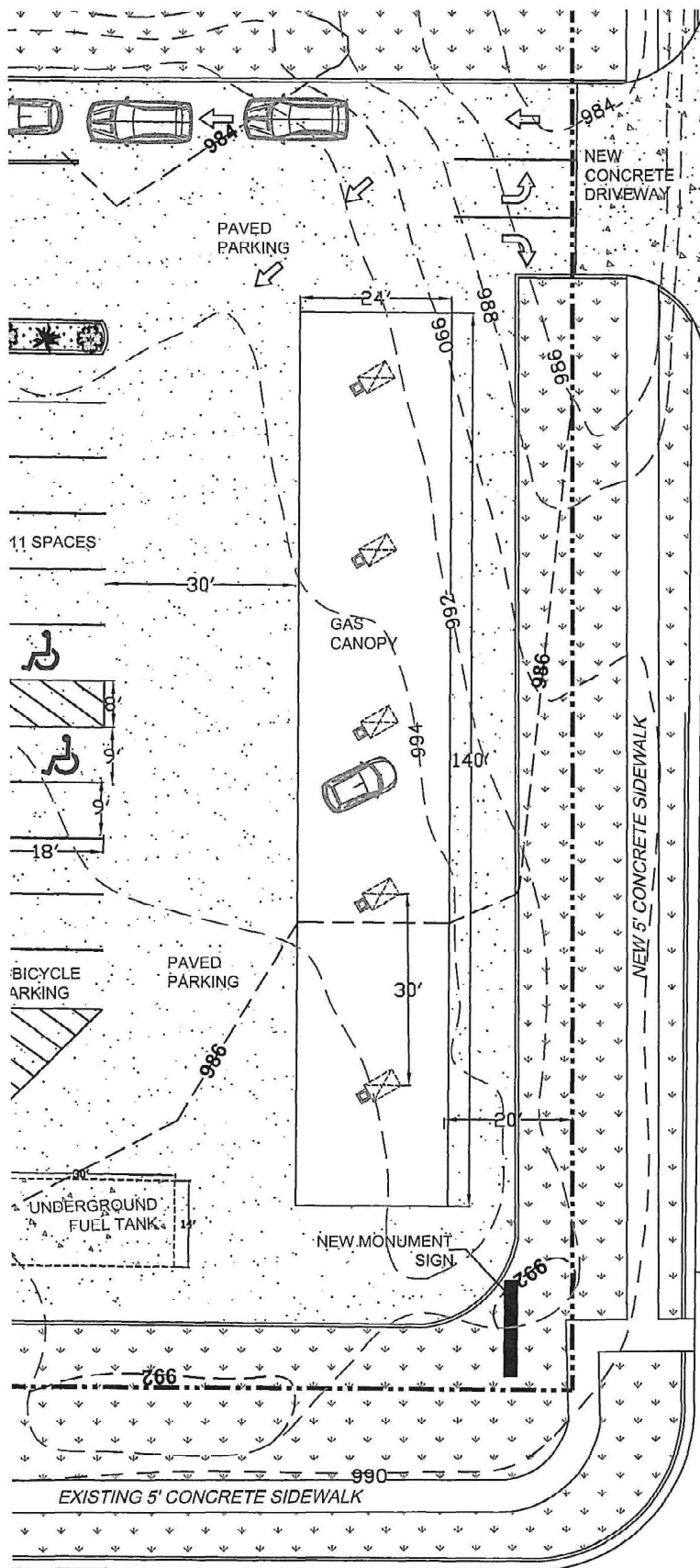
Legal Description: BEG SW COR LT 12 WILLOW CREEK E146, S340,
Attach under separate cover if SW21.21, W138, N TO POB
needed.

Proposed Change: CONSTRUCTION OF NEW GAS STATION WITH 5000
SF CONVENIENCE STORE AND 5 GAS DISPENSERS
AND DRIVE THRU

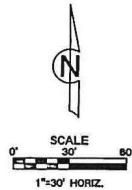
Applicant/Property Owner Information:

- ☐ Applicant/Engineer GERALDW MENEFEE, P.E.
Company KAM DESIGN GROUP LLC
Address 9000 E BANNISTER ROAD, KANSAS CITY MO 64134
Phone 8167972065 Fax: _____ E-Mail: kamdesign@aol.com
- ☐ Property Owner (if different than applicant) MOHAMMAD HAFIZ
Company _____
Address 1121 SW BLAZINGSTAR CT., LEE'S SUMMIT MO 64081
Phone 816 7861622 Fax: _____ E-Mail: mhafiz103@yahoo.com
- ☐ Architect DARRYL W HAWKINS AIA
Company INNOVATIVE DESIGN & RENOVATION
Address 8011 PASEO SUITE 201, KANSAS CITY, MO 64131
Phone 8164052159 Fax: _____ E-Mail: arkitec35@aol.com
Please indicate in one box above which person is to be the contact.

Applicant's Signature *Mohammad Hafiz* Date 4/1/24



Recorded in Clay County, Missouri
 Date and Time: 08/12/2010 at 08:58:37 AM
 Instrument Number: 2010027034
 Book: M Page: 12
 Instrument Type: SURV
 Page Count: 1
 Recording Fee: \$6800.00
 Grantor: 72ND & BROADWAY
 Grantee: 72ND & BROADWAY
 Robert T. Brock, Recorder



PLAN LEGEND

SURVEY MARKERS

- FOUND SECTION CORNER (MONUMENTATION AS NOTED)
- FOUND PROPERTY CORNER (MONUMENTATION AS NOTED)
- SET 1/2" IRON BAR WITH PLASTIC CAP
- BENCHMARK
- OK GAS LINE MARKER
- SMH SANITARY MANHOLE
- UTILITY LINES
- E66H — ELECTRIC, OVERHEAD
- 100 — INDEX CONTOURS
- 100 — INTERMEDIATE CONTOURS

ELECTRIC

- GUY GUY ANCHOR
- LP LIGHT POLE
- PP POWER POLE

STORM

- CI CURB INLET
- SMH STORM MANHOLE

WATER

- WV WATER VALVE

TRAFFIC

- TSP TRAFFIC SIGNAL POLE
- TSC TRAFFIC SIGNAL CONTROLS
- TSP TRAFFIC SIGNAL VAULT

TELEPHONE

- FOM FIBER OPTIC MARKER

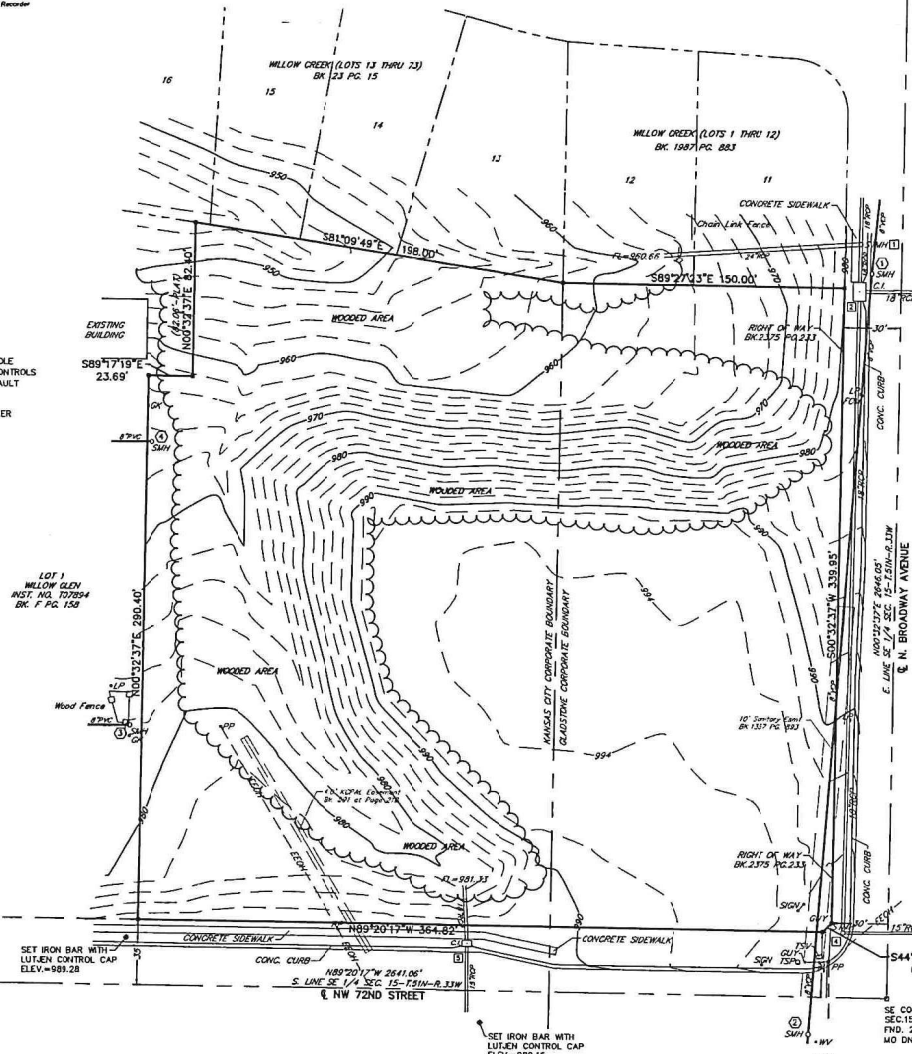
STORM INVERTS

- 1 TOP MH-986.66
FL IN S-971.16
FL IN N-976.06
FL OUT W-961.96
- 2 TOP CI-980.45
FL IN S-972.80
FL IN E-976.65
FL OUT N-973.45
- 3 TOP CI-980.45
FL OUT W-973.96
- 4 TOP MH-996.00
FL IN E-985.60
FL OUT N-982.70
- 5 TOP CI-988.79
FL IN S-983.69
FL OUT N-982.70

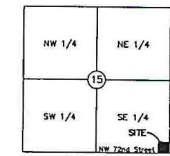
SANITARY INVERTS

- 1 TOP SMH-980.17
FL IN S-975.17
FL OUT W-974.97
- 2 TOP SMH-996.38
FL IN S-985.38
FL OUT N-984.38
- 3 TOP SMH-978.32
FL OUT W-966.92
- 4 TOP SMH-966.74
FL OUT W-955.24

LOT 1
MILLOW CREEK
NOTED NO. 77094
BK. F PG. 150



NE CORNER SE 1/4
 SEC.15-T.51N-R.33W
 FND. 2" GAS PIPE
 MO DNR. DOC NO. 600-51378



Sec. 15, Twp. 51 N., Rge. 33 W.
 (N.T.S.)

Property Description:

A tract of land in the Southeast Quarter of Section 15, Township 51 North, Range 33 West of the 5th Principal Meridian in Kansas City and Gasstone, Clay County, Missouri, being bounded and described as follows: Beginning at the Southeast corner of Lot 11, MILLOW CREEK (LOTS 1 THRU 12), a subdivision of land in said Clay County, thence South 00°32'37" West, along the West right-of-way line of N. Broadway Avenue, as now established, 339.95 feet; thence South 44°27'23" West, continuing along said West right-of-way line, 6.92 feet to a point on the North right-of-way line of NW 72nd Street, as now established; thence North 89°27'23" East, along said North right-of-way line, 364.82 feet to the Southeast corner of MILLOW CREEK, a subdivision of land in said Clay County, Missouri; thence North 00°32'37" East, along the East line of said MILLOW CREEK (LOTS 1 THRU 12); thence South 89°27'23" East, along the South line of said land in said Clay County, thence South 81°09'49" East, along the South line of said MILLOW CREEK (LOTS 1 THRU 12); thence South 89°27'23" East, along the South line of said MILLOW CREEK (LOTS 1 THRU 12), 150.00 feet to the Point of Beginning. Containing 125,666 square feet or 2.96 acres, more or less.

SURVEYORS NOTES:

1. Property information referencing this survey was taken from the Commitment for Title Insurance Report, issued by Integrity Land Title Company, Inc., Firm File No. KC-IT-7089-10, with an effective of May 14, 2010 at 8:00 a.m.
2. Bearings used herein are based on the Missouri State Plane Coordinate System, NAD 1983, West Zone. Vertical Datum is based on the North American Vertical Datum of 1988 (NAVD 88).
3. The underground utilities shown herein have been located from field survey information, existing drawings and marking provided by Missouri One Call System, Inc. The surveyor makes no guarantee that underground utilities shown comprise all such utilities in the area, either in service or abandoned. The surveyor further does not certify that they are located as accurately as possible from information available at the time of survey. The surveyor has not physically located the underground facilities.
4. Field work was completed in May 2010.

SE CORNER SE 1/4
 SEC.15-T.51N-R.33W
 FND. 2" BRASS CAP
 MO DNR. DOC NO. 600-51391

CERTIFICATION

I hereby certify that this survey was prepared by me or under my direct personal supervision and that I am a duly licensed Professional Land Surveyor under the laws of the State of Missouri and that this survey was performed in accordance with the requirements of the current Missouri Minimum Standards for Professional Land Surveyors.

JASON S. ROBERTSON, L.S.
 DATE: 6-2-10

BOUNDARY / TOPOGRAPHIC SURVEY
 72ND AND BROADWAY
 SEC. 15 - T51N - R33W
 KANSAS CITY, CLAY COUNTY, MISSOURI

DATE OF SURVEY: 05-02-10

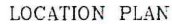
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Surveyed By: ZB / KB
 Reviewed By: BAL
 Drafted By: JR
 Lutjen Project No.: 10081



1301 Burlington, #103
 North Kansas City, MO 64116
 816.467.4225
 816.467.1933 fax
 www.lutjen.com

Sheet No.:
 1 of 1



400 NE 72ND STREET, GLADSTONE, MISSOURI



BEG SW COR LT 12 WILLOW CREEK E146, S340, SW21-21, W138, N
TO POB

BEG SE COR LT 13 WILLOW CRK, S TO NL NW 72ND ST, W210,
N290.4, E23.69, N82.06, SELY TO POB

 EXISTING/PROPOSED CONCRETE SURFACE
 GRASS COVER
 BUILDING OUTLINE
 PROPERTY LINE
 FIRE HYDRANT
 STREET CENTER LINE



EXISTING ZONING	CP1 (GLADSTONE)
PROPOSED ZONING	CP1
TOTAL LAND	1.19 ACRES
LAND AREA FOR EXISTING & PROPOSED STREET RIGHT-OF-WAY	NONE
NET LAND AREA OR ACRES PROPOSED USE	1.19 ACRES
BUILDING HEIGHT	M - GAS STATION WITH 5,000 SFT CONVENIENCE STORE SINGLE STORY BUILDING 11 FEET C-STORY A 5,000 SFT STORE
GROSS FLOOR AREA / BUILDING COVERAGE / FLOOR AREA RATIO / PARKING SPACES REQUIRED	0.10 % 24 SPACES PER 1000 SFT OF RETAIL SPACE (13 SPACES) 14 SPACES PLUS TWO ELECTRIC CAR CHARGING INCLUDING 1 ACCESSIBLE SPACE
PARKING SPACES PROVIDED	24 SPACES
BICYCLE PARKING REQUIRED	3 BICYCLE SPACES
BICYCLE PARKING PROVIDED	3 BICYCLE SPACES WITH 2 LONG TERM SPACE
BUSINESS START DATE	SPRING 2024
EASEMENTS	NONE
HOURS OF OPERATION	24 HOURS
EXISTING PARKING LOT	CONCRETE/ASPHALT COVERED
PROPOSED PARKING LOT	CONCRETE PAVEMENT

PLEASE SEE ELEVATION PLANS THAT SHOW THE BUILDING EXTERIORS

DEVELOPER
MPS CONTRACTING LLC
14926 BENSON STREET
OVERLAND PARK, KS 66221

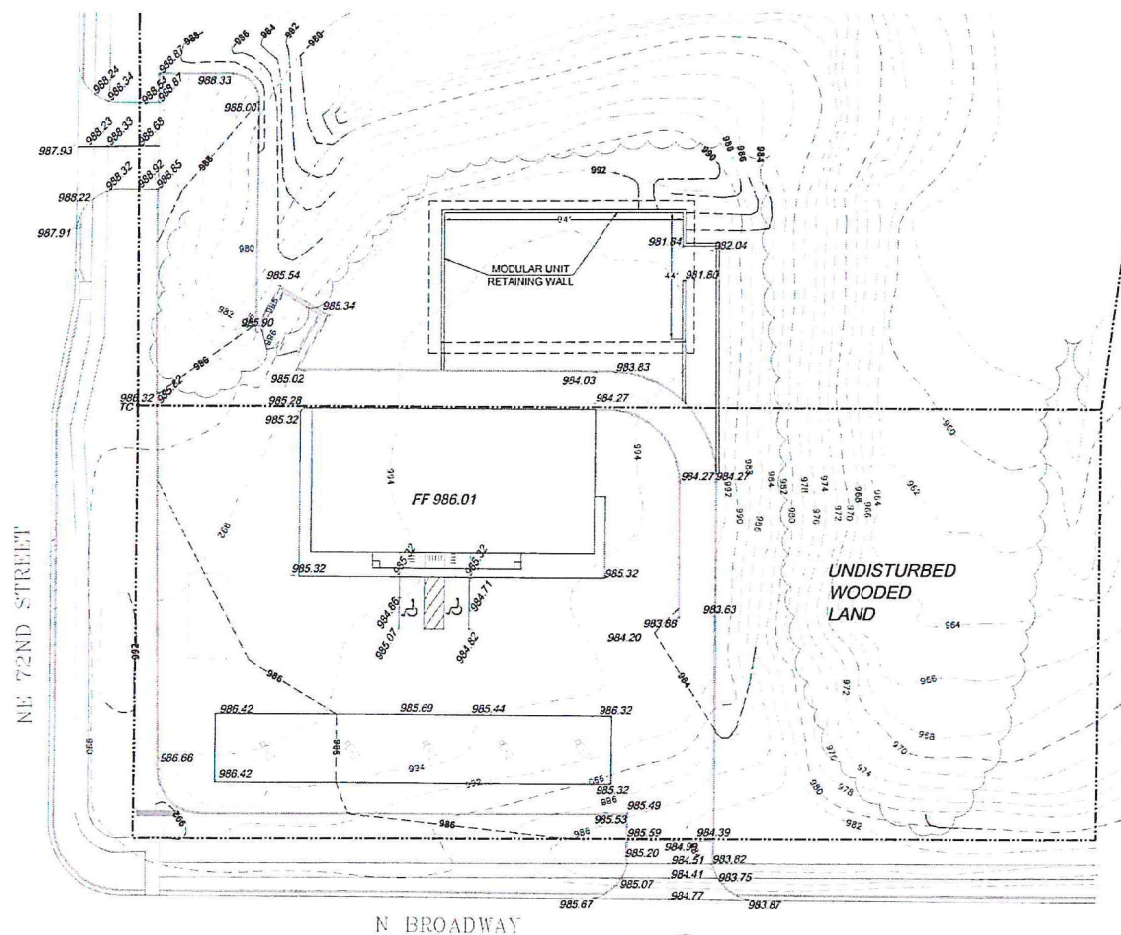
No.	Description
1	SITE PLAN
2	FLOOR PLAN & DETAILS
3	BUILDING ELEVATIONS
4	BUILDING ELEVATION RENDERING
5	GRADING PLAN
6	DETAILS SHEET I
7	DETAILS SHEET II
8	UTILITY PLAN
9	ELECTRICAL PHOTOMETRIC PLAN
10	LANDSCAPING PLAN



400 NE 72ND STREET
GLADSTONE, MISSOURI

Project number	2023-109
Drawn by	KRB
Checked by	GWM

SHEET 1



LEGEND

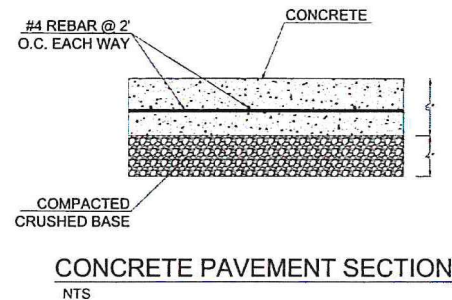
- BUILDING OUTLINE
- PROPERTY LINE
- 809.92 SPOT ELEVATIONS
- 809.92 TOP OF CURB ELEVATION
- 809.42 TOP OF PAVEMENT ELEVATION
- - - EXISTING CONTOUR
- - - PROPOSED CONTOUR

GRADING PLAN



GENERAL NOTES:

1. THE CONTRACTOR SHALL NOTIFY THE ENGINEER OF ANY OBSERVED DISCREPANCIES IN DIMENSIONS, DETAILING, OR OTHER ITEMS AS SHOWN ON THE PLANS OR SPECIFIED PRIOR TO PROCEEDING WITH WORK RELATED TO SAID DISCREPANCIES.
2. ALL WORK SHALL BE DONE IN ACCORDANCE WITH LOCAL CODES.
3. CONTRACTOR SHALL INCLUDE ALL LABOR, MATERIAL, AND EQUIPMENT TO PROVIDE COMPLETE AND FUNCTIONING INSTALLATIONS, AND ALL MATERIAL AND EQUIPMENT SHALL BE NEW UNLESS OTHERWISE SPECIFIED.
4. ACCEPTANCE OF WORK SHALL BE SUBJECT TO OWNERS REPRESENTATIVE APPROVAL OF WORK IN PLACE AS WELL AS SHOP DRAWINGS AND SAMPLE OF MATERIALS AND EQUIPMENT WHICH SHALL BE CHECKED BY CONTRACTOR BEFORE SUBMITTAL.
5. PROTECT ALL EXISTING UTILITIES ALONG THE SOUTH FOR FUTURE USE OF THE NEW BUILDING.
6. REMOVE ALL EXISTING PAVEMENT AND RESURFACE THE PARKING AREA WITH 6" CONCRETE PAVEMENT PLEASE FOLLOW THE DETAIL SHOWN ON THIS SHEET. THE TANK AREA SHALL BE PAVED WITH 8" CONCRETE PAVED WITH REINFORCEMENT.
7. INSTALL NEW DRIVEWAY ALONG THE WEST ACCESS ROAD. NEW DRIVE APPROACHES SHALL BE CONSTRUCTED PER KCMO STANDARD COMMERCIAL DRIVEWAY DRAWING. CONSTRUCT ADA COMPLIANCE ACCESSIBLE RAMPS ON EACH SIDE OF NEW DRIVEWAY.



Date	03/09/24
Drawn by	KRB
Checked by	GWM
Submitted for Owner Approval	
By	
Date	



Design Group LLC
9000 E. Bonner Road
Suite 100
Kansas City, Missouri 64114
(816) 797-2005

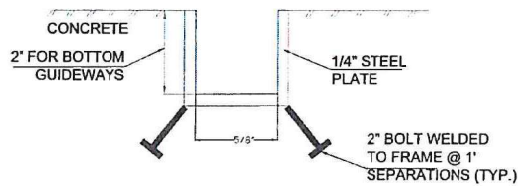
SHORT STOP GAS STATION PROJECT

400 NE 72ND STREET
GLADSTONE, MISSOURI

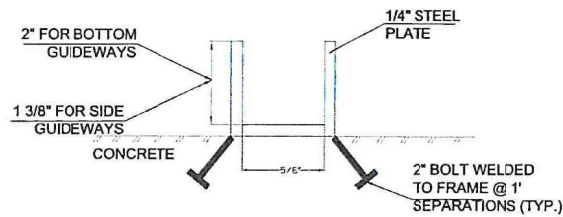
GRADING PLAN

Project Number: 2023-109
Drawn by: KRB
Checked by: GWM

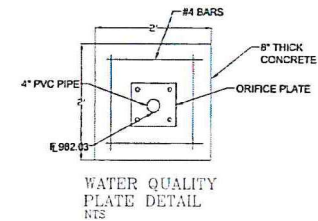
SHEET 5



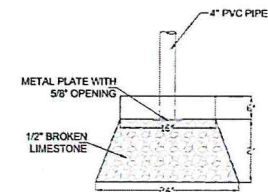
BOTTOM FRAME RESTRAINER FOR ORIFICE PLATE
NTS
DETAIL "C"



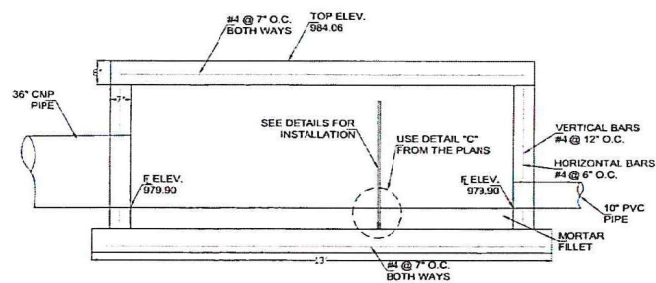
SIDE FRAME RESTRAINER FOR ORIFICE PLATE
NTS
DETAIL "D"



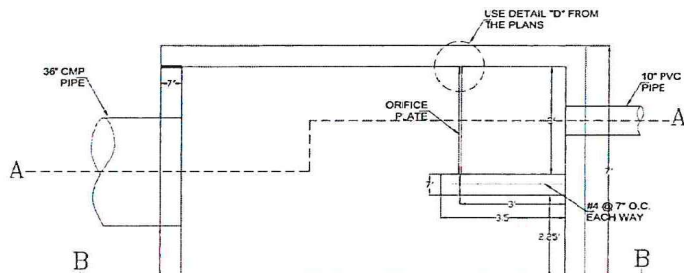
WATER QUALITY
PLATE DETAIL
NTS



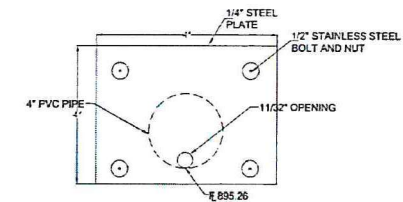
OUTFALL FOR WATER
QUALITY BASIN
NTS



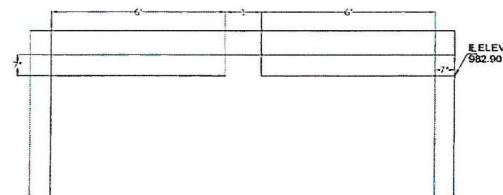
SECTION A-A



STRUCTURE PLAN VIEW

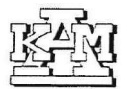


WATER QUALITY DRAIN OUTLET DETAIL
NTS



SECTION B-B

DATE	07/10/2023
DESCRIPTION	REVISION FOR CANTILE APPROVAL
BY	



Design Group LLC
3000 E. Delaware Road
Suite 100
Kansas City, Missouri 64134
(816) 797-1245

SHORT STOP GAS STATION
PROJECT

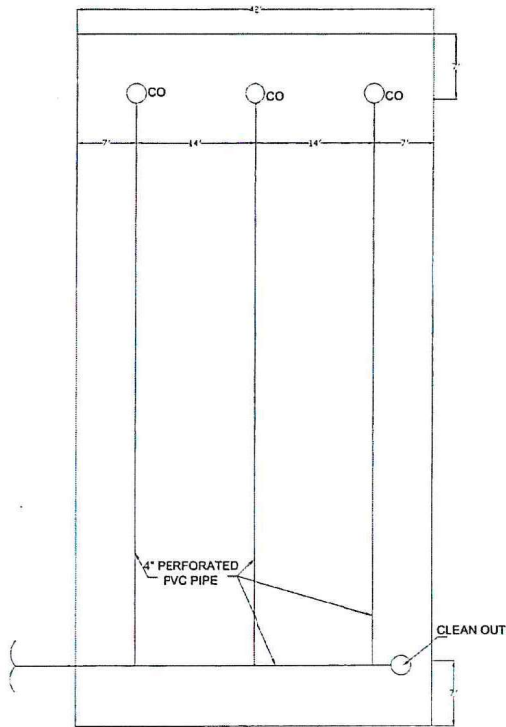
400 NE 72ND STREET
GLADSTONE, MISSOURI

DETAILS SHEET

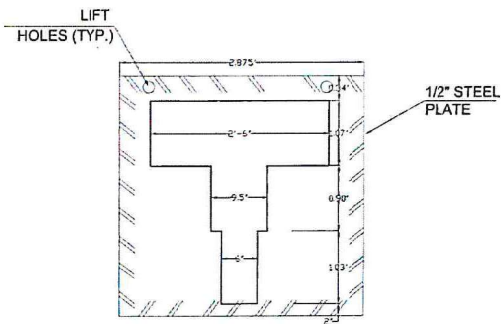
Project Number 2023-109
Drawn by KRB
Checked by GWM



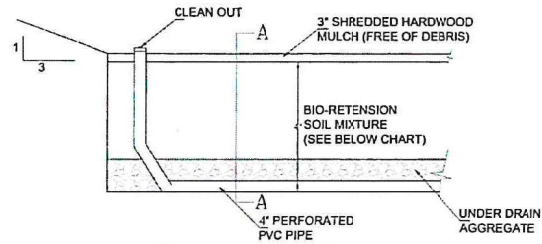
SHEET 6



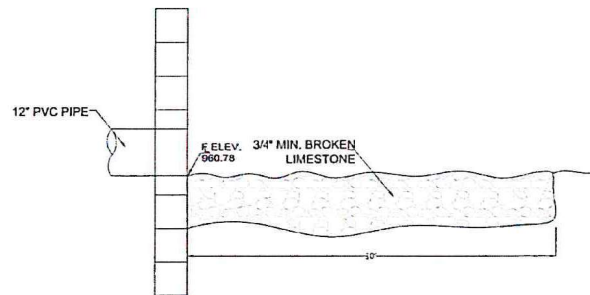
4" PVC PIPE PLAN FOR BIORETENSION BED
NTS



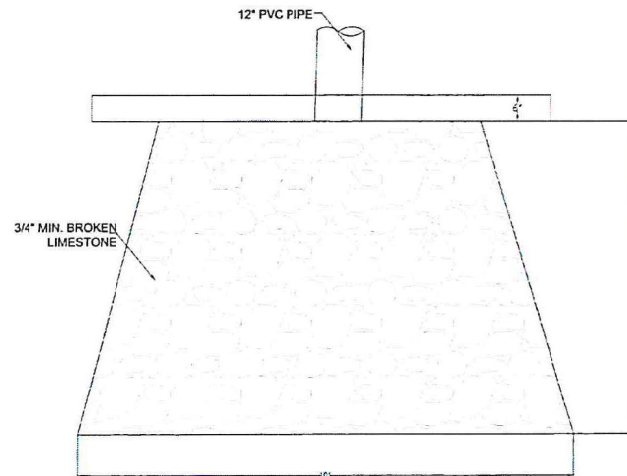
ORIFICE PLATE FOR DETENTION OUTFLOW
NTS



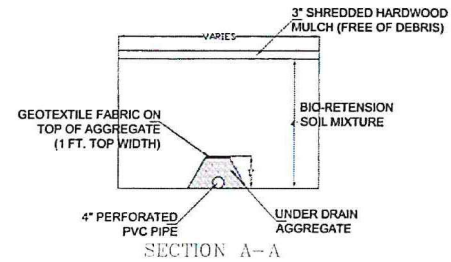
BIO-RETENSION BASIN TYPICAL X-SECTION
NTS



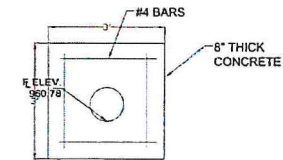
SECTION VIEW
NTS



OUTFALL FOR WATER
QUALITY BASIN
NTS



SECTION A-A



DETENTION DISCHARGE
PLATE DETAIL
NTS

BIO-RETENSION SOIL MIXTURE

COMPONENTS	RATIO BY VOLUME
FILTER SAND	70% (+/- 3%)
COCONUT COIR FIBER	20% (+/- 2%)
HIGH CARBON WOOD ASH	10% (+/- 1%)



DATE	DESCRIPTION	QUANTITY	ON ORDER	REVISION
07/05/23				



K&M
Design Group LLC
9000 E. Bonhomme Road
Suite 100
Kansas City, Missouri 64114
(816) 790-2000

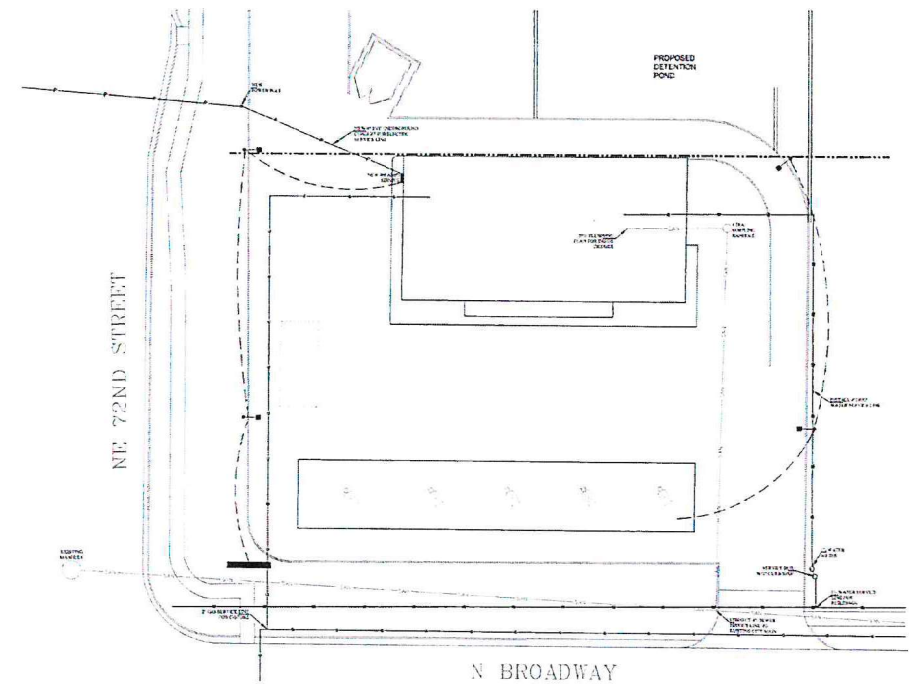
SHORT STOP GAS STATION PROJECT

400 NE 72ND STREET
GLADSTONE, MISSOURI

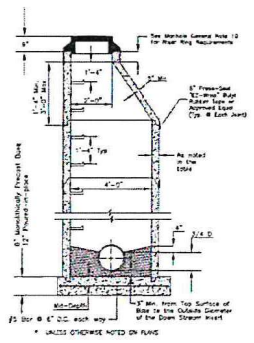
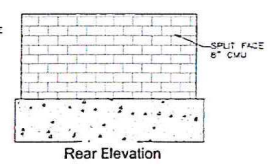
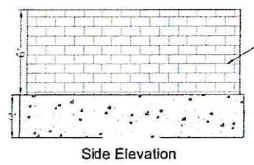
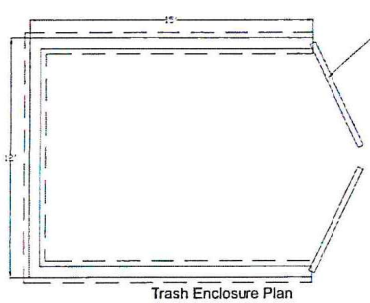
DETAILS SHEET II

Project Number: 2023-109
Drawn by: KRB
Checked by: GWM

SHEET 7

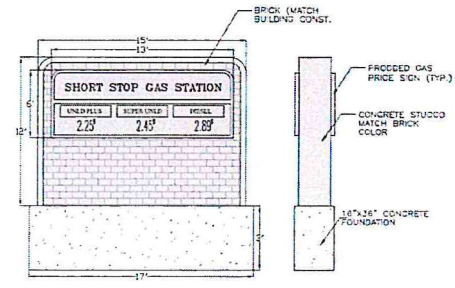


- LEGEND**
- BUILDING OUTLINE
 - PROPERTY LINE
 - WATER SERVICE LINE
 - GAS SERVICE LINE
 - SANITARY SERVICE LINE
 - ELECTRICAL SERVICE LINE
 - UNDERGROUND CONDUIT FOR LP'S

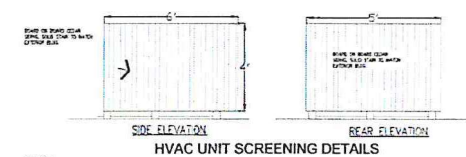


- MANHOLE GENERAL NOTES**
- All manhole rings to be placed in cement or in press to be subsequently poured shall have manhole manhole bearing surfaces and shall comply with Class B as established in ASTM A-442.
 - The inside diameter of the manhole shall be 4'-0" for pipe diameter from 18" thru 24" and shall be 2'-0" for pipe diameter from 27" thru 36". In addition, the pipe diameter (ID) of manholes up to 20 feet deep shall be 4'-0", ID shall be 2'-0" for depths up to 25 feet and ID shall be 4'-0" for depths exceeding 25 feet unless otherwise noted on the plans.
 - All manhole bases (pre-cast or poured-in-place) shall have No. 5 reinforcing bars placed on 6" centers both ways.
 - All standard manhole rings and covers to be Dwyer (D-20-22), Harsco (H-20-22) (frame) and H-20-22 (cover), or approved equal. All manhole rings to covers shall be shown to be equal. An extra payment for furnishing reinforcement and cover is shown in plans will not be made, but shall be considered as auxiliary to the item, "Standard Manhole".
 - Standard manhole steps to be steel core, plastic coated steps DWA, Inc. No. P21-PR, P22-PR, or approved equal.
 - Manhole girth adjustment diameter is 8". Minimum ultimate thickness for precast concrete girth adjustment ring is 4".
 - Reinforcement in all precast sections shall equal or exceed ASTM C-478 specifications.
 - Butyl material to be used at all precast sections, joints. Gaskets may be used for joints below the cone section, but the cone section itself shall not have gasket joints.
 - Riser Rings
 - A. Manholes in Plaster: The thickness of the recycled rubber riser rings shall not be less than one (1) inch nor greater than four (4) inches. If the required thickness of riser rings exceeds 4 inches, a 4-inch or 6-inch precast concrete riser ring shall be installed between the rubber riser ring and the cone. Riser rings may be used up to 4 inches or 6 inches. The manhole riser rings shall be spaced to match the slope of the existing or proposed ground at the manhole. The joints between the cone, rubber riser rings, and casing shall be sealed with the manufacturer-specified sealant.
 - B. Recycled Riser in Plaster: All manholes shall be provided with riser rings underneath the existing riser shown on drawings. All manhole riser rings shall be installed on top of the existing riser. The riser rings shall be spaced to match the slope of the existing or proposed ground at the manhole. The joints between the cone, rubber riser rings, and casing shall be sealed with the manufacturer-specified sealant.
 - C. Brick and mortar adjustments will not be allowed.

4\"/>




NOTE:
THE CONTRACTOR SHALL APPLY SEPARATELY TO THE PERMIT DIVISION FOR SIGN PERMIT.



NOTE:
THE HEIGHT OF THE SCREENING APPARATUS SHALL BE AT LEAST 12\"/>





Design Group LLC
 9060 E. Bonanza Road
 Suite 100
 Kansas City, Missouri 64134
 (816) 797-2000

SHORT STOP GAS STATION PROJECT

**400 NE 72ND STREET
GLADSTONE, MISSOURI**

UTILITY PLAN

Project number: 2003-109
 Drawn by: KRB
 Checked by: GWM

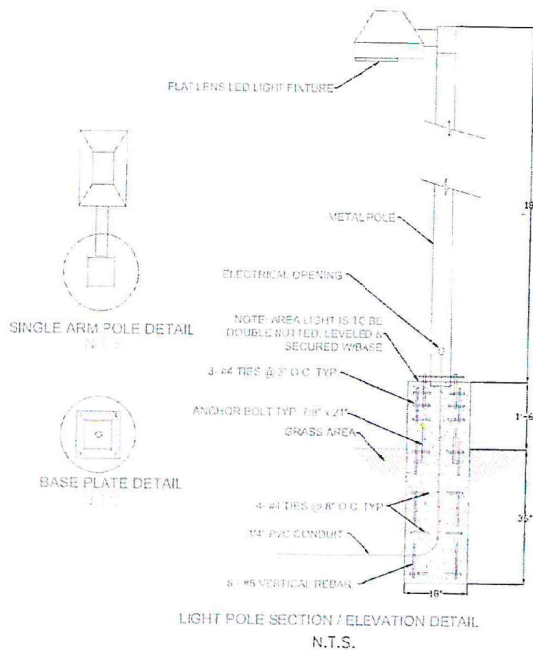
SHEET 8

PLAN NOTES:

1. ROUTE 120V HOME RUN BELOW GRADE TO QUAZITE BOX SHOWN ON PLANS. ASSUMED VOLTAGE USED TO DETERMINE VOLTAGE DROP AND WIRE SIZES IS 120V, 1-PHASE.
2. PARKING LOT LIGHT WITH STEEL POLE LIGHT AND CONCRETE FOUNDATION REFERENCE LIGHT FIXTURE SPECIFICATION THIS SHEET.
3. ASSUMED LOCATIONS OF CONDUIT ENTRY INTO BUILDING FOR SITE LIGHTING. REFER TO BUILDING ELECTRICAL ENGINEERING PLANS AND BUILDING ELECTRICAL ENGINEER FOR UPDATED LOCATIONS OF CONDUIT ROUTING INTO THE BUILDING.
4. LIGHTING CONTROLS AND CONNECTIONS, PROVISIONS FOR ELECTRICAL POWER, AND CONDUIT ROUTING INTO BUILDING ARE NOT INCLUDED WITHIN THE SCOPE OF THIS WORK. REFER TO BUILDING ELECTRICAL ENGINEER FOR MORE INFORMATION. NOTIFY ENGINEER IF ACTUAL LOCATION OF ELECTRICAL CONNECTION/CONTROL IS IN A SIGNIFICANTLY DIFFERENT AREA OF BUILDING.
5. PROVIDE QUAZITE BOX IN APPROXIMATE LOCATION FOR FULL POINT TO CONNECT WITH HOME RUNS FROM SITE LIGHTING.

LIGHT FIXTURE SPECIFICATIONS:

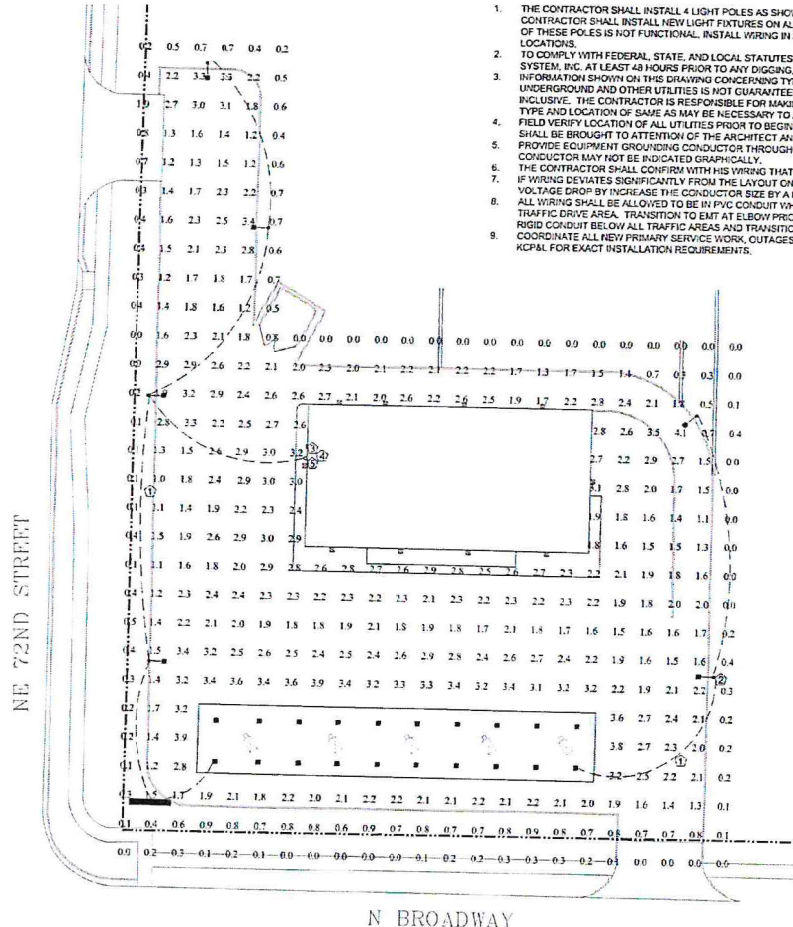
MANUFACTURER INNOVATIVE LIGHTING
LIGHT TYPE LED LIGHT ENGINE
POWER 48 WATTS
TYPE II
MODEL EF2-U-28-3-N
INSTALLATION POLE MOUNTED



LIGHT POLE SECTION / ELEVATION DETAIL
N.T.S.

GENERAL NOTES:

1. THE CONTRACTOR SHALL INSTALL 4 LIGHT POLES AS SHOWN ON THIS SHEET. THE CONTRACTOR SHALL INSTALL NEW LIGHT FIXTURES ON ALL THESE POLES. IF WIRING TO ANY OF THESE POLES IS NOT FUNCTIONAL, INSTALL WIRING IN 3/4\"/>



LEGEND

- NEW LIGHT POLE
- CANOPY LIGHT
- WALL MOUNTED LIGHT
- UNDERGROUND ELECTRIC

SITE LIGHTING PHOTOMETRIC PLAN



DATE	DESCRIPTION
02/20/2024	DESIGN GROUP LLC

KRM
Design Group LLC
8003 E. Shawnee Road
Suite 100
Kansas City, Missouri 64124
(816) 797-2255

SHORT STOP GAS STATION PROJECT

400 NE 72ND STREET
GLADSTONE, MISSOURI

PARKING LOT PHOTOMETRIC PLAN

Project number 2023-109
Drawn by KRB
Checked by GWM

PLANT LIST

NO	SYMBOL	COMMON NAME	BOTANICAL NAME	SIZE
SHADE TREES				
5	SYM	SHANTUNG MAPLE	ACER TRUNCATUM	2.5" CAL
9	BDC	BALD CYPRESS	TAXODIUM DISTICHUM	2.5" CAL
EVERGREEN SHRUBS				
25	BOX	GREEN VELVET BOXWOOD	DUX'S 'GREEN VELVET'	3 GAL. CONTAINER
26	WY	WARD'S YEW	TAXUS MEDIA 'WARDI'	3 GAL. CONTAINER

LANDSCAPING NOTES:

1. ALL PLANT MATERIAL SHALL BE FIRST CLASS REPRESENTATIVES OF SPECIFIED SPECIES, VARIETY OR CULTIVAR, IN HEALTHY CONDITION WITH NORMAL WELL DEVELOPED BRANCHES AND ROOT PATTERNS. PLANT MATERIAL MUST BE FREE OF OBJECTIONABLE FEATURES. PLANTS SHALL COMPLY IN ALL APPLICABLE RESPECTS WITH PROPER MOST RECENT STANDARDS AS SET FORTH IN THE AMERICAN ASSOCIATION OF NURSERYMEN'S 'AMERICAN STANDARD OF NURSERY STOCK', ANSI Z60.1, AND THE GLADSTONE NURSERY AND LANDSCAPE ASSOCIATION.
2. ORNAMENTALS AND SHRUBS SHALL BE CONTAINER GROWN AND WILL BE FREE OF DISEASE AND PESTS. ABSOLUTELY NO BARE ROOT MATERIALS. FERTILIZER OF 10-20-10: ONE PELLET OR 1-2 OZ. SHALL BE ADDED TO SOIL AT TIME OF PLANTING. ALL SHRUB AND PLANT BEDS TO BE MULCHED WITH 3" DEPTH DARK HARDWOOD MULCH. AS AN ALTERNATE IN SHRUB BEDS, 2" DEEP SMOOTH RIVER ROCK OVER PERMEABLE WEED BARRIER FABRIC USED FOR WEED PREVENTION MAY BE INSTALLED INSTEAD OF HARDWOOD MULCH. HARDWOOD MULCH TO BE INSTALLED IN ALL ORNAMENTAL GRASS BEDS.
3. PLANTING BEDS ARE TO BE FREE OF WEEDS AND GRASS. TREAT BEDS WITH A PRE-EMERGENT HERBICIDE PRIOR TO PLANTING AND MULCH PLACEMENT. APPLY IN ACCORDANCE WITH STANDARD TRADE PRACTICE.
4. ALL TREES SHALL BE FERTILIZED WITH FERTILOME BRAND LIQUID ROOT STIMULATOR, 1.5 TABLESPOONS PER GAL. OF WATER, AS A SUBSTITUTE, 1948-10 GRANULAR FERTILIZER, 75 LB. FOR 2" CAL. & 1.5 LBS. FOR 2" CAL. SHALL BE ADDED. INCORPORATE FERTILIZER INTO THE AMENDED PLANTING SOIL BEFORE PLANTING TREE. HOLE AREA FOR TREE TO BE TWICE (2x) THE DIAMETER OF THE ROOT BALL AND ROOT BALL SHALL BE MOUND. ALL TREES TO BE STAKED AND GUYPED WITH A MINIMUM OF 3 POSTS AND PROTECTED W/ COVERING AT TREE W/ GUY WIRE.
5. ALL PLANT MATERIALS SHALL BE PROTECTED FROM THE DRYING ACTION OF THE SUN AND WIND AFTER BEING DUG, WHILE BEING TRANSPORTED, AND WHILE AWAITING PLANTING. BALLS OF PLANTS WHICH CANNOT BE PLANTED IMMEDIATELY SHALL BE PROTECTED FROM DRYING ACTION BY COVERING THEM WITH MOIST MULCH. PERIODICALLY, APPLY WATER TO MULCH-COVERED BALLS TO KEEP MOIST. IF PLANTING SHOULD OCCUR DURING GROWING SEASON, APPLY ANTI-DESICCANT TO LEAVES BEFORE TRANSPORT TO REDUCE THE LIKELIHOOD OF WINDBURN. REAPPLY ANTI-DESICCANT AFTER PLANTING TO REDUCE TRANSPIRATION.
6. AFTER PLANTING IS COMPLETED, REPAIR INJURIES TO ALL PLANTS AS REQUIRED. LIMIT AMOUNT OF PRUNING TO A MINIMUM TO REMOVE DEAD OR INJURED TWIGS AND BRANCHES. PRUNE IN SUCH A MANNER AS NOT TO CHANGE THE NATURAL HABIT OR SHAPE OF THE PLANT. MAKE CUTS FLUSH, LEAVING NO STUBS. CUTS OF ONE INCH OR MORE TO BE PAINTED WITH TREE PAINT. CENTRAL LEADERS SHALL NOT BE REMOVED.
7. THE INSTALLATION OF ALL PLANT MATERIAL SHALL BE IN COMPLIANCE WITH THE REQUIREMENTS OF THE CITY OF GLADSTONE, MO.
8. ALL LANDSCAPE AREAS TO BE FREE OF ALL BUILDING DEBRIS AND TRASH. BACK FILLED WITH CLEAN FILL SOIL AND TOP DRESSED WITH 6" OF TOPSOIL. TOPSOIL SHALL HAVE A pH RANGE OF 5.5 TO 7 AND A 4% ORGANIC MATERIAL MINIMUM. ASTM D5268.
9. ALL PLANT BED AREAS TO RECEIVE DAILY COW MANURE SOIL CONDITIONER AT A RATE OF 4.5 CU. YDS. PER 1000 SF. AND ORGANIC COMPOST AT A RATE OF 4.5 CU. YDS. PER 1000 SF. TO DETERMINE THE AMOUNT OF PHOSPHOROUS AND POTASSIUM THE CONTRACTOR SHALL PERFORM A SOIL TEST AND ADD THOSE FERTILIZERS ACCORDING TO THE TEST RESULTS. AFTER APPLYING SOIL CONDITIONER AND FERTILIZER, THOROUGHLY TILL AREA TO A DEPTH OF 12". CONTRACTOR TO INSTALL A PERMEABLE LANDSCAPE WEED CONTROL FABRIC, 3 OZ. PER SQ. YD. MIN. IN ALL PLANT BEDS EXCEPT IN AREAS OF GROUND COVER, PERENNIAL OR ANNUAL PLANTINGS. PLANT BEDS TO BE "MOUNDING". ALL PLANT MATERIAL, PLANT BEDS, MULCH AND EDGING TO BE INSTALLED PER LANDSCAPE PLANS AND DETAILS. NYKE PRO MYCORRHIZAE GRANULES TO BE ADDED TO ALL PLANTINGS PER MANUFACTURERS RECOMMENDATIONS.
10. REESTABLISH FINISH GRADES TO WITHIN ALLOWABLE TOLERANCES ALLOWING 1-1/2" FOR 500 AND 2" FOR MULCH IN PLANT BEDS. HAND RAKE ALL AREAS TO SMOOTH EVEN SURFACES FREE OF DEBRIS, CLODS, ROCKS, AND VEGETATIVE MATTER GREATER THAN 1".
11. THE EXACT LOCATION OF ALL UTILITIES, STRUCTURES AND UNDERGROUND UTILITIES SHALL BE DETERMINED AND VERIFIED ON SITE BY THE LANDSCAPE CONTRACTOR PRIOR TO INSTALLATION OF THE MATERIALS. DAMAGE TO EXISTING UTILITIES AND OR STRUCTURES SHALL BE REPLACED TO THEIR ORIGINAL CONDITION BY THE LANDSCAPE CONTRACTOR AT NO COST TO THE OWNER.
12. LANDSCAPE CONTRACTOR IS RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS AND APPROVALS AND REG'D INSPECTIONS BY LEGAL AUTHORITIES. THE LANDSCAPE CONTRACTOR SHALL UNCONDITIONALLY GUARANTEE ALL PLANT MATERIAL FOR ONE CALENDAR YEAR.
13. ANY SUBSTITUTIONS OF DEVIATIONS SHALL BE REQUESTED IN WRITING BY THE CONTRACTOR FOR APPROVAL BY THE OWNER OR LANDSCAPE ARCHITECT.
14. THE LANDSCAPE CONTRACTOR IS RESPONSIBLE FOR THE DESIGN, OBTAINING AND INSTALLATION OF ALL IRRIGATION COMPONENTS, SLEEVING, PIPE, METERS, PERMITS, CONNECTION AND CONTROL SYSTEMS. DESIGN DRAWINGS OF THE PROPOSED IRRIGATION SYSTEM SHALL BE SUBMITTED TO THE CITY FOR REVIEW AND APPROVAL PRIOR TO INSTALLATION.
15. EROSION CONTROL MAT TO BE NORTH AMERICAN SC 150-BN BIODEGRADABLE MAT OR EQUIVALENT.
16. ALL LAWN AREAS TO BE SOODED OR SEEDED WITH TURF TYPE TALL FESCUE BLEND IN LOCATIONS INDICATED ON PLANS. SEEDED LAWN TO BE HYDRO-SEEDED OR DRILLED. SOO AND SEED SHALL COMPLY WITH THE U.S. DEPT. OF AGRICULTURE RULES AND REGULATIONS UNDER THE FEDERAL SEED ACT AND EQUAL IN QUALITY TO STANDARDS FOR CERTIFIED SEED. LAWN SHALL BE TURF TYPE TALL FESCUE 3 WAY BLEND.

LAWN SEED MIX

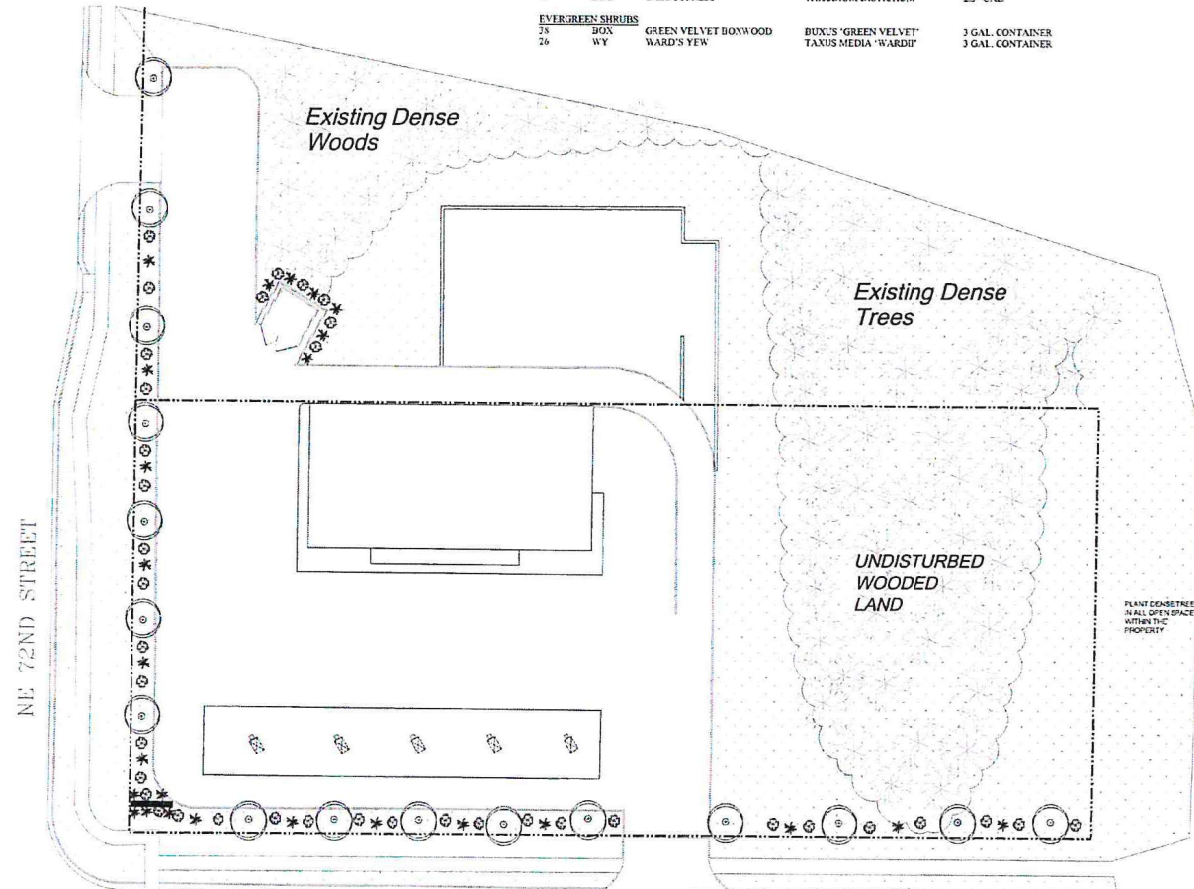
TRI-STAR® QUICK TURF MIXTURE OR SIMILAR BLEND:

SEEDING RATE: 8-10 LBS PER 1,000 SF

- 25% TITAN LTD FESCUE "TRI-STAR SEED COMPANY
- 25% FALCON IV TALL FESCUE SPURRING HILL, KS 66083
- 25% 2ND MILLENNIUM TALL FESCUE 800-574-3308
- 25% TURF PERENNIAL RYEGRASS

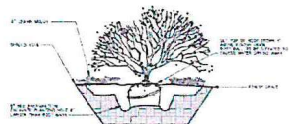
LEGEND

- NEW TREE
- ✱ NEW SHRUB PLANTINGS (LOW TREES)
- BUILDING OUTLINE
- PROPERTY LINE
- DENSE TREE LINE



N BROADWAY

LANDSCAPING PLAN



TYPICAL SHRUB PLANTING

TYPICAL TREE PLANTING DETAIL
NOTE: TREES ARE NOT TO BE PLANTED IN THE SAME LOCATION AS SHOWN IN THE PLANS UNLESS OTHERWISE NOTED.
NEW PLANTING ARE TO BE PLANTED IN THE SAME LOCATION AS SHOWN IN THE PLANS UNLESS OTHERWISE NOTED.

GENERAL NOTES

1. THE LANDSCAPING AREA SHALL BE INSTALLED WITH BUILT IN IRRIGATION SYSTEM.
2. ANY DAMAGES TO CURB AND SIDEWALK IN PUBLIC RIGHT OF WAY SHALL BE REPAIRED PER CITY STANDARD DETAIL AND SPECIFICATIONS.
3. THE TRASH ENCLOSURE STRUCTURE SHALL BE CONSTRUCTED OF THE SAME MATERIAL AS FOR THE MAIN BUILDING.
4. THE GAS METER AREA SHALL BE SCREENED WITH SHRUBS. THE ELECTRICAL METER AND SWITCHGEAR SHALL BE SCREENED WITH ENCLOSURE MATCHING THE BUILDING EXTERIOR.
5. 12 TREES SHALL BE PLANTED ALONG THE PUBLIC RIGHT OF WAY.

SHORT STOP GAS STATION
PROJECT

400 NE 72ND STREET
GLADSTONE, MISSOURI

LANDSCAPING PLAN

Project number: 2023-109
Drawn by: KRB
Checked by: GYM

SHEET 10



Property Owners Within 185' & Other Interested Parties

FROM: Community Development Department

DATE: May 2nd, 2024

SUBJECT: Gas Station & Convenience Store – Site Plan Revision

PUBLIC HEARING

All persons are hereby notified that the Gladstone Planning Commission will conduct a public hearing on Monday, May 20, 2024 at 7:00 PM in the Council Chamber of Gladstone City Hall on a request for a Site Plan Revision at 7200 N Broadway Ave. Legally described as 000000 NW 72ND ST BEG SW COR LT 12 WILLOW CREEK E146, S340, SW21.21, W138, N T O POB.

Applicant: Gerald W. Menefee P.E.

Owner: Mohammad Hafiz

Subsequently, at its regular meeting of June 10th, 2024, at 7:30 PM, the City Council will conduct a public hearing on the same request.

Project Summary: This project was proposed in 2023 and denied by the Gladstone City Council. The property owner has made adjustments to the site plan and is proposing to build a new gas station and convenience store on the vacant land located at 7200 N Broadway Avenue. The primary exterior building materials being used are brick and stucco. There will be two access points; one point on N Broadway Avenue and one point on NW 72nd Street. This property is zoned CP-2, Planned District, General Business and a gas station and convenience store is currently a permitted use for this commercial zoning.

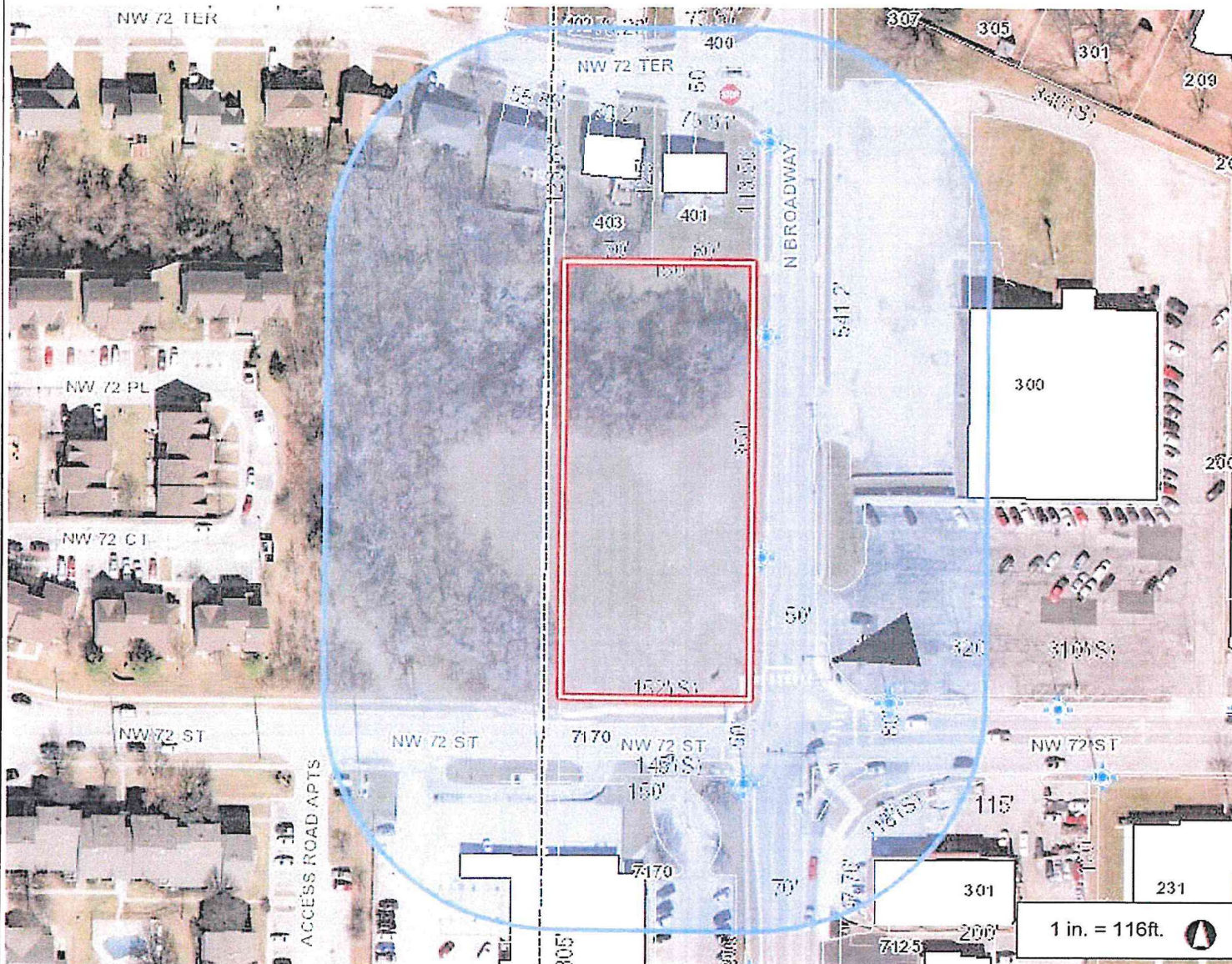
Primary Adjustments to the Site Plan:

- The access point on NW 72nd Street has been shifted west to lineup with the Post Office access point.
- The water detention basin has been moved from the northern side of the property to the western side of the property away from the residential homes located to the north. This basin will be located on the KCMO parcel.
- The wooded area on the northern side of the property will primarily remain untouched.

If you have any questions or concerns, please contact Austin Greer, Community Development Director & Assistant City Manager at austing@gladstone.mo.us and/or 816-423-4102.



Gladstone, MO



Legend

- Stop Sign
- KCPL Lights
- Gladstone Lights
- School Point
- Bike Parking
- Bus Stop
- Point of Interest
- Church
- Apartment Point
- Street Centerline
- Edge Of Pavement
- Driveway
- City Limits
- Parcel
- House Number
- Building Footprint
- School Polygon
- City Park
- Villages
- Apartment Polygon

Notes

This map is a user generated static output from an Internet mapping site and is for reference only. Data layers that appear on this map may or may not be accurate, current, or otherwise reliable.
THIS MAP IS NOT TO BE USED FOR NAVIGATION

(minus street right-of-ways), the final City Council action has to have a minimum of four (4) positive votes for the request to be approved. The application cannot be approved if three (3) vote "yes" and two (2) "no". For further information regarding this handout, please call or come by the Community Development Department at 7010 N. Holmes, 423-4110.

☐ City Code Variance Request: Board of Zoning Adjustment

REQUIREMENTS

Completed application
Owner's authorization signed (if applicable)
Legal description- County records
Information on the proposed change including pictures of the property, property surveys, written comments from impacted neighbors, etc.

DEPOSIT FEE

The \$200 fee listed on the form and paid at the time of application is a deposit toward the costs the City of Gladstone incurs during the processing of your application. This fee goes toward the following costs:

Office fee \$75.00
Certified mail notices to surrounding property owners within 185' - amount varies.*
Planning Commission Legal Notice- amount varies*

** Indicates fees for items required by State Law. The fee amount for certified mail will vary depending upon the number of property owners within 185 feet of your property. The Legal Notice fee will also vary generally depending upon the length of the legal description of your property.*

After the total costs are compiled for your application, you will be billed for any costs remaining over the initial \$200 application deposit fee. If the costs accrued are under \$200, you will be reimbursed for the difference.

As the money deposited for your application goes toward real costs paid by the City, there is no refund if your application is denied by the Board of Zoning Adjustment. If you withdraw your application before some of the costs are accrued by the City, you may be entitled to a refund.

Preliminary & Final Plat/Replat Submittals

REQUIREMENTS

Completed application
Owner's authorization signed (if applicable)
Legal description- County records
Digital copy of plans
(1) 11x17 paper copy
(3) 24x36 paper copies folded
(1) 24x36 Mylar Copy - Completion of the Plat

FEE

The \$75 fee listed on the form and paid at the time of application goes toward the costs the City of Gladstone incurs during the processing of your application. As the fee for your application goes toward real costs paid by the City, there is no refund.

**At completion of the plat, please submit to Community Development (1) 24x36 Mylar copy.

OWNER'S AUTHORIZATION

I, Mohammad Hachiz, do hereby authorize _____
(Owner's name) (Applicant's name)
to apply for the following action on my property at _____

- a. Rezone from to
- b. Site Plan Revision
- c. Special Use Permit
- d. Variance
- e. Plat/Replat


Date: 5/20/24 Owner's Signature: 

NOTARIZATION

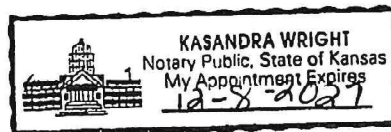
State of Kansas
 County of Wyandotte

Subscribed and sworn before me this 20th day of May, 2024.

Notary's Signature:



My Commission expires: 12-8-2027



Additional Required Documents

(check if needed)	Comments
Site Plan <u> </u>	
Traffic Study <u> </u>	
Landscaping Plans <u> </u>	
Stormwater <u> </u>	
(Pre - Post - BMP) <u> </u>	
Photometric Study <u> </u>	
Master Sign Plan <u> </u>	
Colored Elevation / Rendering <u> </u>	
Materials Board <u> </u>	

Gladstone Convenience Store

TRAFFIC IMPACT STUDY

May 20, 2024

Prepared For:
Mr. Muhammed Hafiz

Prepared By:
Priority Engineers, Inc.
PO Box 563
Garden City, MO 64747





May 20, 2024

Mr. Muhammed Hafiz

RE: Gladstone Convenience Store Traffic Impact Study – Gladstone, MO

Dear Mr. Hafiz:

In response to your request, Priority Engineers, Inc. has completed a traffic impact analysis for the above referenced project. The purpose of the analysis is to determine the potential traffic impacts associated with this development on the intersections and streets surrounding this site, primarily during the AM and PM peak hours. The following report documents our analysis and recommendations.

We appreciate the opportunity to work with you on this project. Please contact us with any questions or if you require additional information.

Sincerely,

PRIORITY ENGINEERS, INC.

A handwritten signature in blue ink, which appears to read 'Kristin L. Skinner', is written over the printed name.

Kristin L. Skinner, P.E., PTOE
President

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1) INTRODUCTION

The purpose of this study is to examine the potential traffic impacts associated with a proposed Gladstone Convenience Store development located within the municipal limits of Gladstone, in Clay County, Missouri. This proposed development will construct a convenience store located to the north and the west of the intersection of NW 72nd Street and N Broadway Street.

The study area is shown in Figure 1. The site layout is shown in Figure 2.

2) EXISTING CONDITIONS

The proposed Gladstone Convenience Store development is located on a parcel of undeveloped land located northwest of the intersection of N Broadway Street and NW 72nd Street. To the north and west of the proposed development there are existing residential developments. To the south of the proposed development is a USPS facility and to the east of the proposed development is the Gladstone Bowl bowling alley.

N Broadway Street, south of the intersection with NW 72nd Street has a cross-section of two lanes in each direction without separation and it has curb and gutter and an enclosed drainage system. This segment N Broadway Street has a posted speed limit of 35 MPH. North of the intersection with NW 72nd Street has a cross section that consists of one lane in each direction, and curb and gutter with an enclosed drainage system. The posted speed limit on this segment of N Broadway Street is 30 MPH. The Mid America Regional Council (MARC) has given N Broadway Street a functional classification of Minor Arterial south of NW 72nd Street and a functional classification of Minor Collector north of NW 72nd Street. The Gladstone Comprehensive Plan identifies N Broadway Street as an Arterial south of NW 72nd Street and as a Primary Collector to the north of NW 72nd Street.

NW 72nd Street, to the east, has a cross section with two through lanes in each direction. NW 72nd Street has curb and gutter and an enclosed drainage system. MARC has given NW 72nd Street a functional classification of Minor Arterial to the west. The Gladstone Comprehensive Plan identifies NW 72nd Street as an Arterial. NW 72nd Street has a posted speed limit of 35 MPH.

Peak Hour turning movement counts were collected for the following intersections:

- NE 72nd Street N Broadway Street
- NE 72nd Street and West Drive of the USPS facility
- N Broadway Street and Gladstone Bowl entrance

These counts were performed on January 17th of this year. The Peak Hour turning movement counts were performed from 7:00 to 9:00 AM and from 4:00 to 6:00 PM. The AM Peak Hour was found to be from 8:00 to 9:00 and the PM Peak Hour was found to be from 4:30 to 5:30 for the overall roadway network. The complete traffic counts are shown in Appendix II. The peak hour traffic volumes and existing lane configurations are shown in Figures 3-6.

3) PROPOSED DEVELOPMENT

The proposed development will build an approximately 5,000 SF convenience store with 10 vehicle fueling positions (VFP). The provided site plan shows a drive through window on the west side of convenience store. There will be two full access entrances into the development. The first proposed entrance is a full access entrance onto NE 72nd Street located opposite of the

west entrance into the USPS facility. Street. The second full access entrance will provide access onto N Broadway Street. This access will be located to the north of the existing Gladstone Bowl drive.

4) TRIP GENERATION

The vehicle trips generated by the proposed development were estimated using the Institute of Transportation Engineers' (ITE) Trip Generation, 11th Edition. Land Use 945, Convenience Store / Gas Station. Since this location has a drive-through window, both Land Use 935 (fast food restaurant with drive-through window and no indoor seating) and Land Use 934 (fast food restaurant with drive through window) were considered for a portion of the 5,000 SF store. It was determined that the trips generated by Land Use 945 is higher than Land Use 935 and it is slightly higher than Land Use 934, so the complete footprint of the store was considered using Land Use 945 for a more conservative trip generation estimate.

Land Use 945 has two subcategories in the ITE data set, and GFA of the Store (with independent variable of VFP and VFP (with independent variable of GFA). Selecting data from the VFP subcategory resulted in a more conservative trip generation and was selected for this study.

The estimated AM and PM peak hour traffic volumes associated with the full buildout of this development are shown in Table 1.

Table 1: ITE Trip Generation								
Land Use	Intensity	Daily	AM Peak Hour			PM Peak Hour		
			Total	In	Out	Total	In	Out
Convenience Store/Gas Station (VFP 9-15)	5,000 SF	3353	283	141	142	273	136	137

Pass-by trips are made as intermediate stops on the way from an origin to a primary trip destination without a route diversion. For this site, pass-by trips will be those vehicles already traveling through the intersection of NW 72nd Street and N Broadway Street. Chapter 10 and Appendix E of the ITE Trip Generation Handbook, 3rd Edition were consulted in estimating these trips. Research indicates that on average 76 percent of AM Peak Period Hour and 75 percent of PM Peak Hour for land use 945 are pass-by in nature. The Trip Generation volumes anticipated by the development are shown in Table 2 below.

Table 2: ITE Trip Generation

<i>Land Use</i>	<i>Intensity</i>	<i>ITE Code</i>	<i>AM Peak Hour</i>			<i>PM Peak Hour</i>		
			<i>Total</i>	<i>In</i>	<i>Out</i>	<i>Total</i>	<i>In</i>	<i>Out</i>
Convenience Store/Gas Station (VFP 9-15)	5,000 SF	945	283	141	142	273	136	137
			-215	-107	-108	-205	-102	-103
Subtotal			283	141	142	273	136	137
<i>Pass-By Trips</i>			-215	-107	-108	-205	-102	-103
Total New Trips			68	34	34	68	34	34

5) TRIP DISTRIBUTION AND ASSIGNMENT

Trips generated by the Gladstone Convenience Store development were distributed based on existing traffic flows and a general analysis of the surrounding area. The trips were distributed onto the existing street system approximately as follows:

- 15 percent to and from the north via N Broadway Street
- 40 percent to and from the south via N Broadway Street
- 40 percent to and from the east via NW 72nd Street
- 5 percent to and from the west via NW 72nd Street

Pass-by trips were distributed based upon the existing traffic patterns near the study intersection of NW 72nd Street and N Broadway Street.

6) LEVEL OF SERVICE AND VOLUME/CAPACITY ANALYSES

Capacity analysis was used to quantify the impacts of the increased traffic on the intersections studied. The methodology outlined in the Highway Capacity Manual, 7th Edition was used as a basis to perform the analysis for this study. Capacity analysis defines the quality of traffic operation for an intersection using a grading system called Level of Service (LOS). The LOS is defined in terms of average vehicle delay. Levels of service A through F have been established with A representing the best and F the worst.

Table 3: Level of Service Definitions

<i>Level of Service</i>	<i>Unsignalized Intersection</i>	<i>Signalized Intersection</i>
A	< 10 Seconds	< 10 Seconds
B	< 15 Seconds	< 20 Seconds
C	< 25 Seconds	< 35 Seconds
D	< 35 Seconds	< 55 Seconds
E	< 50 Seconds	< 80 Seconds
F	≥ 50 Seconds	≥ 80 Seconds

The study intersections were evaluated using Synchro based on part on Highway Capacity Manual methods. The analysis reports are included in Appendix II. Signal Timing Inputs were based upon data provided by City Staff.

Existing Conditions

The levels of service, lane configuration, and queue lengths for existing conditions are shown in Figures 5 and 6 in Appendix I.

During the AM and PM Peak Hours, the overall level of service for the signalized intersection at NW 72nd Street and North Broadway Street is a C in both the AM and PM Peak Hour.

At all STOP-controlled intersections within the study area, the minor movements operate with a level of service B or better during both AM and PM Peak Hours.

Existing + Proposed Development Conditions

The levels of service, lane configuration, and queue lengths for existing conditions are shown in Figures 9 and 10 in Appendix I.

The overall level of service remains a C in both Peak Hours for the signalized intersection with the addition of the traffic generated by the proposed development.

All STOP controlled intersections within the study area operate with a level of service C or better during both Peak Hours.

7) SIGHT DISTANCE

Intersection sight distance and stopping sight distance was measured at the proposed entrances into the development. Intersection sight distance represents the distance and time required for the driver to make the decision to turn and to complete the turn without slowing oncoming traffic. Stopping sight distance represents the amount of distance required for a driver to make an unexpected stopping maneuver based upon observing a 2' tall object in the roadway. At both locations, the AASHTO minimum sight distance for a 35 MPH design speed.

8) ACCESS MANAGEMENT

The proposed drive onto N Broadway Street is located between two existing intersections located on the east side of the street. The drive into Gladstone Bowl is approximately 110' from the intersection of NW 72nd Street and N Broadway Street. Typically, it would be recommended that proposed drive be aligned with an existing drive to minimize turning conflicts. It is not recommended that the drive be located at the Gladstone Bowl drive due to the proximity of this drive to the signalized intersection. The proposed drive however is located approximately as far north as possible and has an approximate offset of 35' from the entrance further to the north. The next entrance to the north has a spacing of approximately 160' to the north from the Gladstone Bowl Entrance.

APWA section 5200 spacing requirements can not be met due to the close proximity of the existing entrances on the east side of N Broadway Street. The proposed drive, however, is located as far north as possible to minimize the impact of the entrance on the function of the intersection.

The entrances at both NW 72nd Street and N Broadway Street were evaluated for right and left turn lanes in accordance with the methodology associated with NCHRP Report 457 using the turn lane guidelines found in MoDOT EPG section 940.9.

At the entrance on NW 72nd Street, neither a left turn lane (EPG Section 940.9.1 left turn guidelines for roads less than or equal to 40 MPH) nor a right turn lane guideline (EPG 940.9.8 right turn lane guidance for two lane roads) is met.

At the entrance onto N Broadway Street a right turn lane is not recommended (EPG 940.9.8 right turn lane guidance for two lane roads), but a left turn lane is recommended when the 40% left turn trend line is selected as per EPG guidance. This is documented in Figure 11 of Appendix I.

9) RECOMMENDATIONS & CONCLUSIONS

This study documents the impact of the proposed Gladstone Convenience Store development on the adjacent roadway network during the AM and PM Peak Hour. Analysis of unsignalized intersections indicate that they operate with acceptable levels of service both before and after the construction of the proposed development. The signalized intersection at NW 72nd Street and N Broadway Street has an overall level of service that is acceptable both before and after construction of the proposed development.

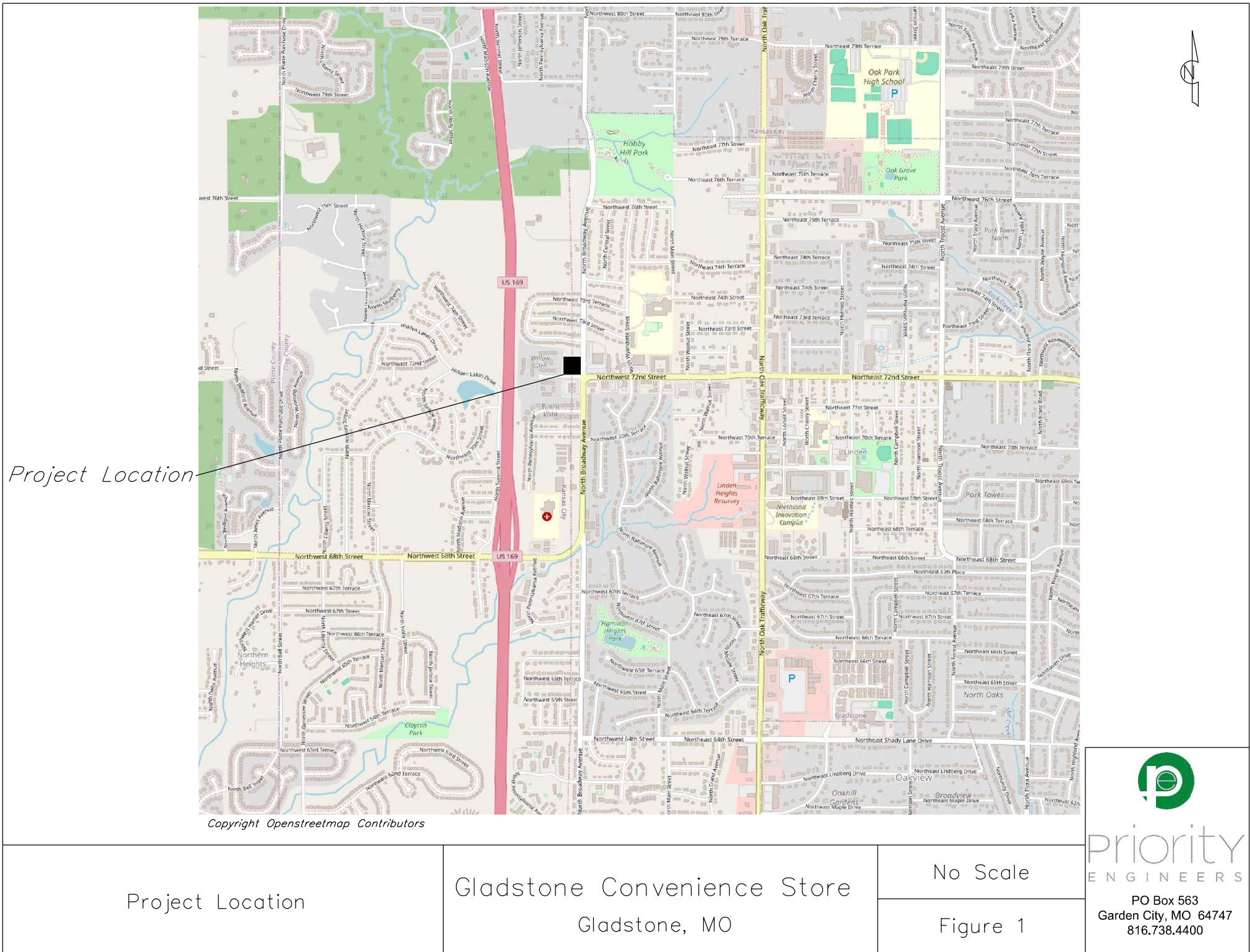
The proposed entrance locations have sufficient sight distance.

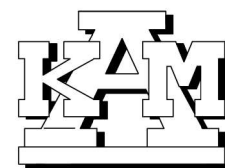
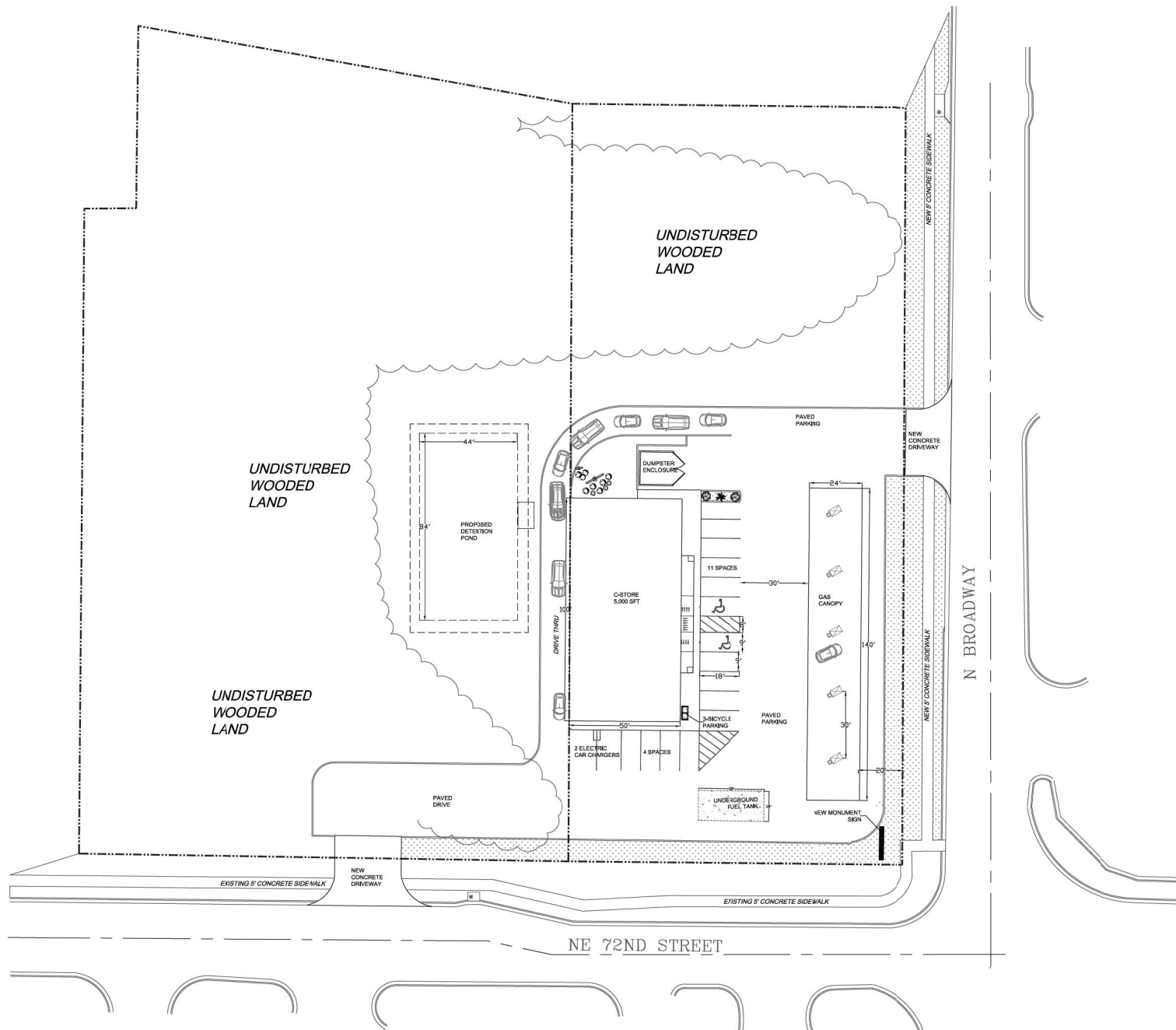
A left turn lane is recommended according to MoDOT guidelines for the entrance on N Broadway Street in the PM Peak Hour. Due to the geometric constraints of this location, if such a turn lane were constructed, it would need to be designed so that it does not interfere with the southbound left turn lane at the signalized intersection with NW 72nd Street. The levels of service at this entrance without the left turn lane are a B or better with a design queue of less than one vehicle.

No other improvements are required as a result of this development.

APPENDIX I

Project Location	Figure 1
Site Plan	Figure 2
Existing AM Peak Hour Traffic Volumes	Figure 3
Existing PM Peak Hour Traffic Volumes	Figure 4
Existing AM Peak Hour Lane Configurations & Levels of Service	Figure 5
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Left Turn Lane Guidelines for Two-Lane Roads less than or equal to 40 mph (MoDOT EPG Figure 940.9.1)	Figure 11





Design Group LLC.
9000 E Bannister Road
Suite 100
Kansas City, Missouri 64134
(816) 797-2065



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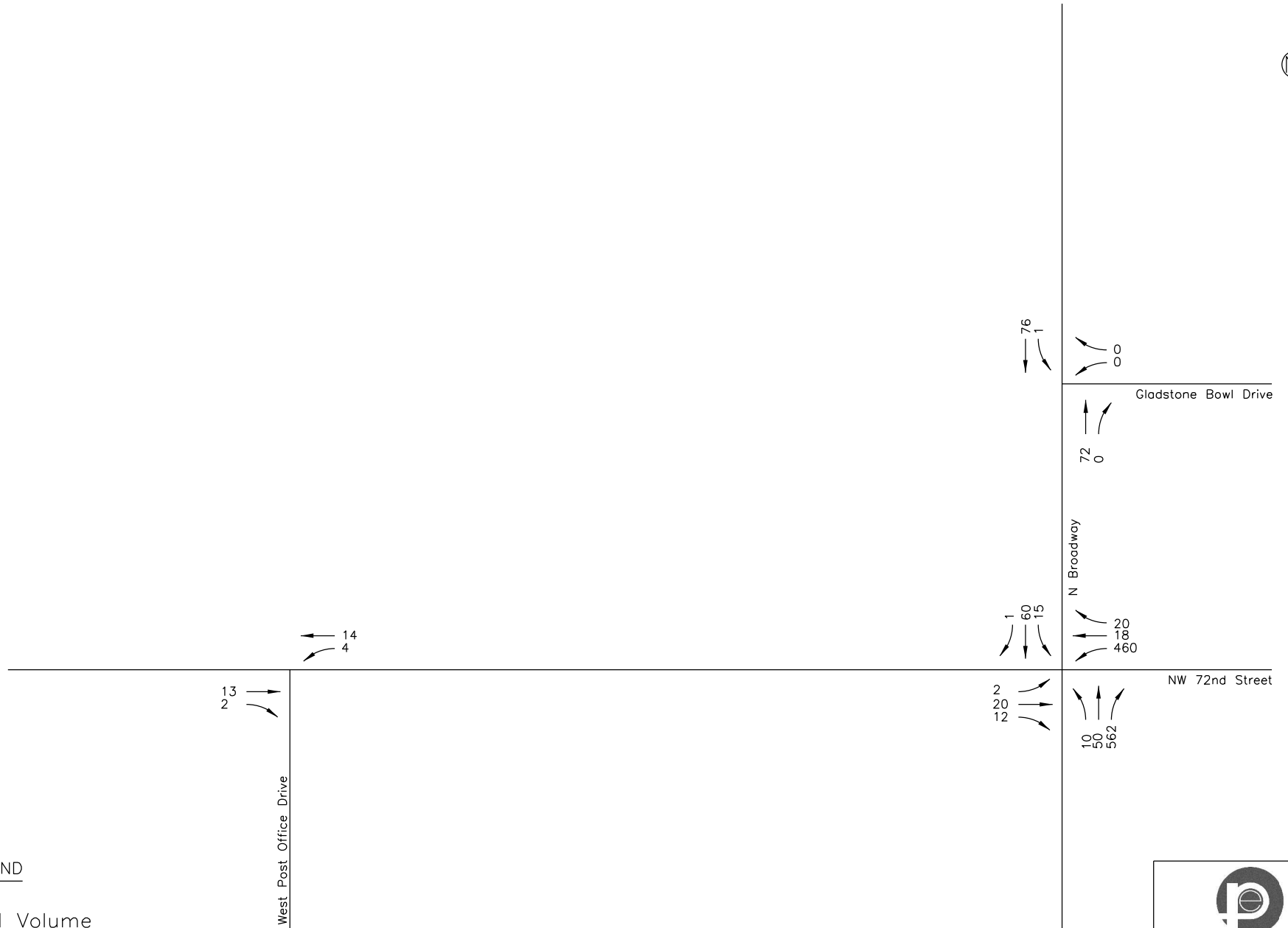
PO Box 563
Garden City, MO 64747
816.738.4400

Site Plan

Gladstone Convenience Store
Gladstone, MO

No Scale

Figure 2

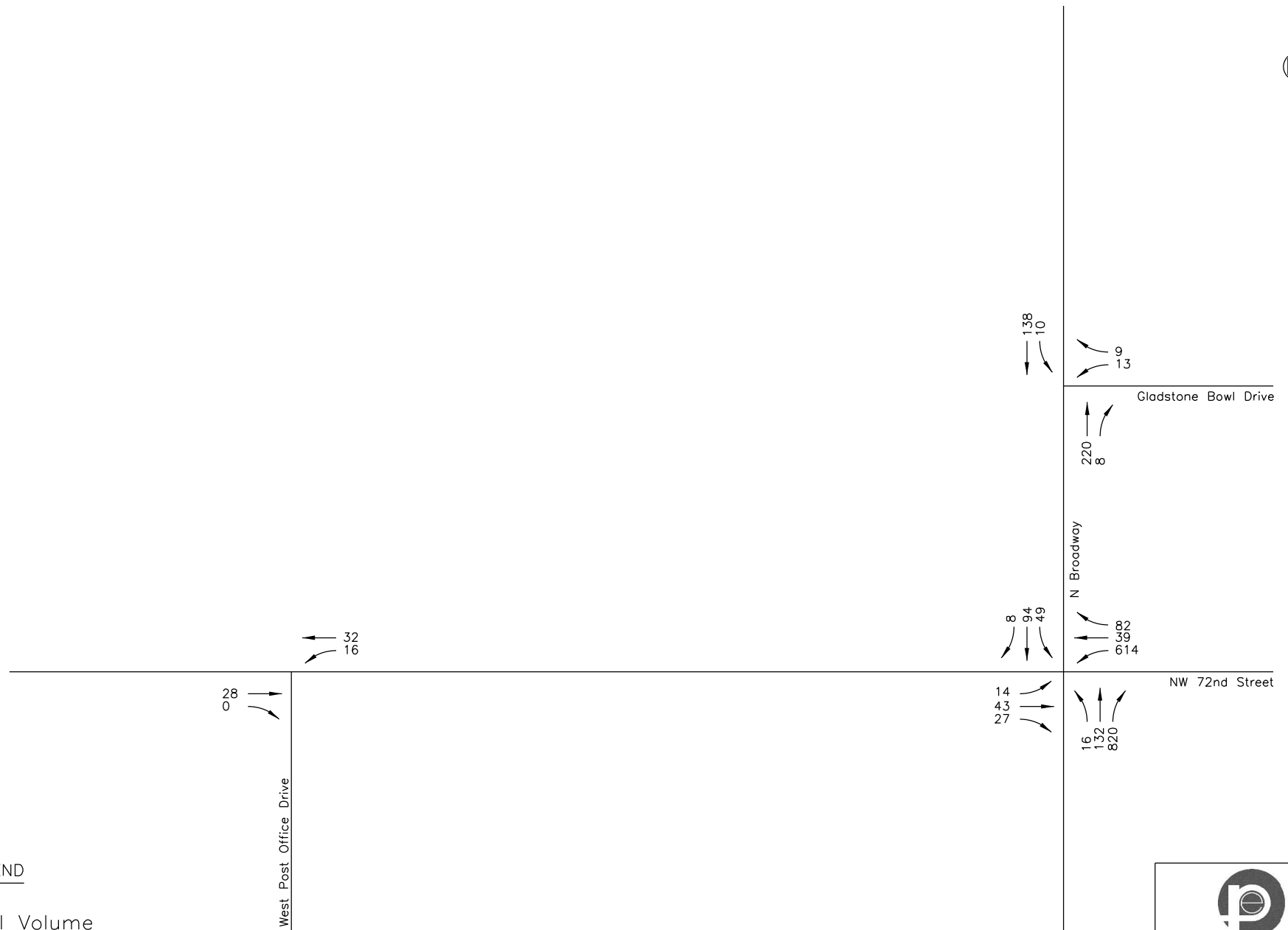


Existing AM Peak Hour
Traffic Volumes

Gladstone Convenience Store
Gladstone, MO

No Scale

Figure 3

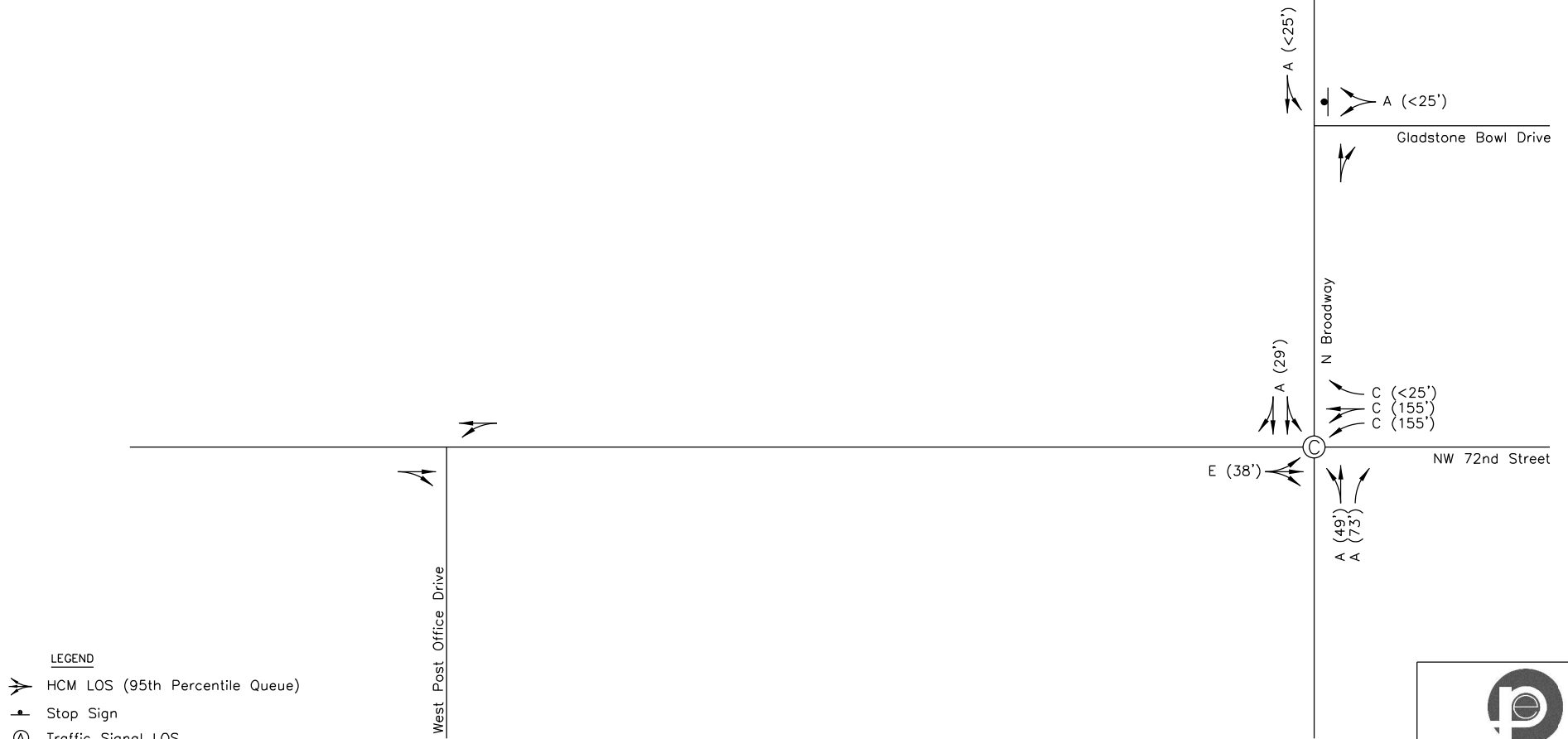


Existing PM Peak Hour
Traffic Volumes

Gladstone Convenience Store
Gladstone, MO

No Scale

Figure 4



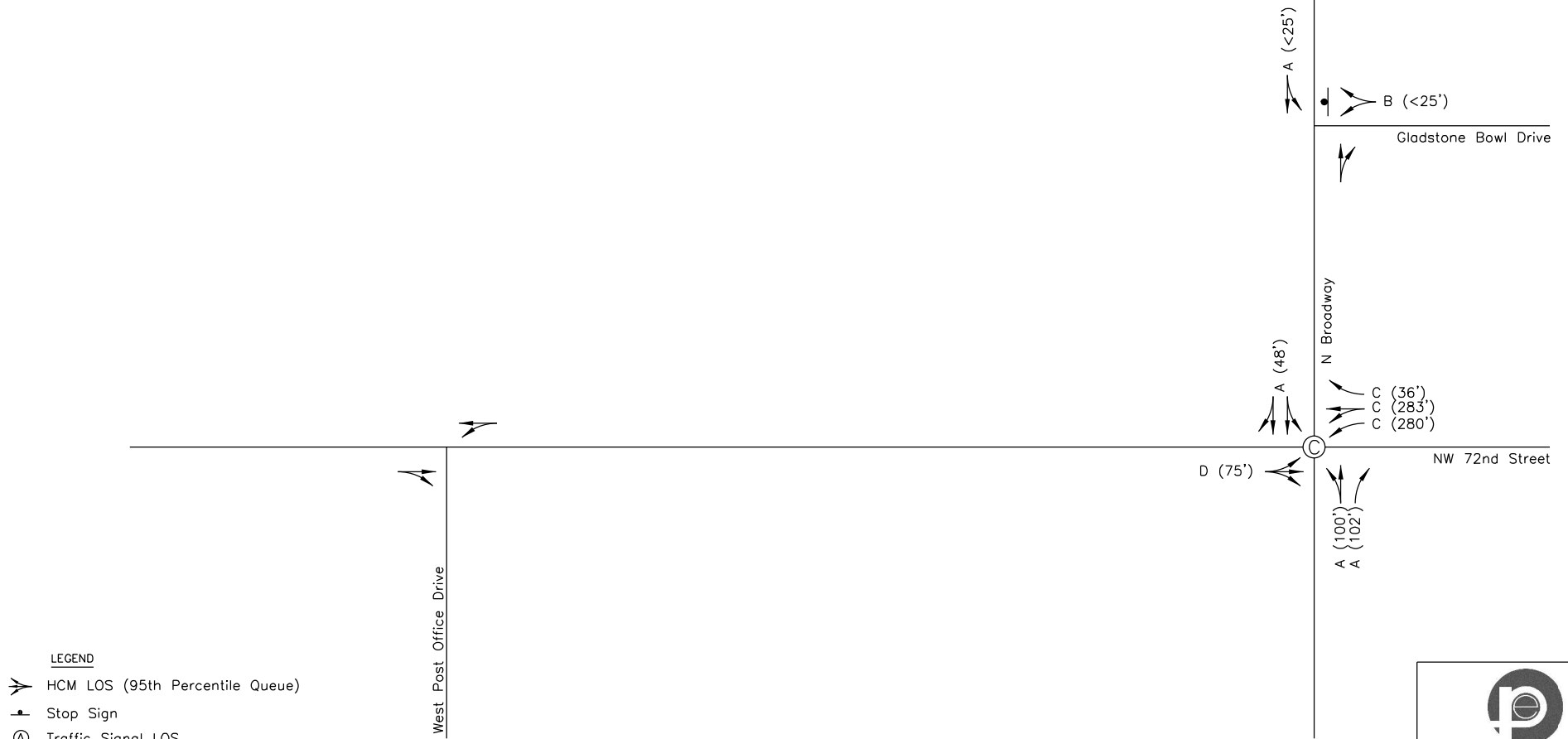
Existing AM Peak Hour
Lane Configuration &
Levels of Service

Gladstone Convenience Store
Gladstone, MO

No Scale

Figure 5


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Existing PM Peak Hour
Lane Configuration &
Levels of Service

Gladstone Convenience Store
Gladstone, MO

No Scale

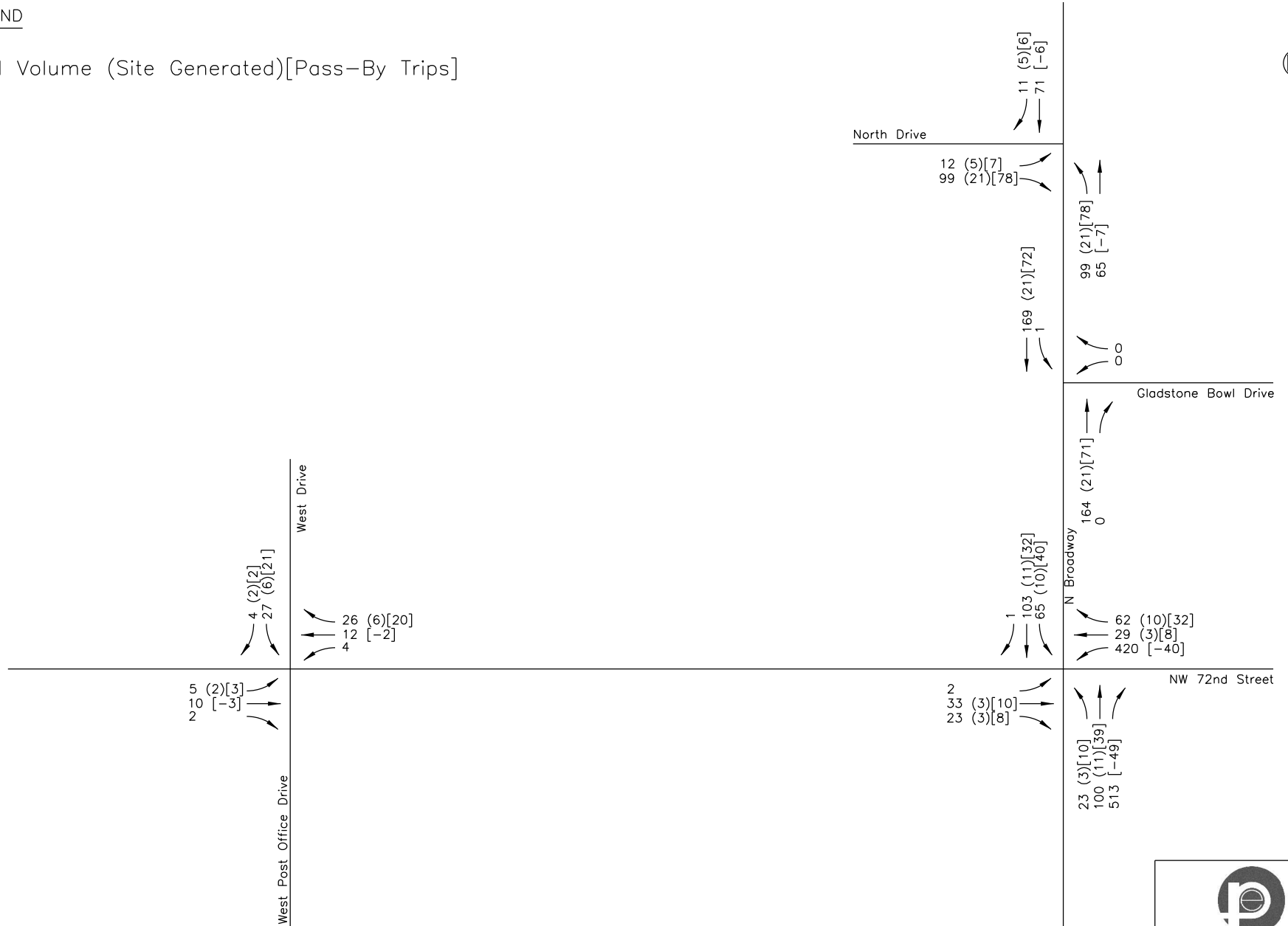
Figure 6


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LEGEND



Total Volume (Site Generated)[Pass-By Trips]



Existing + Proposed Development
AM Peak Hour
Traffic Volumes

Gladstone Convenience Store
Gladstone, MO

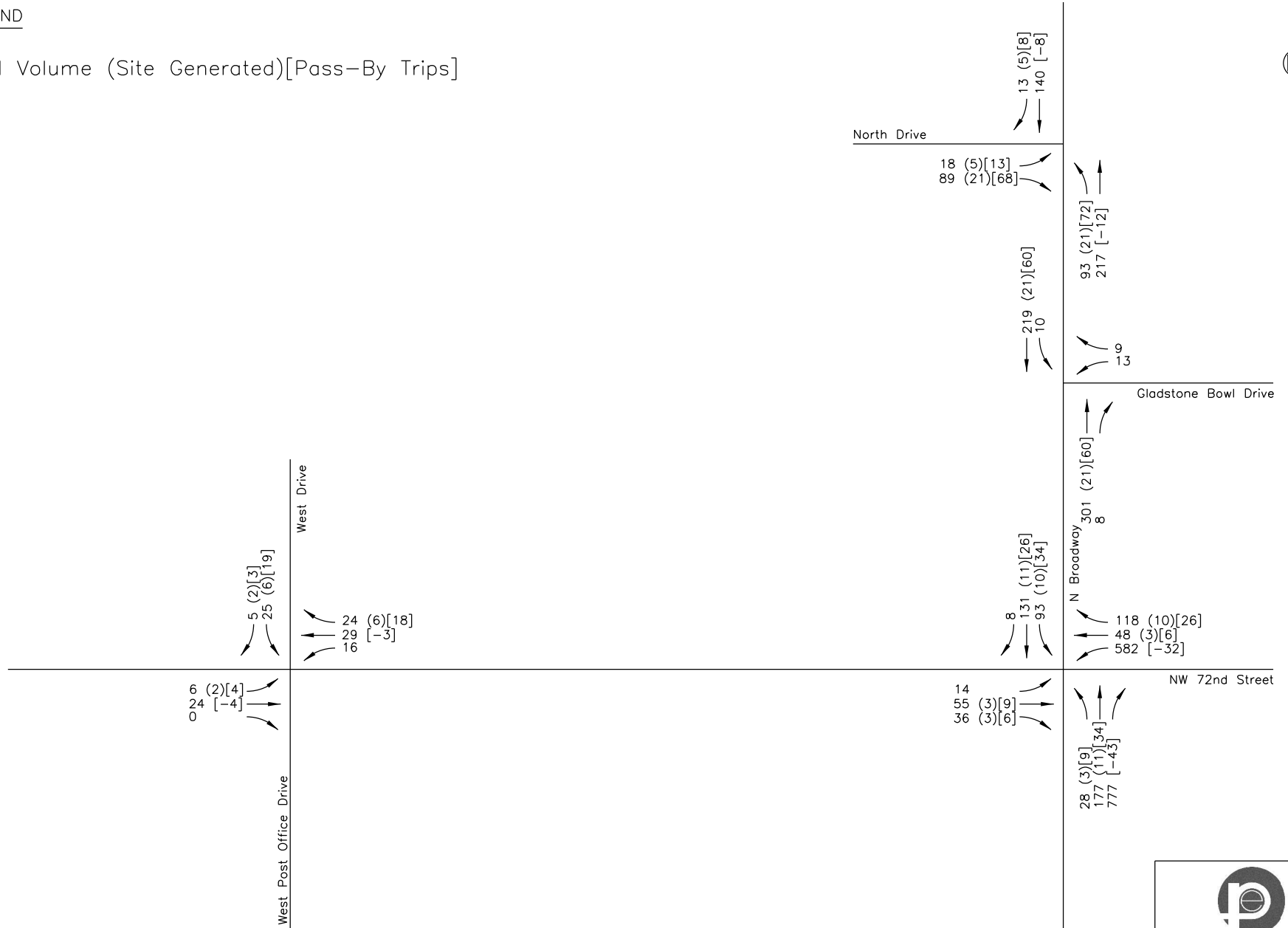
No Scale

Figure 7

LEGEND



Total Volume (Site Generated)[Pass-By Trips]

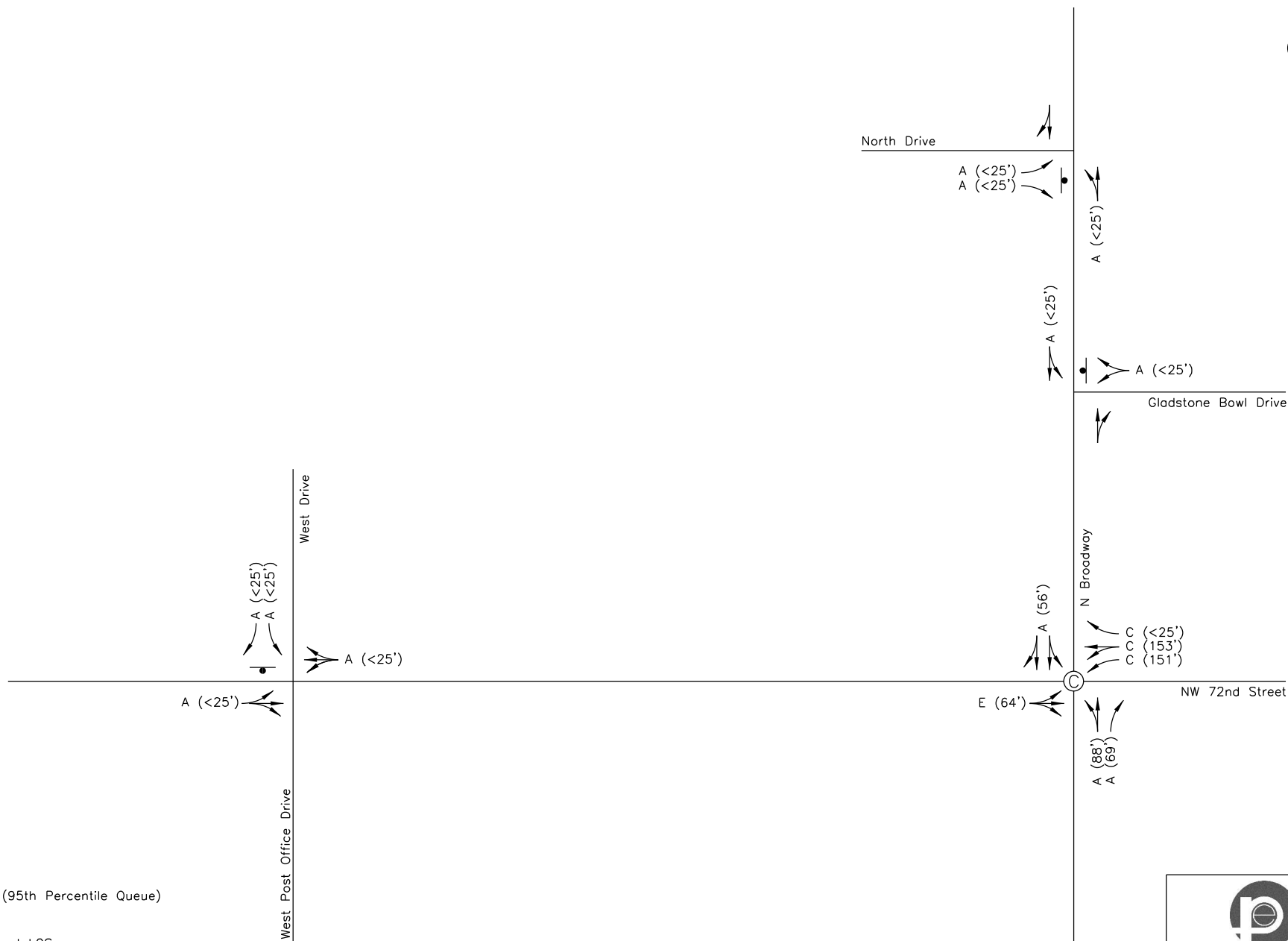


Existing + Proposed Development
PM Peak Hour
Traffic Volumes

Gladstone Convenience Store
Gladstone, MO

No Scale

Figure 8



LEGEND

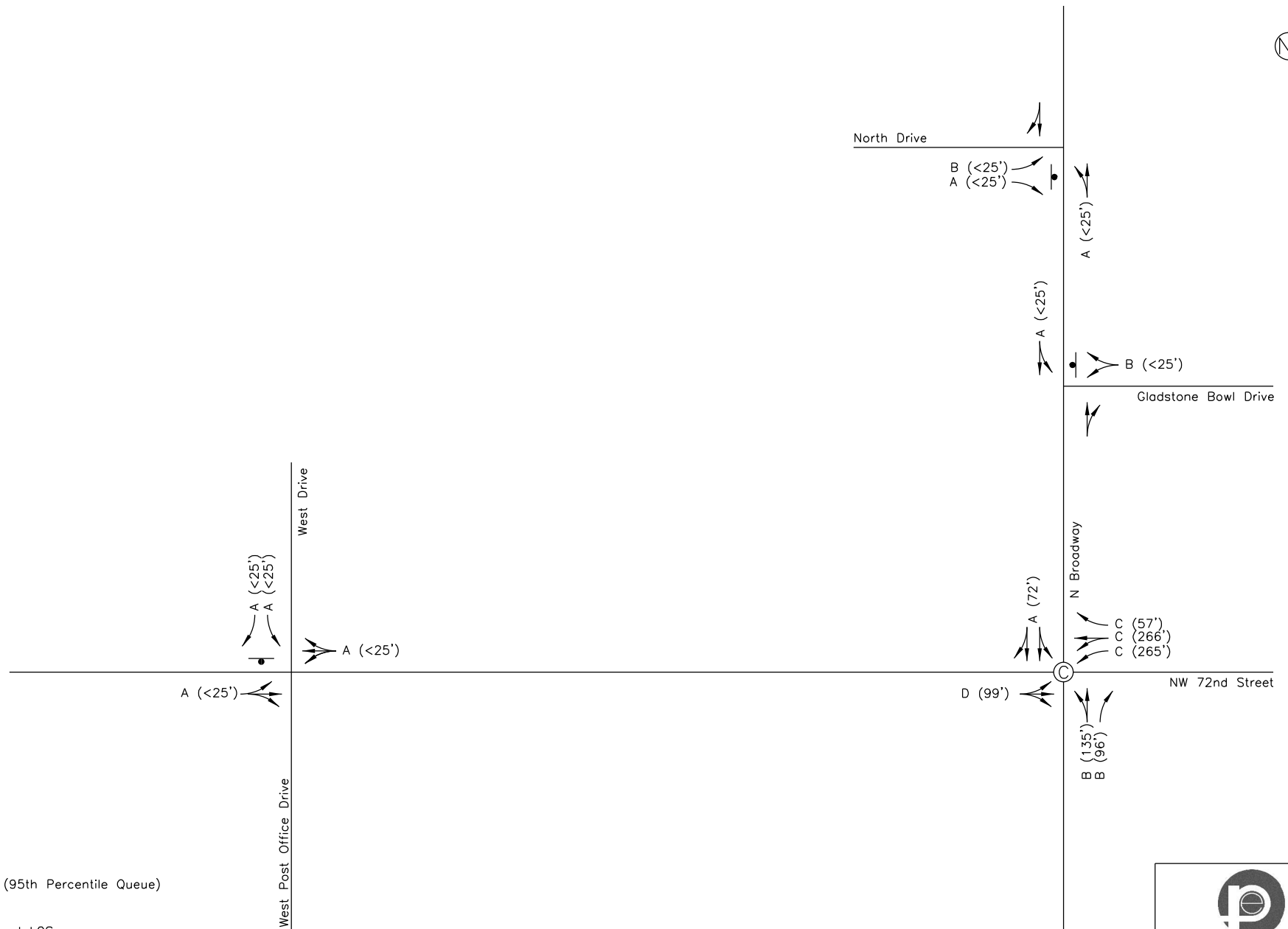
- HCM LOS (95th Percentile Queue)
- ⊥ Stop Sign
- ⓐ Traffic Signal LOS

Existing + Proposed Development
AM Peak Hour
Lane Configuration &
Levels of Service

Gladstone Convenience Store
Gladstone, MO

No Scale

Figure 9



LEGEND

- HCM LOS (95th Percentile Queue)
- Stop Sign
- Traffic Signal LOS

Existing + Proposed Development
PM Peak Hour
Lane Configuration &
Levels of Service

Gladstone Convenience Store
Gladstone, MO

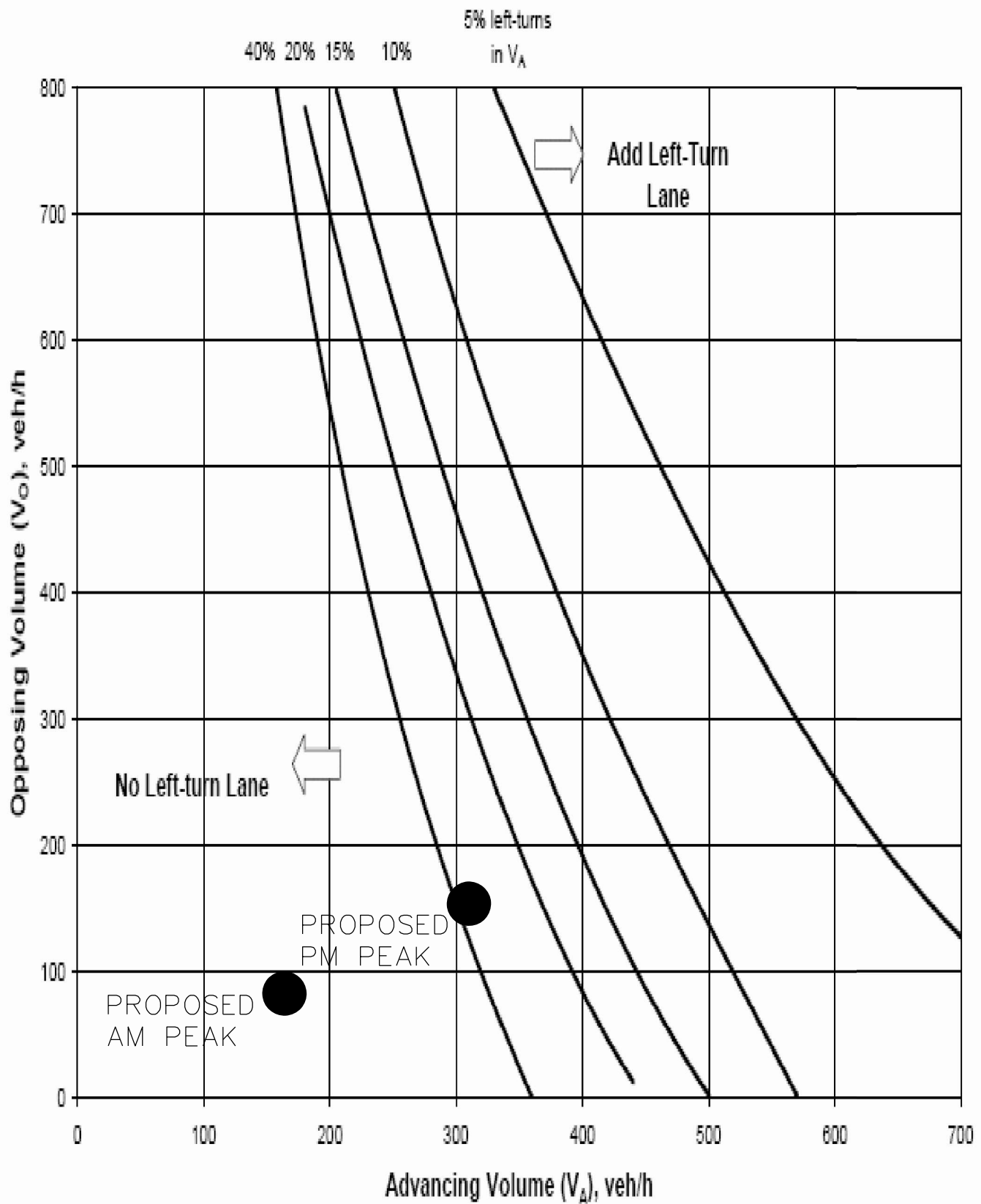
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Figure 10



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Left Turn Lane Guidelines
for Two-Lane Roads less
than or equal to 40 mph
(MoDOT EPG Figure 940.9.1)

Gladstone
Convenience Store
Gladstone, MO

No Scale

Figure 11



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APPENDIX II

Peak Hour Traffic Counts

Synchro Reports

Existing AM Peak Hour

Pages 1-3

Existing PM Peak Hour

Pages 4-6

Proposed AM Peak Hour

Pages 7-11

Proposed PM Peak Hour

Pages 12-16

Broadway & 72nd Street

	Southbound					Westbound					Northbound					Eastbound					Totals		
	Start Time	Left	Through	Right	Ped Bike	Left	Through	Right	Ped Bike	Left	Through	Right	Ped Bike	Left	Through	Right	Ped Bike						
7:00	6	22	0			69	4	7			1	7	62			1	4	4	0		187		
7:15	3	22	0			99	2	4			0	5	79			2	1	0	1		218		
7:30	4	19	0			127	0	3			0	11	125			0	3	2	0		294		
7:45	6	22	1			100	5	11			0	13	136			0	4	1	0		299	998	1187
8:00	7	23	0			110	2	4			3	11	109			1	3	2	0		275	1086	1275
8:15	3	17	0			127	4	3			0	7	167			0	3	1	0		332	1200	1381
8:30	3	14	0			128	5	6			3	16	115			0	3	5	1		299	1205	1393
8:45	2	6	1			95	7	7			4	16	171			1	11	4	0		325	1231	1408
Totals	15	60	1	0	0	460	18	20	0	0	10	50	562	0	0	2	20	12	1	0	1231		
Trucks		1				6					1		5			2				PHF=	0.93		
%		2%				1%					10%		1%			10%							

72nd Street & West Post Office Drive

Start Time	Southbound				Westbound				Northbound				Eastbound				Totals			
	Left	Through	Right	Ped Bike	Left	Through	Right	Ped Bike	Left	Through	Right	Ped Bike	Left	Through	Right	Ped Bike				
7:00					2	2	0	0					5	0	2		11			
7:15					0	1	0	0					1	0	7		9			
7:30					0	0	0	1					4	0	1		6			
7:45					2	2	0	0					1	0	0		5	31		
8:00					2	2	0	0					2	0	0		6	26		
8:15					0	3	0	0					2	0	0		5	22		
8:30					2	3	0	0					3	0	1		9	25		
8:45					0	6	0	0					6	2	0		14	34		
Totals	0	0	0	0	0	4	14	0	0	0	0	0	0	0	0	13	2	1	0	34
Trucks							2									2			PHF=	0.61
%							14%									15%				

Broadway & Gladstone Bowl Drive

Southbound					Westbound					Northbound					Eastbound					Totals
Start Time	Left	Through	Right	Ped Bike	Left	Through	Right	Ped Bike	Left	Through	Right	Ped Bike	Left	Through	Right	Ped Bike				
7:00	0	25			0		0				15						40			
7:15	0	22			0		0				11						33			
7:30	0	20			0		0				14						34			
7:45	1	27			1		1				21						51			
8:00	0	29			0		0				16						45			
8:15	0	19			0		0				10						29			
8:30	0	17			0		0				21						38			
8:45	1	8			0		0				22						31			
Totals	1	73	0	0	0	0	0	0	0	0	69	0	0	0	0	0	143			
Trucks											1						PHF= 0.79			
%											1%									

Broadway & 72nd Street

	Southbound					Westbound					Northbound					Eastbound							
Start Time	Left	Through	Right	Ped	Bike	Left	Through	Right	Ped	Bike	Left	Through	Right	Ped	Bike	Left	Through	Right	Ped	Bike	Totals		
16:00	18	18	3			127	12	15	0		4	28	166			2	10	4	0		407		
16:15	16	44	4			126	12	10	0		3	29	203			3	14	5	0		469		
16:30	7	32	2			123	14	13	1		5	28	212			4	11	9	0		461		
16:45	12	20	2			150	10	17	0		3	29	209			5	14	9	0		480	1817	2234
17:00	13	25	1			187	7	22	0		3	31	191			3	9	4	0		496	1906	2340
17:15	17	17	3			154	8	30	1		5	44	208			2	9	5	1		504	1941	2404
17:30	12	13	0			142	1	15	0		7	29	166			0	3	4	1		393	1873	2324
17:45	20	24	1			130	5	15	0		5	27	167			1	5	1	0		401	1794	2228
Totals	49	94	8	0	0	614	39	82	2	0	16	132	820	0	0	14	43	27	1	0	1941		
Trucks		3				4	1						7					1		PHF=	0.96		
Truck %		3%				1%	3%						1%					4%					

72nd Street & West Post Office Drive








Start Time	Southbound					Westbound					Northbound					Eastbound					Totals	
	Left	Through	Right	Ped	Bike	Left	Through	Right	Ped	Bike	Left	Through	Right	Ped	Bike	Left	Through	Right	Ped	Bike		
16:00						8	3		0							2			0		13	
16:15						4	7		0							5			0		16	
16:30						6	5		1							3			0		15	
16:45						4	9		0							8			0		21	65
17:00						3	7		0							8			0		18	70
17:15						3	11		1							9			0		24	78
17:30						1	7		0							6			1		15	78
17:45						0	7		0							3			0		10	67
Totals	0	0	0	0	0	16	32	0	2	0	0	0	0	0	0	0	28	0	0	0	78	
Trucks							1										1					
Truck %							3%										4%				PHF=	0.81

Broadway & Gladstone Bowl Drive

[illegible]




















3: N Broadway & 72nd Street

Existing AM Peak Hour

							
Lane Group	EBT	WBL	WBT	WBR	NBT	NBR	SBT
Lane Group Flow (vph)	37	257	257	22	65	604	82
v/c Ratio	0.45	0.57	0.57	0.04	0.07	0.54	0.04
Control Delay (s/veh)	39.8	28.0	27.9	0.2	14.9	4.0	14.1
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay (s/veh)	39.8	28.0	27.9	0.2	14.9	4.0	14.1
Queue Length 50th (ft)	11	108	108	0	16	0	10
Queue Length 95th (ft)	38	155	155	0	49	73	29
Internal Link Dist (ft)	204		604		384		28
Turn Bay Length (ft)				25			
Base Capacity (vph)	161	496	499	518	911	1105	1664
Starvation Cap Reductn	0	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0	0
Reduced v/c Ratio	0.23	0.52	0.52	0.04	0.07	0.55	0.05
Intersection Summary							

3: N Broadway & 72nd Street

Existing AM Peak Hour

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (veh/h)	2	20	12	460	18	20	10	50	562	15	60	1
Future Volume (veh/h)	2	20	12	460	18	20	10	50	562	15	60	1
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Lane Width Adj.	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach	No			No			No			No		
Adj Sat Flow, veh/h/ln	1870	1752	1870	1870	1870	1870	1752	1870	1870	1870	1870	1870
Adj Flow Rate, veh/h	2	22	13	509	0	22	11	54	0	16	65	1
Peak Hour Factor	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Percent Heavy Veh, %	2	10	2	2	2	2	10	2	2	2	2	2
Cap, veh/h	3	35	21	691	0	307	199	942		410	1672	26
Arrive On Green	0.04	0.04	0.04	0.19	0.00	0.19	0.61	0.61	0.00	0.61	0.61	0.61
Sat Flow, veh/h	89	977	577	3563	0	1585	234	1543	1585	564	2739	43
Grp Volume(v), veh/h	37	0	0	509	0	22	65	0	0	43	0	39
Grp Sat Flow(s),veh/h/ln	1643	0	0	1781	0	1585	1777	0	1585	1653	0	1694
Q Serve(g_s), s	1.7	0.0	0.0	10.1	0.0	0.9	0.0	0.0	0.0	0.0	0.0	0.7
Cycle Q Clear(g_c), s	1.7	0.0	0.0	10.1	0.0	0.9	1.1	0.0	0.0	0.7	0.0	0.7
Prop In Lane	0.05		0.35	1.00		1.00	0.17		1.00	0.37		0.03
Lane Grp Cap(c), veh/h	59	0	0	691	0	307	1141	0		1075	0	1034
V/C Ratio(X)	0.63	0.00	0.00	0.74	0.00	0.07	0.06	0.00		0.04	0.00	0.04
Avail Cap(c_a), veh/h	438	0	0	950	0	423	1141	0		1075	0	1034
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	0.00	0.00	1.00	0.00	1.00	1.00	0.00	0.00	1.00	0.00	1.00
Uniform Delay (d), s/veh	35.7	0.0	0.0	28.4	0.0	24.7	5.9	0.0	0.0	5.8	0.0	5.8
Incr Delay (d2), s/veh	21.2	0.0	0.0	3.6	0.0	0.2	0.1	0.0	0.0	0.1	0.0	0.1
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	1.0	0.0	0.0	4.4	0.0	0.3	0.4	0.0	0.0	0.3	0.0	0.2
Unsig. Movement Delay, s/veh												
LnGrp Delay(d), s/veh	56.9	0.0	0.0	32.0	0.0	24.9	6.0	0.0	0.0	5.9	0.0	5.9
LnGrp LOS	E			C		C	A			A		A
Approach Vol, veh/h	37			531			65			82		
Approach Delay, s/veh	56.9			31.7			6.0			5.9		
Approach LOS	E			C			A			A		
Timer - Assigned Phs	2			4			6			8		
Phs Duration (G+Y+Rc), s	49.8			6.7			49.8			18.5		
Change Period (Y+Rc), s	4.0			4.0			4.0			4.0		
Max Green Setting (Gmax), s	23.0			20.0			23.0			20.0		
Max Q Clear Time (g_c+l1), s	3.1			3.7			2.7			12.1		
Green Ext Time (p_c), s	0.4			0.2			0.6			2.5		

Intersection Summary

HCM 7th Control Delay, s/veh	27.7
HCM 7th LOS	C




Notes

User approved volume balancing among the lanes for turning movement.

Unsignalized Delay for [NBR] is excluded from calculations of the approach delay and intersection delay.








6: N Broadway & Gladstone Bowl Drive

Existing AM Peak Hour

Intersection						
Int Delay, s/veh	0.1					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	0	0	72	0	1	76
Future Vol, veh/h	0	0	72	0	1	76
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	50	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	79	79	79	79	79	79
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	0	91	0	1	96
Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	142	91	0	0	91	0
Stage 1	91	-	-	-	-	-
Stage 2	51	-	-	-	-	-
Critical Hdwy	6.63	6.23	-	-	4.13	-
Critical Hdwy Stg 1	5.43	-	-	-	-	-
Critical Hdwy Stg 2	5.83	-	-	-	-	-
Follow-up Hdwy	3.519	3.319	-	-	2.219	-
Pot Cap-1 Maneuver	844	966	-	-	1503	-
Stage 1	932	-	-	-	-	-
Stage 2	966	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	843	966	-	-	1503	-
Mov Cap-2 Maneuver	843	-	-	-	-	-
Stage 1	932	-	-	-	-	-
Stage 2	965	-	-	-	-	-
Approach	WB	NB		SB		
HCM Control Delay, s/v	0	0		0.1		
HCM LOS	A					
Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT		
Capacity (veh/h)	-	-	-	47	-	
HCM Lane V/C Ratio	-	-	-	0.001	-	
HCM Control Delay (s/veh)	-	-	0	7.4	0	
HCM Lane LOS	-	-	A	A	A	
HCM 95th %tile Q(veh)	-	-	-	0	-	

3: N Broadway & 72nd Street

Existing PM Peak Hour




















							
Lane Group	EBT	WBL	WBT	WBR	NBT	NBR	SBT
Lane Group Flow (vph)	88	339	342	85	155	854	157
v/c Ratio	0.72	0.70	0.70	0.16	0.21	0.74	0.13
Control Delay (s/veh)	51.3	33.4	33.4	7.8	18.9	6.7	16.9
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay (s/veh)	51.3	33.4	33.4	7.8	18.9	6.7	16.9
Queue Length 50th (ft)	26	134	135	4	53	0	25
Queue Length 95th (ft)	#75	#280	#283	36	100	102	48
Internal Link Dist (ft)	204		604		384		28
Turn Bay Length (ft)				25			
Base Capacity (vph)	171	501	504	523	736	1151	1206
Starvation Cap Reductn	0	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0	0
Reduced v/c Ratio	0.51	0.68	0.68	0.16	0.21	0.74	0.13

Intersection Summary

95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.




3: N Broadway & 72nd Street

Existing PM Peak Hour

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (veh/h)	14	43	27	614	39	82	16	132	820	49	94	8
Future Volume (veh/h)	14	43	27	614	39	82	16	132	820	49	94	8
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Lane Width Adj.	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach	No			No			No			No		
Adj Sat Flow, veh/h/ln	1870	1870	1841	1870	1856	1870	1870	1870	1870	1870	1856	1870
Adj Flow Rate, veh/h	15	45	28	669	0	85	17	138	0	51	98	8
Peak Hour Factor	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Percent Heavy Veh, %	2	2	4	2	3	2	2	2	2	2	3	2
Cap, veh/h	21	63	39	836	0	372	120	905		546	1101	94
Arrive On Green	0.07	0.07	0.07	0.23	0.00	0.23	0.54	0.54	0.00	0.54	0.54	0.54
Sat Flow, veh/h	299	897	558	3563	0	1585	124	1690	1585	874	2055	175
Grp Volume(v), veh/h	88	0	0	669	0	85	155	0	0	81	0	76
Grp Sat Flow(s),veh/h/ln	1755	0	0	1781	0	1585	1814	0	1585	1447	0	1657
Q Serve(g_s), s	3.7	0.0	0.0	13.3	0.0	3.3	0.0	0.0	0.0	0.0	0.0	1.7
Cycle Q Clear(g_c), s	3.7	0.0	0.0	13.3	0.0	3.3	3.1	0.0	0.0	1.6	0.0	1.7
Prop In Lane	0.17		0.32	1.00		1.00	0.11		1.00	0.63		0.11
Lane Grp Cap(c), veh/h	122	0	0	836	0	372	1025	0		854	0	888
V/C Ratio(X)	0.72	0.00	0.00	0.80	0.00	0.23	0.15	0.00		0.10	0.00	0.09
Avail Cap(c_a), veh/h	468	0	0	950	0	423	1025	0		854	0	888
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	0.00	0.00	1.00	0.00	1.00	1.00	0.00	0.00	1.00	0.00	1.00
Uniform Delay (d), s/veh	34.2	0.0	0.0	27.0	0.0	23.2	8.8	0.0	0.0	8.5	0.0	8.5
Incr Delay (d2), s/veh	15.6	0.0	0.0	5.5	0.0	0.7	0.3	0.0	0.0	0.2	0.0	0.2
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	2.0	0.0	0.0	5.9	0.0	1.2	1.2	0.0	0.0	0.6	0.0	0.6
Unsig. Movement Delay, s/veh												
LnGrp Delay(d), s/veh	49.7	0.0	0.0	32.6	0.0	23.9	9.1	0.0	0.0	8.7	0.0	8.7
LnGrp LOS	D			C		C	A			A		A
Approach Vol, veh/h	88			754			155			157		
Approach Delay, s/veh	49.7			31.6			9.1			8.7		
Approach LOS	D			C			A			A		
Timer - Assigned Phs	2			4			6			8		
Phs Duration (G+Y+Rc), s	44.2			9.2			44.2			21.6		
Change Period (Y+Rc), s	4.0			4.0			4.0			4.0		
Max Green Setting (Gmax), s	23.0			20.0			23.0			20.0		
Max Q Clear Time (g_c+l1), s	5.1			5.7			3.7			15.3		
Green Ext Time (p_c), s	1.3			0.5			1.4			2.3		
Intersection Summary												
HCM 7th Control Delay, s/veh	26.9											
HCM 7th LOS	C											
Notes												
User approved volume balancing among the lanes for turning movement.												
Unsignalized Delay for [NBR] is excluded from calculations of the approach delay and intersection delay.												

6: N Broadway & Gladstone Bowl Drive

Existing PM Peak Hour

Intersection						
Int Delay, s/veh	0.8					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	13	9	220	8	10	138
Future Vol, veh/h	13	9	220	8	10	138
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	50	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	82	82	82	82	82	82
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	16	11	268	10	12	168
Major/Minor	Minor1	Major1		Major2		
Conflicting Flow All	382	273	0	0	278	0
Stage 1	273	-	-	-	-	-
Stage 2	109	-	-	-	-	-
Critical Hdwy	6.63	6.23	-	-	4.13	-
Critical Hdwy Stg 1	5.43	-	-	-	-	-
Critical Hdwy Stg 2	5.83	-	-	-	-	-
Follow-up Hdwy	3.519	3.319	-	-	2.219	-
Pot Cap-1 Maneuver	607	765	-	-	1283	-
Stage 1	772	-	-	-	-	-
Stage 2	904	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	601	765	-	-	1283	-
Mov Cap-2 Maneuver	601	-	-	-	-	-
Stage 1	772	-	-	-	-	-
Stage 2	896	-	-	-	-	-
Approach	WB	NB		SB		
HCM Control Delay, s/v	10.7	0		0.59		
HCM LOS	B					
Minor Lane/Major Mvmt	NBT	NBRWBLn1		SBL	SBT	
Capacity (veh/h)	-	-		659	243	-
HCM Lane V/C Ratio	-	-		0.041	0.01	-
HCM Control Delay (s/veh)	-	-		10.7	7.8	0.1
HCM Lane LOS	-	-		B	A	A
HCM 95th %tile Q(veh)	-	-		0.1	0	-

3: N Broadway & 72nd Street

Existing + Proposed Development AM Peak Hour






















Lane Group	EBT	WBL	WBT	WBR	NBT	NBR	SBT
Lane Group Flow (vph)	62	240	243	67	133	552	182
v/c Ratio	0.64	0.55	0.56	0.14	0.15	0.51	0.12
Control Delay (s/veh)	50.7	28.3	28.3	5.2	15.0	3.9	13.8
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay (s/veh)	50.7	28.3	28.3	5.2	15.0	3.9	13.8
Queue Length 50th (ft)	16	102	103	0	35	0	24
Queue Length 95th (ft)	#64	151	153	22	88	69	56
Internal Link Dist (ft)	204		604		384		28
Turn Bay Length (ft)				25			
Base Capacity (vph)	165	488	492	511	880	1078	1488
Starvation Cap Reductn	0	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0	0
Reduced v/c Ratio	0.38	0.49	0.49	0.13	0.15	0.51	0.12

Intersection Summary

95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.




3: N Broadway & 72nd Street

Existing + Proposed Development AM Peak Hour

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (veh/h)	2	33	23	420	29	62	23	100	513	65	103	1
Future Volume (veh/h)	2	33	23	420	29	62	23	100	513	65	103	1
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Lane Width Adj.	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1870	1752	1870	1870	1870	1870	1752	1870	1870	1870	1870	1870
Adj Flow Rate, veh/h	2	35	25	474	0	67	25	108	0	70	111	1
Peak Hour Factor	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Percent Heavy Veh, %	2	10	2	2	2	2	10	2	2	2	2	2
Cap, veh/h	3	46	33	665	0	296	215	897		712	1239	12
Arrive On Green	0.05	0.05	0.05	0.19	0.00	0.19	0.60	0.60	0.00	0.60	0.60	0.60
Sat Flow, veh/h	53	921	658	3563	0	1585	262	1487	1585	1042	2054	19
Grp Volume(v), veh/h	62	0	0	474	0	67	133	0	0	93	0	89
Grp Sat Flow(s),veh/h/ln	1631	0	0	1781	0	1585	1750	0	1585	1416	0	1699
Q Serve(g_s), s	2.8	0.0	0.0	9.4	0.0	2.7	0.0	0.0	0.0	0.0	0.0	1.6
Cycle Q Clear(g_c), s	2.8	0.0	0.0	9.4	0.0	2.7	2.3	0.0	0.0	1.6	0.0	1.6
Prop In Lane	0.03		0.40	1.00		1.00	0.19		1.00	0.75		0.01
Lane Grp Cap(c), veh/h	81	0	0	665	0	296	1113	0		938	0	1025
V/C Ratio(X)	0.76	0.00	0.00	0.71	0.00	0.23	0.12	0.00		0.10	0.00	0.09
Avail Cap(c_a), veh/h	435	0	0	950	0	423	1113	0		938	0	1025
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	0.00	0.00	1.00	0.00	1.00	1.00	0.00	0.00	1.00	0.00	1.00
Uniform Delay (d), s/veh	35.2	0.0	0.0	28.6	0.0	25.9	6.4	0.0	0.0	6.2	0.0	6.2
Incr Delay (d2), s/veh	26.3	0.0	0.0	3.0	0.0	0.8	0.2	0.0	0.0	0.2	0.0	0.2
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	1.7	0.0	0.0	4.1	0.0	1.0	0.8	0.0	0.0	0.6	0.0	0.5
Unsig. Movement Delay, s/veh												
LnGrp Delay(d), s/veh	61.5	0.0	0.0	31.6	0.0	26.7	6.6	0.0	0.0	6.4	0.0	6.4
LnGrp LOS	E			C		C	A			A		A
Approach Vol, veh/h		62			541			133			182	
Approach Delay, s/veh		61.5			31.0			6.6			6.4	
Approach LOS		E			C			A			A	
Timer - Assigned Phs		2		4		6		8				
Phs Duration (G+Y+Rc), s		49.3		7.7		49.3		18.0				
Change Period (Y+Rc), s		4.0		4.0		4.0		4.0				
Max Green Setting (Gmax), s		23.0		20.0		23.0		20.0				
Max Q Clear Time (g_c+l1), s		4.3		4.8		3.6		11.4				
Green Ext Time (p_c), s		1.1		0.3		1.7		2.6				
Intersection Summary												
HCM 7th Control Delay, s/veh			24.7									
HCM 7th LOS			C									
Notes												
User approved volume balancing among the lanes for turning movement.												
Unsignalized Delay for [NBR] is excluded from calculations of the approach delay and intersection delay.												

6: N Broadway & Gladstone Bowl Drive

Existing + Proposed Development AM Peak Hour

Intersection						
Int Delay, s/veh	0					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	0	0	164	0	1	169
Future Vol, veh/h	0	0	164	0	1	169
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	50	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	79	79	79	79	79	79
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	0	208	0	1	214
Major/Minor	Minor1	Major1		Major2		
Conflicting Flow All	317	208	0	0	208	0
Stage 1	208	-	-	-	-	-
Stage 2	109	-	-	-	-	-
Critical Hdwy	6.63	6.23	-	-	4.13	-
Critical Hdwy Stg 1	5.43	-	-	-	-	-
Critical Hdwy Stg 2	5.83	-	-	-	-	-
Follow-up Hdwy	3.519	3.319	-	-	2.219	-
Pot Cap-1 Maneuver	663	832	-	-	1362	-
Stage 1	826	-	-	-	-	-
Stage 2	903	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	663	832	-	-	1362	-
Mov Cap-2 Maneuver	663	-	-	-	-	-
Stage 1	826	-	-	-	-	-
Stage 2	903	-	-	-	-	-
Approach	WB	NB		SB		
HCM Control Delay, s/v	0	0		0.05		
HCM LOS	A					
Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT		
Capacity (veh/h)	-	-	-	21	-	
HCM Lane V/C Ratio	-	-	-	0.001	-	
HCM Control Delay (s/veh)	-	-	0	7.6	0	
HCM Lane LOS	-	-	A	A	A	
HCM 95th %tile Q(veh)	-	-	-	0	-	





8: West Post Office Drive/West Drive & 72nd Street

Existing + Proposed Development AM Peak Hour

Intersection												
Int Delay, s/veh	3.4											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕					↕	↕	
Traffic Vol, veh/h	5	10	2	4	12	26	0	0	0	27	0	4
Future Vol, veh/h	5	10	2	4	12	26	0	0	0	27	0	4
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	92	61	61	61	61	92	61	92	61	92	92	92
Heavy Vehicles, %	2	15	2	2	14	2	2	2	2	2	2	2
Mvmt Flow	5	16	3	7	20	28	0	0	0	29	0	4
Major/Minor	Major1			Major2			Minor2					
Conflicting Flow All	48	0	0	20	0	0				74	77	34
Stage 1	-	-	-	-	-	-				47	47	-
Stage 2	-	-	-	-	-	-				27	31	-
Critical Hdwy	4.12	-	-	4.12	-	-				6.42	6.52	6.22
Critical Hdwy Stg 1	-	-	-	-	-	-				5.42	5.52	-
Critical Hdwy Stg 2	-	-	-	-	-	-				5.42	5.52	-
Follow-up Hdwy	2.218	-	-	2.218	-	-				3.518	4.018	3.318
Pot Cap-1 Maneuver	1559	-	-	1597	-	-				929	813	1039
Stage 1	-	-	-	-	-	-				976	856	-
Stage 2	-	-	-	-	-	-				995	870	-
Platoon blocked, %		-	-		-	-						
Mov Cap-1 Maneuver	1559	-	-	1597	-	-				922	0	1039
Mov Cap-2 Maneuver	-	-	-	-	-	-				922	0	-
Stage 1	-	-	-	-	-	-				972	0	-
Stage 2	-	-	-	-	-	-				991	0	-
Approach	EB			WB			SB					
HCM Control Delay, s/v	1.58			0.87			8.96					
HCM LOS							A					
Minor Lane/Major Mvmt	EBL	EBT	EBR	WBL	WBT	WBR	SBLn1	SBLn2				
Capacity (veh/h)	377	-	-	194	-	-	922	1039				
HCM Lane V/C Ratio	0.003	-	-	0.004	-	-	0.032	0.004				
HCM Control Delay (s/veh)	7.3	0	-	7.3	0	-	9	8.5				
HCM Lane LOS	A	A	-	A	A	-	A	A				
HCM 95th %tile Q(veh)	0	-	-	0	-	-	0.1	0				

10: N Broadway & North Drive

Existing + Proposed Development AM Peak Hour

Intersection						
Int Delay, s/veh	5					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Vol, veh/h	12	99	99	65	71	11
Future Vol, veh/h	12	99	99	65	71	11
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	-	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	13	108	108	71	77	12
Major/Minor	Minor2	Major1		Major2		
Conflicting Flow All	369	83	89	0	-	0
Stage 1	83	-	-	-	-	-
Stage 2	286	-	-	-	-	-
Critical Hdwy	6.42	6.22	4.12	-	-	-
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-	-
Follow-up Hdwy	3.518	3.318	2.218	-	-	-
Pot Cap-1 Maneuver	631	976	1506	-	-	-
Stage 1	940	-	-	-	-	-
Stage 2	763	-	-	-	-	-
Platoon blocked, %				-	-	-
Mov Cap-1 Maneuver	584	976	1506	-	-	-
Mov Cap-2 Maneuver	584	-	-	-	-	-
Stage 1	870	-	-	-	-	-
Stage 2	763	-	-	-	-	-
Approach	EB	NB		SB		
HCM Control Delay, s/v	9.38	4.57		0		
HCM LOS	A					
Minor Lane/Major Mvmt	NBL	NBT	EBLn1	EBLn2	SBT	SBR
Capacity (veh/h)	1087	-	584	976	-	-
HCM Lane V/C Ratio	0.071	-	0.022	0.11	-	-
HCM Control Delay (s/veh)	7.6	0	11.3	9.1	-	-
HCM Lane LOS	A	A	B	A	-	-
HCM 95th %tile Q(veh)	0.2	-	0.1	0.4	-	-

3: N Broadway & 72nd Street

Existing + Proposed Development PM Peak Hour























Lane Group	EBT	WBL	WBT	WBR	NBT	NBR	SBT
Lane Group Flow (vph)	110	327	329	123	213	809	241
v/c Ratio	0.77	0.70	0.70	0.25	0.29	0.72	0.21
Control Delay (s/veh)	53.8	33.8	33.6	11.2	20.0	6.2	18.0
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay (s/veh)	53.8	33.8	33.6	11.2	20.0	6.2	18.0
Queue Length 50th (ft)	33	129	130	16	77	0	43
Queue Length 95th (ft)	#99	#265	#266	57	135	96	72
Internal Link Dist (ft)	204		604		384		28
Turn Bay Length (ft)				25			
Base Capacity (vph)	187	488	492	511	712	1123	1104
Starvation Cap Reductn	0	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0	0
Reduced v/c Ratio	0.59	0.67	0.67	0.24	0.30	0.72	0.22

Intersection Summary

95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

3: N Broadway & 72nd Street

Existing + Proposed Development PM Peak Hour

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (veh/h)	14	55	36	582	48	118	28	177	777	93	131	8
Future Volume (veh/h)	14	55	36	582	48	118	28	177	777	93	131	8
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Lane Width Adj.	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach	No			No			No			No		
Adj Sat Flow, veh/h/ln	1870	1870	1841	1870	1856	1870	1870	1870	1870	1870	1856	1870
Adj Flow Rate, veh/h	15	57	38	642	0	123	29	184	0	97	136	8
Peak Hour Factor	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Percent Heavy Veh, %	2	2	4	2	3	2	2	2	2	2	3	2
Cap, veh/h	21	79	53	820	0	365	141	847		631	964	58
Arrive On Green	0.09	0.09	0.09	0.23	0.00	0.23	0.52	0.52	0.00	0.52	0.52	0.52
Sat Flow, veh/h	239	907	604	3563	0	1585	166	1622	1585	1043	1846	112
Grp Volume(v), veh/h	110	0	0	642	0	123	213	0	0	122	0	119
Grp Sat Flow(s),veh/h/ln	1750	0	0	1781	0	1585	1787	0	1585	1333	0	1668
Q Serve(g_s), s	4.6	0.0	0.0	12.7	0.0	4.9	0.0	0.0	0.0	0.0	0.0	2.8
Cycle Q Clear(g_c), s	4.6	0.0	0.0	12.7	0.0	4.9	4.6	0.0	0.0	2.7	0.0	2.8
Prop In Lane	0.14		0.35	1.00		1.00	0.14		1.00	0.80		0.07
Lane Grp Cap(c), veh/h	153	0	0	820	0	365	988	0		783	0	872
V/C Ratio(X)	0.72	0.00	0.00	0.78	0.00	0.34	0.22	0.00		0.16	0.00	0.14
Avail Cap(c_a), veh/h	467	0	0	950	0	423	988	0		783	0	872
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	0.00	0.00	1.00	0.00	1.00	1.00	0.00	0.00	1.00	0.00	1.00
Uniform Delay (d), s/veh	33.3	0.0	0.0	27.1	0.0	24.1	9.7	0.0	0.0	9.2	0.0	9.2
Incr Delay (d2), s/veh	12.7	0.0	0.0	4.9	0.0	1.2	0.5	0.0	0.0	0.4	0.0	0.3
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	2.4	0.0	0.0	5.6	0.0	1.8	1.8	0.0	0.0	1.0	0.0	1.0
Unsig. Movement Delay, s/veh												
LnGrp Delay(d), s/veh	46.0	0.0	0.0	32.0	0.0	25.2	10.2	0.0	0.0	9.6	0.0	9.5
LnGrp LOS	D			C		C	B			A		A
Approach Vol, veh/h	110			765			213			241		
Approach Delay, s/veh	46.0			30.9			10.2			9.6		
Approach LOS	D			C			B			A		
Timer - Assigned Phs	2			4			6			8		
Phs Duration (G+Y+Rc), s	43.2			10.6			43.2			21.3		
Change Period (Y+Rc), s	4.0			4.0			4.0			4.0		
Max Green Setting (Gmax), s	23.0			20.0			23.0			20.0		
Max Q Clear Time (g_c+I1), s	6.6			6.6			4.8			14.7		
Green Ext Time (p_c), s	1.8			0.7			2.3			2.6		

Intersection Summary

HCM 7th Control Delay, s/veh	25.0
HCM 7th LOS	C




Notes

User approved volume balancing among the lanes for turning movement.

Unsignalized Delay for [NBR] is excluded from calculations of the approach delay and intersection delay.

6: N Broadway & Gladstone Bowl Drive

Existing + Proposed Development PM Peak Hour

Intersection						
Int Delay, s/veh	0.6					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	13	9	301	8	10	219
Future Vol, veh/h	13	9	301	8	10	219
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	50	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	82	82	82	82	82	82
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	16	11	367	10	12	267
Major/Minor	Minor1	Major1		Major2		
Conflicting Flow All	530	372	0	0	377	0
Stage 1	372	-	-	-	-	-
Stage 2	158	-	-	-	-	-
Critical Hdwy	6.63	6.23	-	-	4.13	-
Critical Hdwy Stg 1	5.43	-	-	-	-	-
Critical Hdwy Stg 2	5.83	-	-	-	-	-
Follow-up Hdwy	3.519	3.319	-	-	2.219	-
Pot Cap-1 Maneuver	494	673	-	-	1180	-
Stage 1	696	-	-	-	-	-
Stage 2	855	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	489	673	-	-	1180	-
Mov Cap-2 Maneuver	489	-	-	-	-	-
Stage 1	696	-	-	-	-	-
Stage 2	846	-	-	-	-	-
Approach	WB	NB		SB		
HCM Control Delay, s/v11.87		0		0.43		
HCM LOS	B					
Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT		
Capacity (veh/h)	-	-	551	157	-	
HCM Lane V/C Ratio	-	-	0.049	0.01	-	
HCM Control Delay (s/veh)	-	-	11.9	8.1	0.1	
HCM Lane LOS	-	-	B	A	A	
HCM 95th %tile Q(veh)	-	-	0.2	0	-	

8: West Post Office Drive & 72nd Street

Existing + Proposed Development PM Peak Hour

Intersection												
Int Delay, s/veh	3.3											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕					↕	↕	
Traffic Vol, veh/h	6	24	0	16	29	24	0	0	0	25	0	5
Future Vol, veh/h	6	24	0	16	29	24	0	0	0	25	0	5
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	92	81	81	81	81	92	81	92	81	92	92	92
Heavy Vehicles, %	2	4	2	2	3	2	2	2	2	2	2	2
Mvmt Flow	7	30	0	20	36	26	0	0	0	27	0	5
Major/Minor	Major1			Major2			Minor2					
Conflicting Flow All	62	0	0	30	0	0				131	131	49
Stage 1	-	-	-	-	-	-				88	88	-
Stage 2	-	-	-	-	-	-				43	43	-
Critical Hdwy	4.12	-	-	4.12	-	-				6.42	6.52	6.22
Critical Hdwy Stg 1	-	-	-	-	-	-				5.42	5.52	-
Critical Hdwy Stg 2	-	-	-	-	-	-				5.42	5.52	-
Follow-up Hdwy	2.218	-	-	2.218	-	-				3.518	4.018	3.318
Pot Cap-1 Maneuver	1541	-	-	1583	-	-				863	760	1020
Stage 1	-	-	-	-	-	-				935	822	-
Stage 2	-	-	-	-	-	-				980	859	-
Platoon blocked, %		-	-		-	-						
Mov Cap-1 Maneuver	1541	-	-	1583	-	-				848	0	1020
Mov Cap-2 Maneuver	-	-	-	-	-	-				848	0	-
Stage 1	-	-	-	-	-	-				931	0	-
Stage 2	-	-	-	-	-	-				967	0	-
Approach	EB			WB			SB					
HCM Control Delay, s/v	1.33			1.77			9.25					
HCM LOS							A					
Minor Lane/Major Mvmt	EBL	EBT	EBR	WBL	WBT	WBR	SBLn1	SBLn2				
Capacity (veh/h)	325	-	-	402	-	-	848	1020				
HCM Lane V/C Ratio	0.004	-	-	0.012	-	-	0.032	0.005				
HCM Control Delay (s/veh)	7.3	0	-	7.3	0	-	9.4	8.5				
HCM Lane LOS	A	A	-	A	A	-	A	A				
HCM 95th %tile Q(veh)	0	-	-	0	-	-	0.1	0				

10: N Broadway & North Drive

Existing + Proposed Development PM Peak Hour

Intersection

Int Delay, s/veh 3.2

Movement	EBL	EBR	NBL	NBT	SBT	SBR
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Lane Configurations						
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Traffic Vol, veh/h	18	89	93	217	140	13
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Future Vol, veh/h	18	89	93	217	140	13
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Conflicting Peds, #/hr	0	0	0	0	0	0
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Sign Control	Stop	Stop	Free	Free	Free	Free
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RT Channelized	-	None	-	None	-	None
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Storage Length	-	-	-	-	-	-
----------------	---	---	---	---	---	---

Veh in Median Storage, #	0	-	-	0	0	-
--------------------------	---	---	---	---	---	---

Grade, %	0	-	-	0	0	-
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Peak Hour Factor	92	92	92	92	92	92
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Heavy Vehicles, %	2	2	2	2	2	2
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Mvmt Flow	20	97	101	236	152	14
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Major/Minor	Minor2	Major1	Major2
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Conflicting Flow All	597	159	166	0	-	0
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Stage 1	159	-	-	-	-	-
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Stage 2	438	-	-	-	-	-
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Critical Hdwy	6.42	6.22	4.12	-	-	-
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Critical Hdwy Stg 1	5.42	-	-	-	-	-
---------------------	------	---	---	---	---	---

Critical Hdwy Stg 2	5.42	-	-	-	-	-
---------------------	------	---	---	---	---	---

Follow-up Hdwy	3.518	3.318	2.218	-	-	-
----------------	-------	-------	-------	---	---	---

Pot Cap-1 Maneuver	466	886	1412	-	-	-
--------------------	-----	-----	------	---	---	---

Stage 1	869	-	-	-	-	-
---------	-----	---	---	---	---	---

Stage 2	650	-	-	-	-	-
---------	-----	---	---	---	---	---

Platoon blocked, %				-	-	-
--------------------	--	--	--	---	---	---

Mov Cap-1 Maneuver	427	886	1412	-	-	-
--------------------	-----	-----	------	---	---	---

Mov Cap-2 Maneuver	427	-	-	-	-	-
--------------------	-----	---	---	---	---	---

Stage 1	798	-	-	-	-	-
---------	-----	---	---	---	---	---

Stage 2	650	-	-	-	-	-
---------	-----	---	---	---	---	---

Approach	EB	NB	SB
----------	----	----	----

HCM Control Delay, s/v10.28		2.32	0
-----------------------------	--	------	---

HCM LOS	B		
---------	---	--	--

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	EBLn2	SBT	SBR
-----------------------	-----	-----	-------	-------	-----	-----

Capacity (veh/h)	540	-	427	886	-	-
------------------	-----	---	-----	-----	---	---

HCM Lane V/C Ratio	0.072	-	0.046	0.109	-	-
--------------------	-------	---	-------	-------	---	---

HCM Control Delay (s/veh)	7.7	0	13.8	9.6	-	-
---------------------------	-----	---	------	-----	---	---

HCM Lane LOS	A	A	B	A	-	-
--------------	---	---	---	---	---	---

HCM 95th %tile Q(veh)	0.2	-	0.1	0.4	-	-
-----------------------	-----	---	-----	-----	---	---

Drainage Report
For
400 NW 72nd Street
Gladstone, Missouri

April 01, 2024

By:
Gerald W. Menefee, PE
KAM Design LLC
9000 Bannister Road
Kansas City, Missouri 64134

menefeegerald@gmail.com



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Section 1 General

The proposed site for a new convenience store with gasoline pumps is just northwest corner of the intersection of N Broadway and NW 72nd Street in Gladstone, Missouri. The tract of land is currently covered by grassland. The developed portion of the site is expected to cover approximately the south two thirds of the site.

Section 2 Methodology

HydroCAD 10.00 was utilized for the drainage calculations developed for this project. The Water Quality solution was developed utilizing Manual of Best Management Practices for Stormwater Quality, October 2012 edition.

Section 3 Existing Drainage Patterns

From the peak elevation of the site located near the southeast corner of the site, there are three basins radiating out from it. Reference Maps Section. Basins E1 generally exhibits flow toward the west side of the property; Basin E2 drains to the east part of the property; while Basin E3 drains toward the west side of the site. Table 1 shows the amounts of existing runoff from each of the basins for the 1-year, 10-year and 100-year storms are as follows:

**Table 1
Existing Site Runoff**

Storm Year	Basin E1 (cfs)	Basin E2 (cfs)	Basin E3 (cfs)	Total Site (cfs)
1	0.66	0.03	1.53	2.22
10	2.04	0.08	4.62	6.74
100	3.65	0.15	8.24	12.04

Proposed Drainage Patterns Section 4

The proposed drainage patterns are consolidated into six basins. Reference the Maps Section. The north or 1P Basin allows for runoff to flow toward the north edge of the property and thence to the Bioretention Bed located to its immediate north. Basins 2P and 3P are much smaller basins

draining to the west. The Basin 4P Generally drains that portion of the east property. The P5 Basin is the water quality Bioretention Area and land immediately around. It drains excess runoff to the sites underground detention system. The area surrounding P5 is comprised of P6 land which is uncontrolled drainage to the west side of the property. A summary of the proposed runoff expected from the site for the 1-year, 10-year and 100-year storms are noted in Table 2. The calculated detention depth and storage are noted in Table 3 as follows:

**Table 2
Proposed Site Runoff**

Storm Year	Basin 1P (cfs)	Basin 1P And 5P w/ Detention (cfs)	Basin 2P (cfs)	Basin 3P (cfs)	Basin 4P (cfs)	Basin 5P (cfs)	Basin 6P (cfs)	Total Site w/ Detention (cfs)
1	4.33	1.70	0.01	0.01	0.27	0.23	0.23	2.06
10	8.53	5.20	0.03	0.03	0.82	0.70	0.61	5.38
100	12.83	8.78	0.06	0.06	1.45	1.23	1.23	10.81

**Table 3
Detention Depth and Storage**

Storm Year	Detained Depth (ft)	Detained Volume (ac-ft)
1	1.02	0.064
10	1.71	0.126
100	5.98	0.177

**Table 4
Final Detention Volume Minus the WQv Volume**

	Calculated Detention Volume	WQv Volume Stored	Final Detention Volume
Acre-Feet Volumes	0.211 ac-ft	0.081 ac-ft	0.13 ac- ft
Linear Feet of Pipe	1300.00 Lf	499.00 Lf	801.00 Lf

As a part of this analysis, it was assumed that the outflow pipe of the detention basin would consist of a 12-inch diameter PVC pipe. As can be seen in the Tables 1 that at all storm levels

the 12-inch PVC pipe provides an adequate release of water so that the discharge in the post developed situation results in the sites runoff being less than the existing runoff.

As for an emergency spillover, it shall be incorporated as a part of the discharge of the 12-inch PVC pipe. The pipe can handle the excess flow by allowing the water in the inlet structure to exceed the height of the orifice plate and travel down through the 12-inch discharge pipe.

The total detention utilized for the site incorporates a reduction in volume. See Table 4. This reduction is predicated on the assumption that the runoff stored in the Bioretention area is effectively detained water and therefore extra volume was left in the detention system pipes.

Section 5 Water Quality

Water quality goals for the site will be achieved through the use Bioretention Area. The area is located to immediate north of drainage basin P1. Runoff water will fill the Area with runoff to a depth of 1 foot. Once this volume is achieved, excess water over the maximum depth of the subsurface storage area flows in an into an inlet structure located at the southwest portion of the Area corner of the property and then into the detention piping.

Water in the Bioretention Area is to drain down the through a 3- inch cover of hardwood wood chips and thence through a 4-foot-thick layer of porous soil. Runoff will be removed from the Area utilizing a system of perforated 4-inch PVC pipes to allow water to leave and travel to a point of daylight. The Area is constructed to allow for the minimum drawdown of one foot per day.

Section 6 Summary

The proposed new improvements on will increase impervious cover necessitating the need for a detention facility to control the additional runoff generated. Since there is insufficient area to construct a detention pond on the surface, it was determined that a subsurface pipe system should be constructed on the north side of the developed portion of the site. A bio retention pond is too be constructed just before the runoff is directed to the detention system in order to allow for the treatment of the first flush of rain water.

Section 7

Conclusions and Recommendations

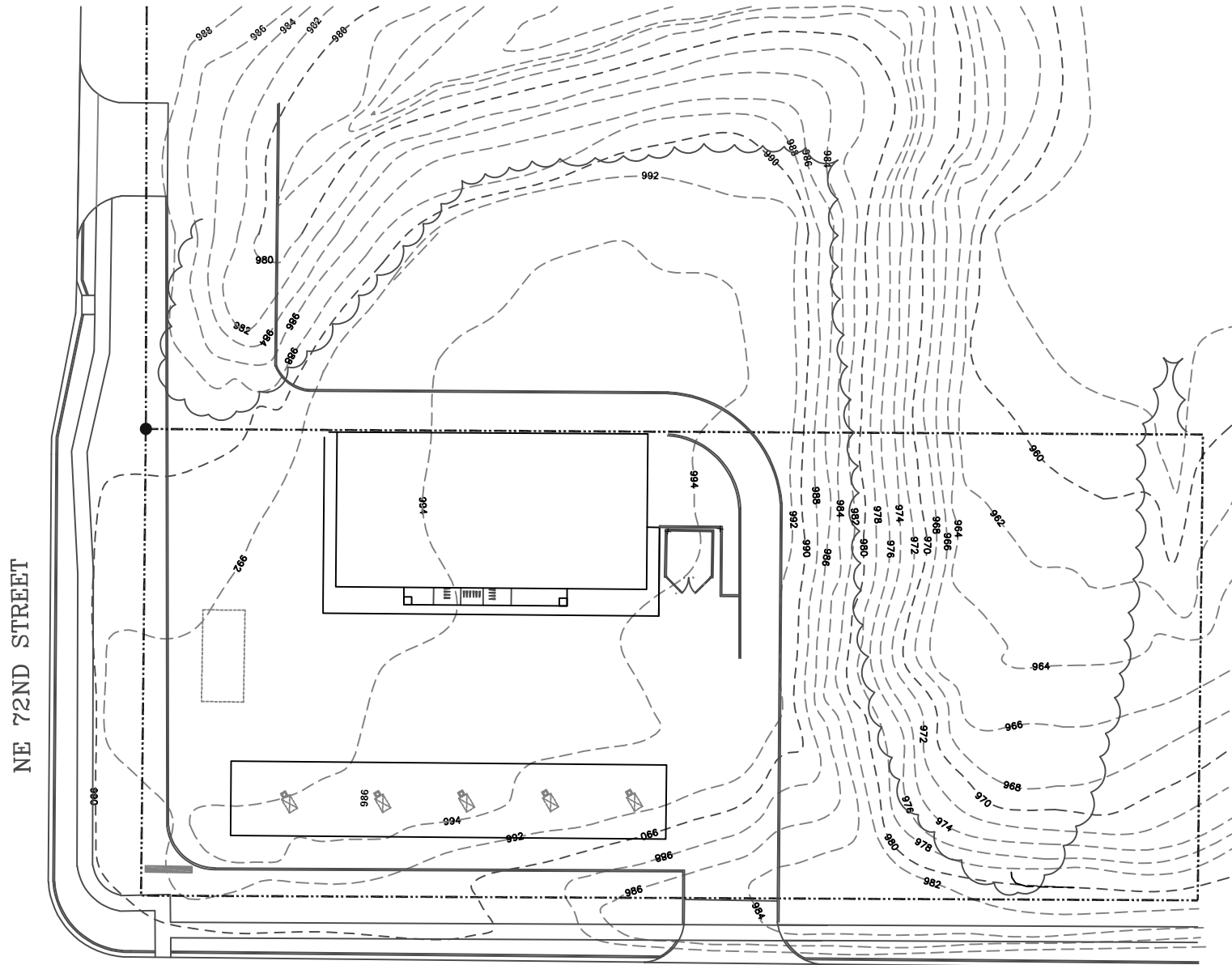
Based upon review of the site involving existing and proposed conditions, conclusions and recommendations are provided as follows:

1. Installation of the Bioretention Area will increase the quality of water exiting the site by filtering water leaving the proposed parking areas.
2. Detention will be provided to mitigate the increasing runoff due to the additional impervious cover added to the site.
3. The detention volume was reduced by the storage volume of the water quality storage. Since not doing this would result in the site being penalized by the extra water stored in the water quality structure.
4. Over flow runoff will be incorporated within the discharge piping of the detention control structure.

Section 8
Drainage Area Maps

SHORT STOP GAS STATION

400 N 72ND STREET, GLADSTONE, MISSOURI



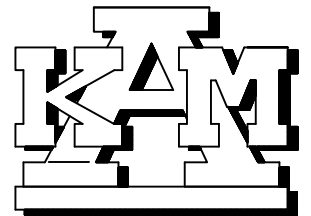
LEGEND

EXISTING CONTOURS

N BROADWAY

EXISTING DRAINAGE AREA MAP

SCALE 1" = 50'

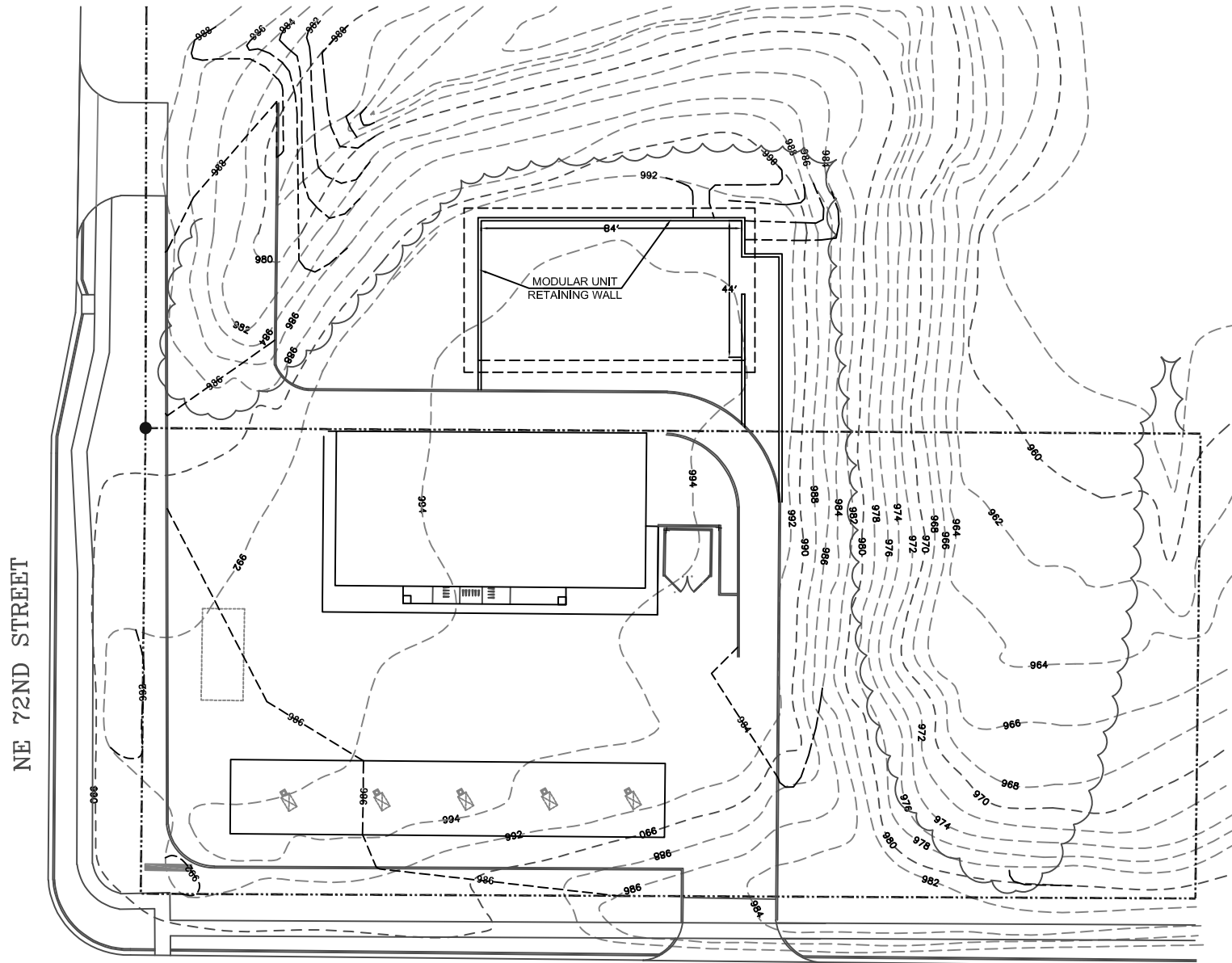


Design Group LLC.


9264 Blue Ridge Blvd.
Suite A

Kansas City, Missouri 64138
(816) 797-2065

SHORT STOP GAS STATION
400 N 72ND STREET, GLADSTONE, MISSOURI



LEGEND

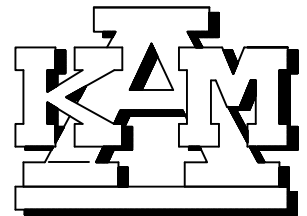
-  EXISTING CONTOURS
 PROPOSED CONTOURS

N BROADWAY



PROPOSED DRAINAGE AREA MAP

SCALE 1' = 50'



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Section 9
Supporting Calculations

Exhibit 1

Water Quality Equations

$$WQ_v = P \cdot R_v \cdot A / 12$$

$$P = 1.37$$

$$I = 68 \%$$

$$R_v = 0.05 + 0.009 \cdot I = 0.05 + 0.009 \cdot 68 =$$

$$A = 0.87$$

$$= 1.37 \cdot 0.62 \cdot 0.87 / 12 = 0.062 \text{ a-ft} = 2665.87 \text{ cf}$$

Refer to Bioretention Worksheet that follows:

Design Procedure Form: Bioretention
Main Worksheet

Designer: GERALD MENEZES
Checked By: GERALD MENEZES
Company: KAM DESIGN LLC
Date: 2/21/23
Project: SHORE STOP GAS STATION
Location: 400 NW 72ND STREET

I. Water Quality Volume

Step 1) Tributary area to bioretention area, A_T (ac)

A_T (ac) = 1.207

Step 2) Calculate WQv using methodology in Section 6

WQv (cu-ft) = 0.91

Ila. Pretreatment

Step 1) Specify type of inflow to Bioretention facility:

Type 1 = sheet flow

Type 2 = concentrated or channelized

Inflow type = TYPE 1

Step 2) Pretreatment

Step 3) Proceed to Part IIb, IIc, or IId for design guidance on different pretreatment options

IIb. Vegetated Pretreatment Strip

Step 1) Type of land cover of contributing area:

Type 1 = Impervious (i.e., parking lot)

Type 2 = Pervious (i.e., residential lawn)

Land cover type = TYPE 1

Step 2) Maximum inflow approach length, L_{approach} (ft)

L_{approach} (ft) = 30

Step 3) Average slope of pretreatment strip, S_{fs} (%)

(Maximum slope of 6%)

S_{fs} (%) = 2%

Step 4) Vegetated pretreatment strip minimum length, L_{fs} (ft), from Table 8.2

L_{fs} (ft) = 30

IIc. Vegetated Pretreatment Channel

Step 1) Percent imperviousness of contributing area, % imp

% imp = 68

Step 2) Average slope of vegetated channel, S_{vc} (%)

(Maximum slope of 6%)

S_{vc} (%) = 2%

Step 3) Vegetated pretreatment channel minimum length, L_{vc} (ft), from Table 8.3

L_{vc} (ft) = 30

IId. Other Pretreatment Devices

Other methods of pretreatment may be utilized upstream of a bioretention facility to settle out suspended solids and reduce runoff velocity. Several proprietary devices are available that will achieve these results. Most such devices install below ground and accept inflow from a piped stormwater management system or from surface sheet flow via drop inlets. These devices should be selected and sized based on site-specific conditions for each project.

Design Procedure Form: Bioretention
Main Worksheet

Designer: GERALD MENERES
Checked By: GERALD MENERES
Company: KAM DESIGN LLC
Date: 7/21/23
Project: SHORT STOP GAS STATION
Location: 400 NW 72ND STREET

III. Planting Soil Bed and Ponding Area

- Step 1) Planting bed soil depth, d_f (ft)
(d_f should be between 2.5 feet and 4 feet). d_f (ft) = 4
- Step 2) Coefficient of permeability for planting soil bed, k (ft/day)
(k should be at least 1 ft/day) k (ft/day) = 1
- Step 3) Maximum ponding depth, h_{max} (ft)
(h_{max} should be between 0.25 ft and 1.0 ft). h_{max} (ft) = 1
- Step 4) Average height of water above bioretention bed, h_{avg} (ft)
 $h_{avg} = h_{max}/2$ h_{avg} (ft) = 0.5
- Step 5) Time required for WQv to filter through the planting soil bed, t_f (days)
(t_f of 1 to 3 days is recommended) t_f (days) = 1
- Step 6) Required filter bed surface area, A_f (ft²)
 $A_f = (WQv \cdot d_f) / [k \cdot t_f \cdot (h_{avg} + d_f)]$ A_f (ft²) = 2370
- Step 7) Approximate filter bed length, L_f (ft), assuming a length to width ratio of 2:1
(L_f should be at least 40 ft) L_f (ft) = 84
- Step 8) Approximate filter bed width, W_f (ft), assuming a length to width ratio of 2:1
(W_f should be at least 15 feet, and optimally half of L_f) W_f (ft) = 42
- Step 9) Required Ponding Area, A_p (sf)
 $A_p = WQv/h_{max}$ A_p (ft²) = 266.00

Design Procedure Form: Bioretention
Main Worksheet

Designer: GERALD MONEPREG
 Checked By: GERALD MONEPREG
 Company: KAM DESIGN LLC
 Date: 7/21/23
 Project: SHORT STOP GAS STATION
 Location: 400 NW 72ND STREET

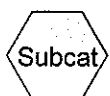
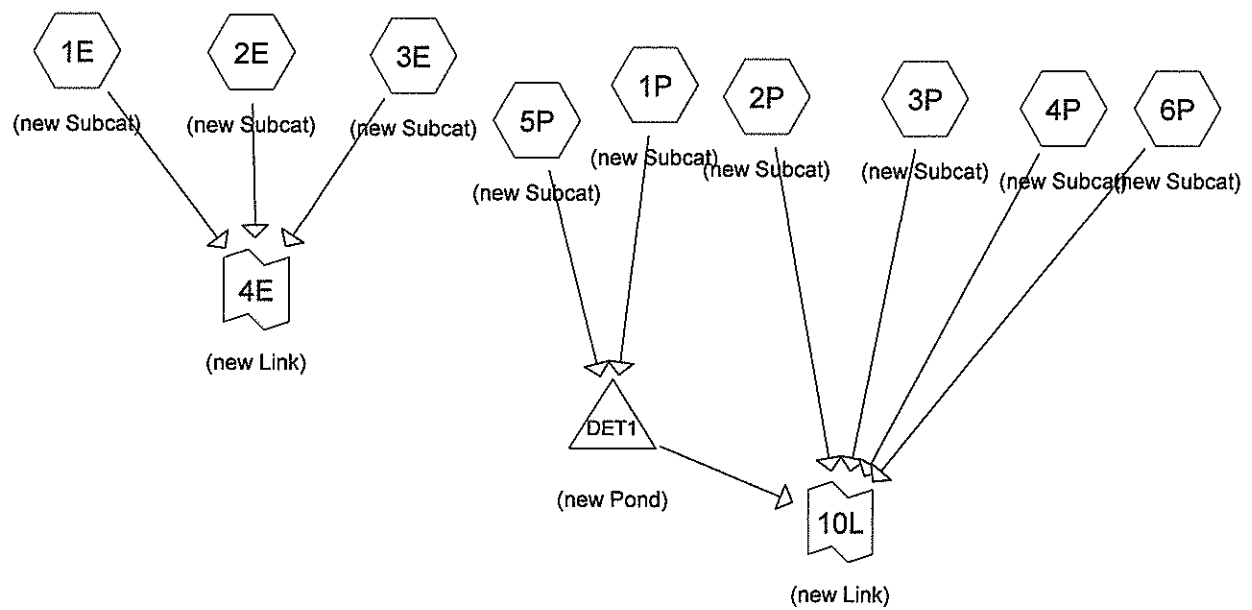
IV. Underdrain

Step 1) Underdrain pipe diameter, D_U (in) (D_U should be at least 4 inches)	D_U (in) = <u>4</u>
Step 2) Depth of gravel blanket, Z_{gravel} (in.) (Z_{gravel} should be at least 8 inches, and at least 2 inches greater than D_U)	Z_{gravel} (in) = <u>12</u>
Step 3) Set underdrain perforation diameters to 0.375 inches.	D_{perf} (in) = <u>0.375</u>
Step 4) Longitudinal center-to-center underdrain perforation spacing, S_{perf} (in)	S_{perf} (in) = <u>14</u>
Step 5) Number of perforations per row (around circumference of underdrain), n_{perf} (n_{perf} should be at least 4)	n_{perf} = <u>4</u>
Step 6) Underdrain collector spacing (approximately 20') S_U (ft)	S_U (ft) = <u>14</u>
Step 7) Pipe grade, G_{pipe} (%), for main pipe and transverse collector pipes (G_{pipe} should be at least 0.5%)	G_{pipe} (%) = <u>0</u>
Step 8) Providing at least one cleanout per pipe run? (Yes or No)	<u>YES</u>
Step 9) Determine design head (h_o) on orifice, $h_o = (d_f + h_{max})/2$	h_o (ft) = <u>2.5</u>
Step 10) Determine Average flow rate, $Q_{avg} = WQ_v/144,000$	Q_{avg} (cfs) = <u>0.019</u>
Step 11) Determine orifice area $A_o = Q_{avg}/(0.6 \cdot (2 \cdot g \cdot h_o)^{0.5})$	A_o (ft ²) = <u>0.0025</u> A_o (in ²) = <u>0.36</u>

V. Overflow

The bioretention overflow shall be designed to safely pass runoff flows from events up to and including the 1 percent event unless the facility is designed with a bypass around the facility for larger storm events. If the 1-percent event is to pass through the facility, the maximum velocity shall be kept below 3 feet per second to avoid erosion of the soil matrix. If facilities are designed with a bypass, it shall be designed to safely pass runoff flows from events up to and including the 1 percent event. The overflow shall be designed as a vegetated or stabilized channel of a yard inlet catch basin. Vegetated or stabilized channels shall be designed using one of the methods presented in APWA Section 5603 and shall conform to the design criteria presented in APWA Section 5607. Methods presented in APWA Section 5604 shall be used for inlet design.

Exhibit 2
1-Year Storm Calculations



Subcat



Reach



Pond



Link

Routing Diagram for 400 NW 72 Street

Prepared by HP, Printed 7/21/2023

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Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
2.354	74	>75% Grass cover, Good, HSG C (1E, 1P, 2E, 2P, 3E, 3P, 4P, 5P, 6P)
0.874	98	Paved parking, HSG C (1P)
3.228	80	TOTAL AREA

Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
3.228	HSG C	1E, 1P, 2E, 2P, 3E, 3P, 4P, 5P, 6P
0.000	HSG D	
0.000	Other	
3.228		TOTAL AREA

400 NW 72 Street

Prepared by HP

Printed 7/21/2023

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Page 4

Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	2.354	0.000	0.000	2.354	>75% Grass cover, Good	1E, 1P, 2E, 2P, 3E, 3P, 4P, 5P, 6P
0.000	0.000	0.874	0.000	0.000	0.874	Paved parking	1P
0.000	0.000	3.228	0.000	0.000	3.228	TOTAL AREA	

Time span=2.00-30.00 hrs, dt=0.05 hrs, 561 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1E: (new Subcat)	Runoff Area=0.544 ac 0.00% Impervious Runoff Depth=0.85"
	Flow Length=81' Slope=0.0247 '/' Tc=10.6 min CN=74 Runoff=0.66 cfs 0.038 af
Subcatchment 1P: (new Subcat)	Runoff Area=1.145 ac 76.33% Impervious Runoff Depth=2.07"
	Flow Length=249' Tc=2.8 min CN=92 Runoff=4.33 cfs 0.197 af
Subcatchment 2E: (new Subcat)	Runoff Area=0.017 ac 0.00% Impervious Runoff Depth=0.85"
	Flow Length=30' Slope=0.0732 '/' Tc=3.1 min CN=74 Runoff=0.03 cfs 0.001 af
Subcatchment 2P: (new Subcat)	Runoff Area=0.007 ac 0.00% Impervious Runoff Depth=0.85"
	Flow Length=33' Slope=0.0758 '/' Tc=3.3 min CN=74 Runoff=0.01 cfs 0.000 af
Subcatchment 3E: (new Subcat)	Runoff Area=1.053 ac 0.00% Impervious Runoff Depth=0.85"
	Flow Length=237' Tc=5.8 min CN=74 Runoff=1.53 cfs 0.074 af
Subcatchment 3P: (new Subcat)	Runoff Area=0.007 ac 0.00% Impervious Runoff Depth=0.85"
	Flow Length=43' Slope=0.5116 '/' Tc=1.9 min CN=74 Runoff=0.01 cfs 0.000 af
Subcatchment 4P: (new Subcat)	Runoff Area=0.167 ac 0.00% Impervious Runoff Depth=0.85"
	Flow Length=83' Tc=2.6 min CN=74 Runoff=0.27 cfs 0.012 af
Subcatchment 5P: (new Subcat)	Runoff Area=0.142 ac 0.00% Impervious Runoff Depth=0.85"
	Flow Length=13' Slope=0.0176 '/' Tc=2.8 min CN=74 Runoff=0.23 cfs 0.010 af
Subcatchment 6P: (new Subcat)	Runoff Area=0.146 ac 0.00% Impervious Runoff Depth=0.85"
	Flow Length=222' Tc=7.5 min CN=74 Runoff=0.20 cfs 0.010 af
Pond DET1: (new Pond)	Peak Elev=983.05' Storage=0.064 af Inflow=4.56 cfs 0.207 af
	Outflow=1.70 cfs 0.207 af
Link 4E: (new Link)	Inflow=2.13 cfs 0.114 af
	Primary=2.13 cfs 0.114 af
Link 10L: (new Link)	Inflow=2.06 cfs 0.230 af
	Primary=2.06 cfs 0.230 af
Total Runoff Area = 3.228 ac Runoff Volume = 0.344 af Average Runoff Depth = 1.28"	
72.92% Pervious = 2.354 ac 27.08% Impervious = 0.874 ac	

Summary for Subcatchment 1E: (new Subcat)

Runoff = 0.66 cfs @ 12.04 hrs, Volume= 0.038 af, Depth= 0.85"

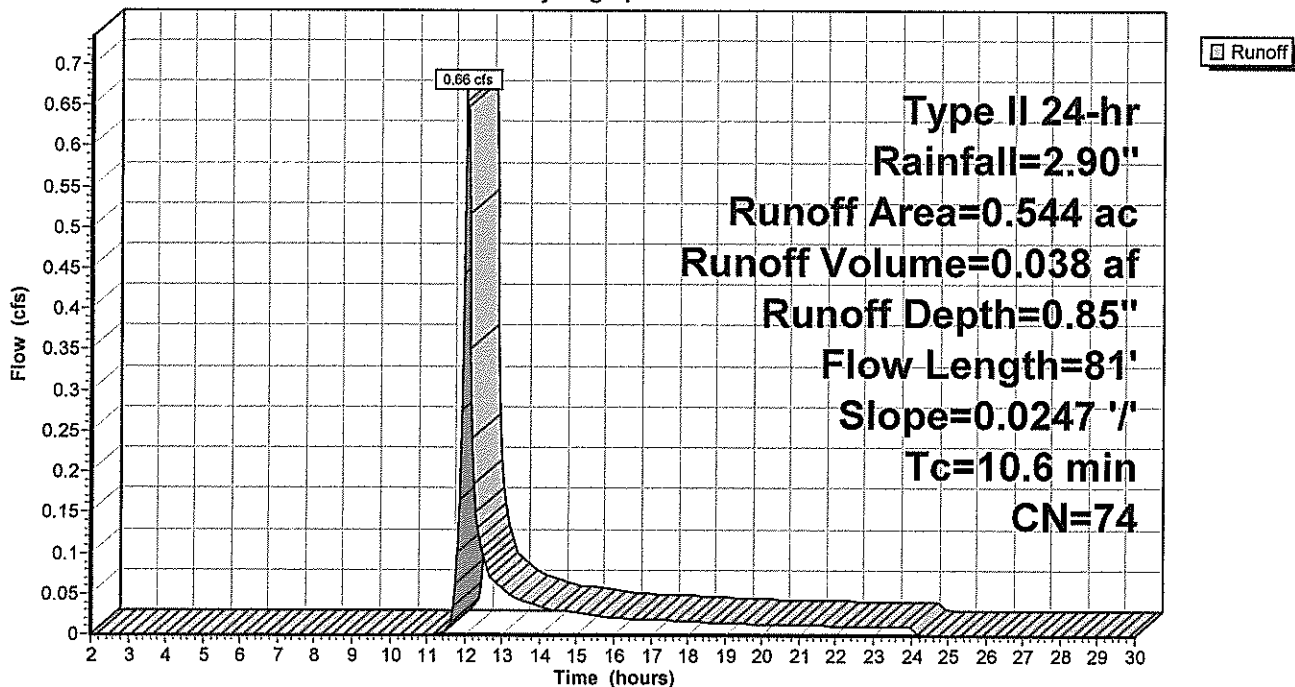
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs
Type II 24-hr Rainfall=2.90"

Area (ac)	CN	Description
0.544	74	>75% Grass cover, Good, HSG C
0.544		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.6	81	0.0247	0.13		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 1E: (new Subcat)

Hydrograph



Summary for Subcatchment 1P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 4.33 cfs @ 11.93 hrs, Volume= 0.197 af, Depth= 2.07"

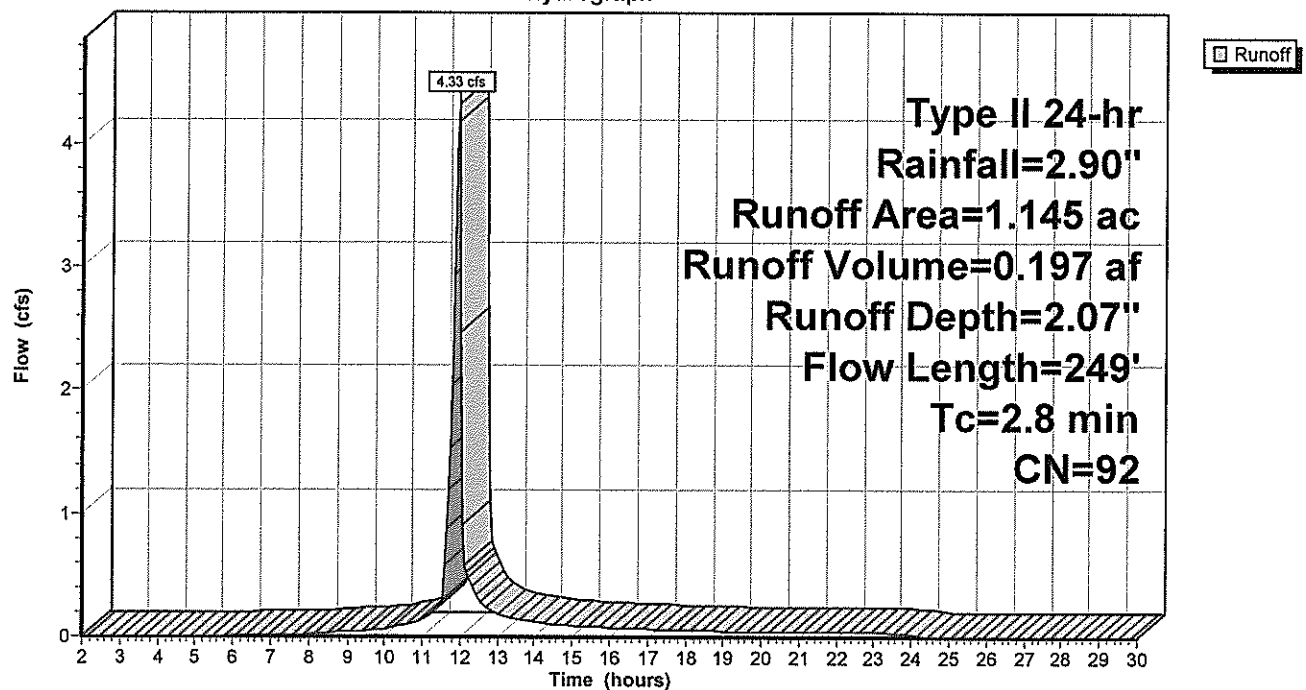
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=2.90"

Area (ac)	CN	Description
0.271	74	>75% Grass cover, Good, HSG C
0.874	98	Paved parking, HSG C
1.145	92	Weighted Average
0.271		23.67% Pervious Area
0.874		76.33% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0065	0.92		Sheet Flow, Smooth surfaces n= 0.011 P2= 3.50"
1.0	149	0.0151	2.49		Shallow Concentrated Flow, Paved Kv= 20.3 fps
2.8	249	Total			

Subcatchment 1P: (new Subcat)

Hydrograph



Summary for Subcatchment 2E: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.03 cfs @ 11.94 hrs, Volume= 0.001 af, Depth= 0.85"

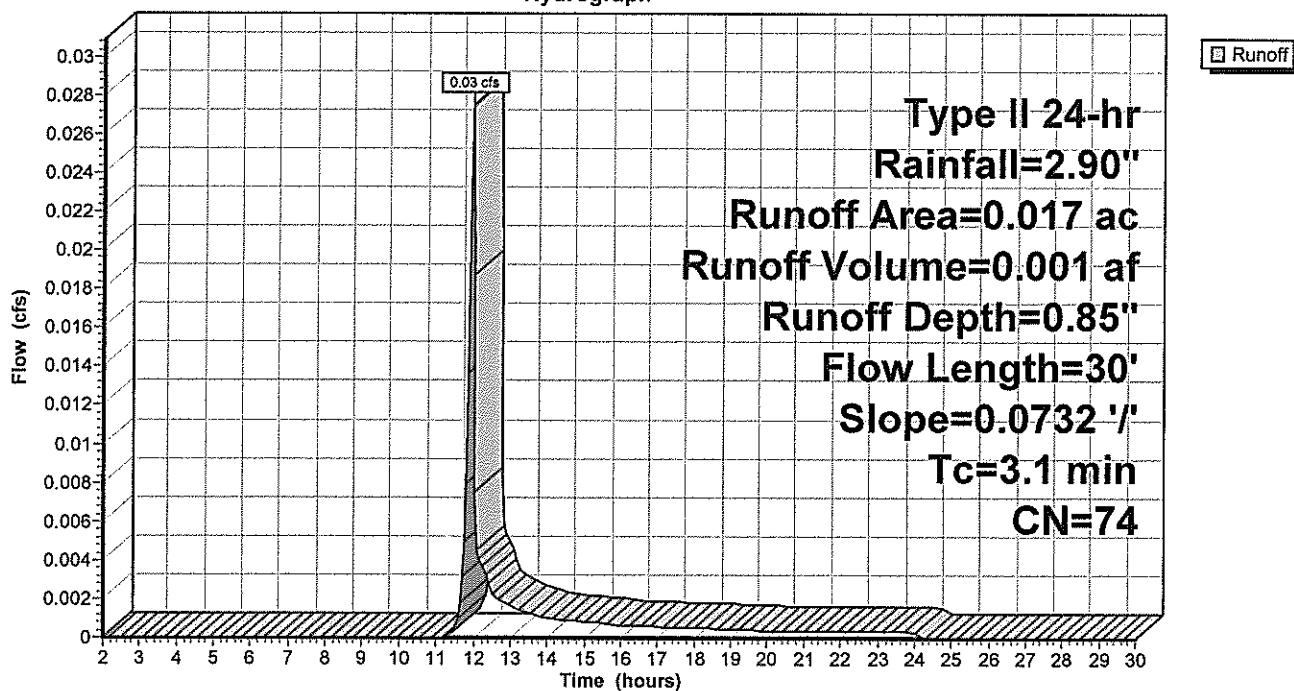
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=2.90"

Area (ac)	CN	Description
0.017	74	>75% Grass cover, Good, HSG C
0.017		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	30	0.0732	0.16		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$

Subcatchment 2E: (new Subcat)

Hydrograph



Summary for Subcatchment 2P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.01 cfs @ 11.95 hrs, Volume= 0.000 af, Depth= 0.85"

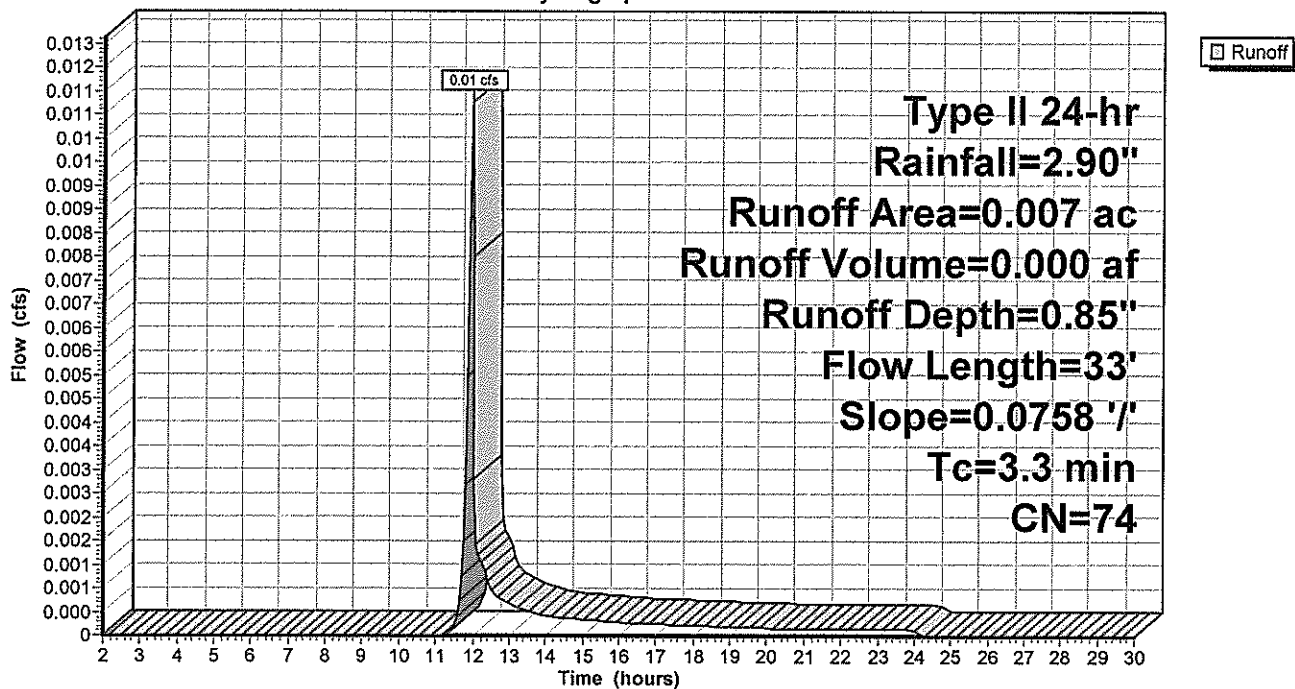
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=2.90"

Area (ac)	CN	Description
0.007	74	>75% Grass cover, Good, HSG C
0.007		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	33	0.0758	0.17		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 2P: (new Subcat)

Hydrograph



Summary for Subcatchment 3E: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 1.53 cfs @ 11.98 hrs, Volume= 0.074 af, Depth= 0.85"

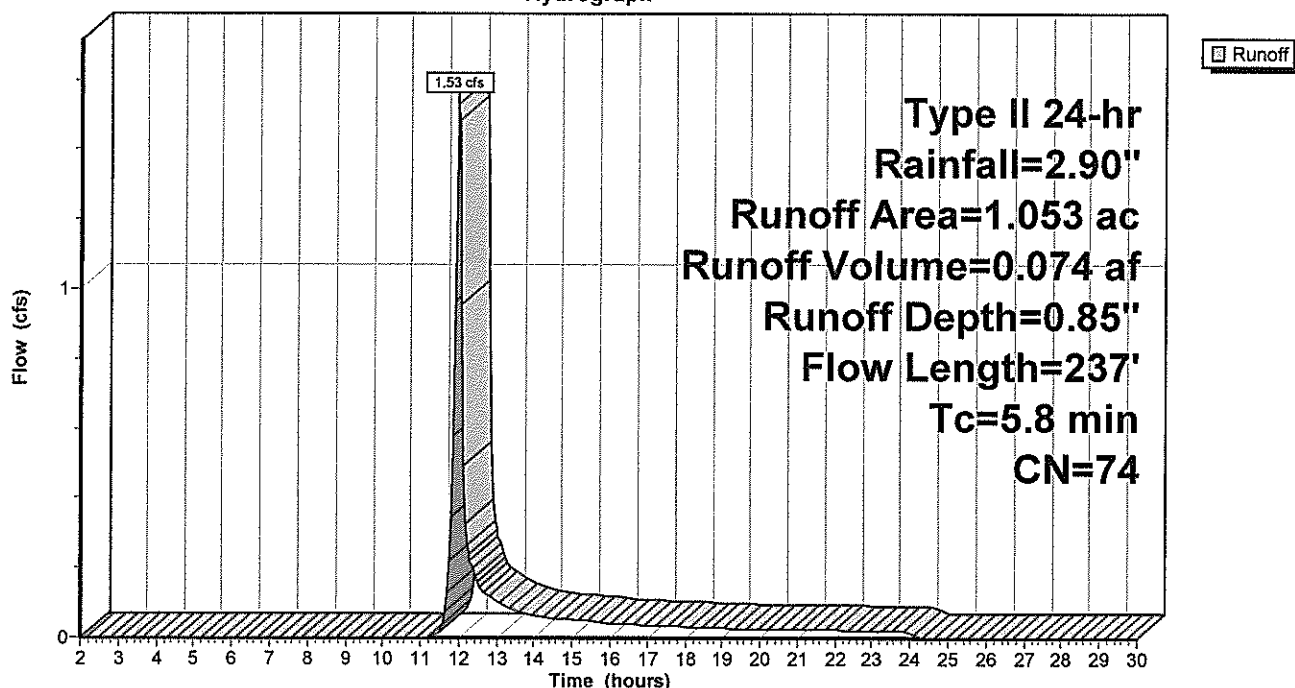
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=2.90"

Area (ac)	CN	Description
1.053	74	>75% Grass cover, Good, HSG C
1.053		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.4	100	0.2000	0.31		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$
0.4	137	0.1339	5.49		Shallow Concentrated Flow, Grassed Waterway $K_v=15.0$ fps
5.8	237	Total			

Subcatchment 3E: (new Subcat)

Hydrograph



Summary for Subcatchment 3P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.01 cfs @ 11.93 hrs, Volume= 0.000 af, Depth= 0.85"

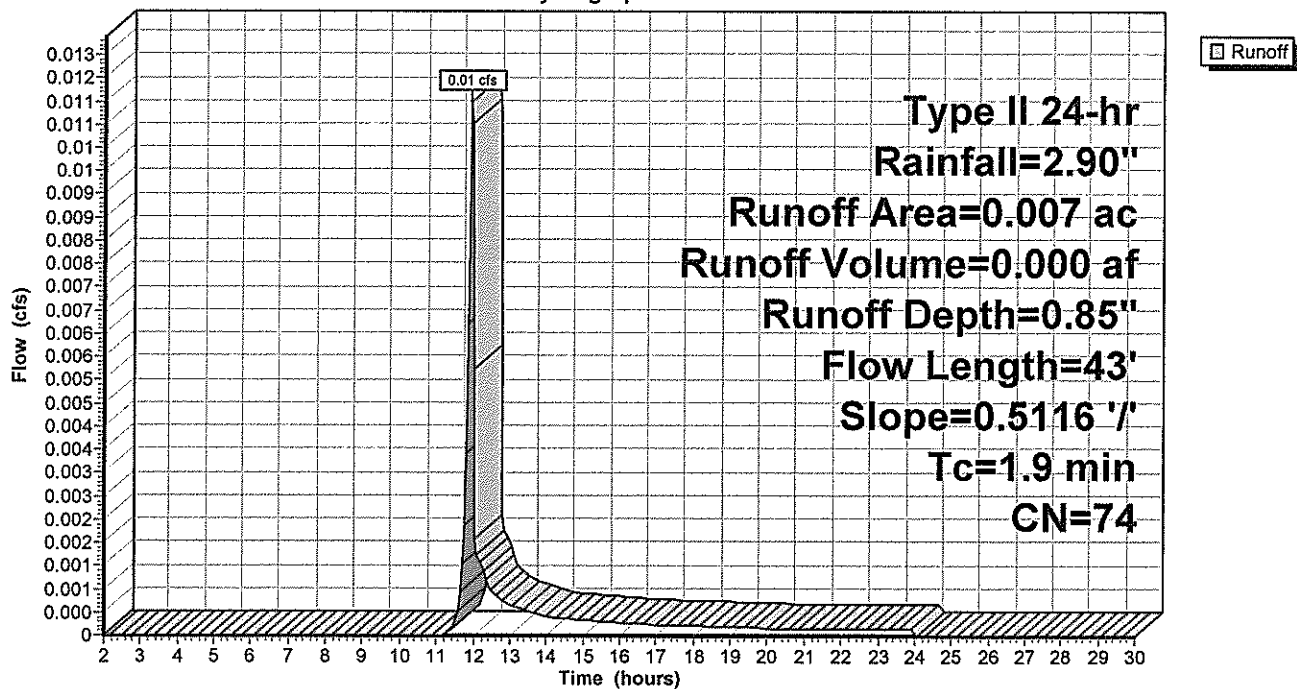
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=2.90"

Area (ac)	CN	Description
0.007	74	>75% Grass cover, Good, HSG C
0.007		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	43	0.5116	0.38		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 3P: (new Subcat)

Hydrograph



Summary for Subcatchment 4P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.27 cfs @ 11.94 hrs, Volume= 0.012 af, Depth= 0.85"

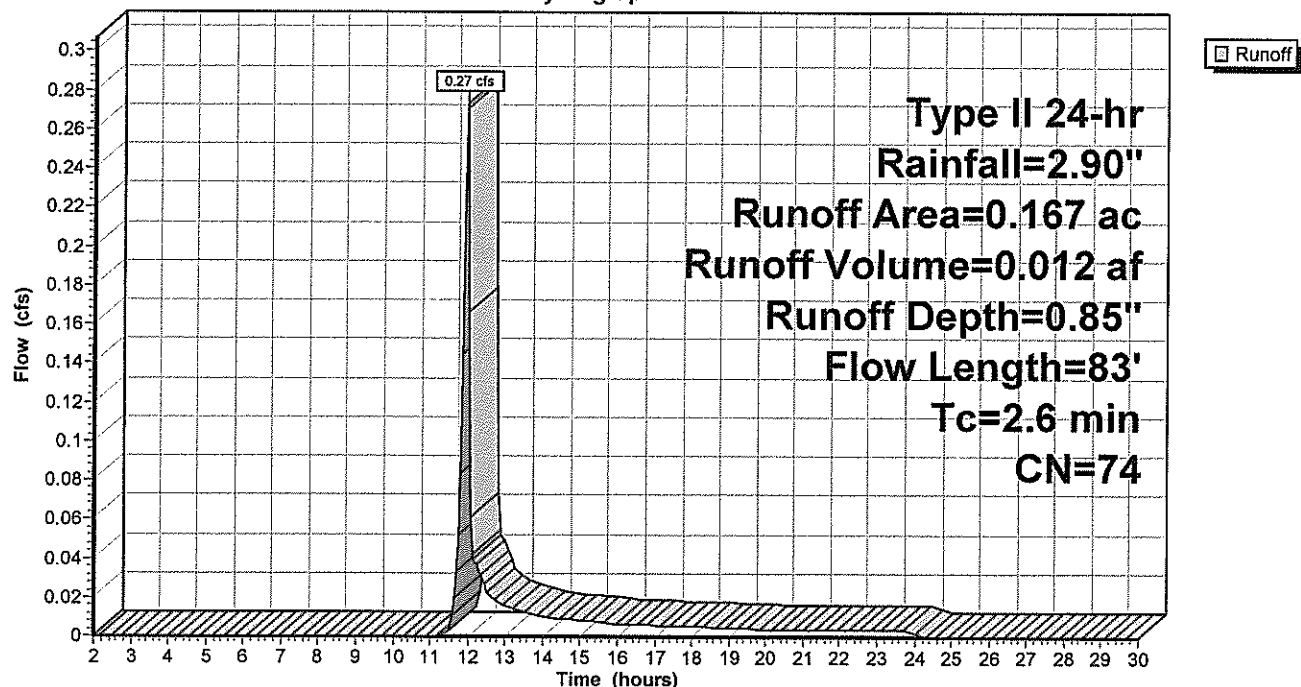
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=2.90"

Area (ac)	CN	Description
0.167	74	>75% Grass cover, Good, HSG C
0.167		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	30	0.1453	0.21		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$
0.2	53	0.0967	5.01		Shallow Concentrated Flow, Unpaved $K_v=16.1$ fps
2.6	83	Total			

Subcatchment 4P: (new Subcat)

Hydrograph



Summary for Subcatchment 5P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.23 cfs @ 11.94 hrs, Volume= 0.010 af, Depth= 0.85"

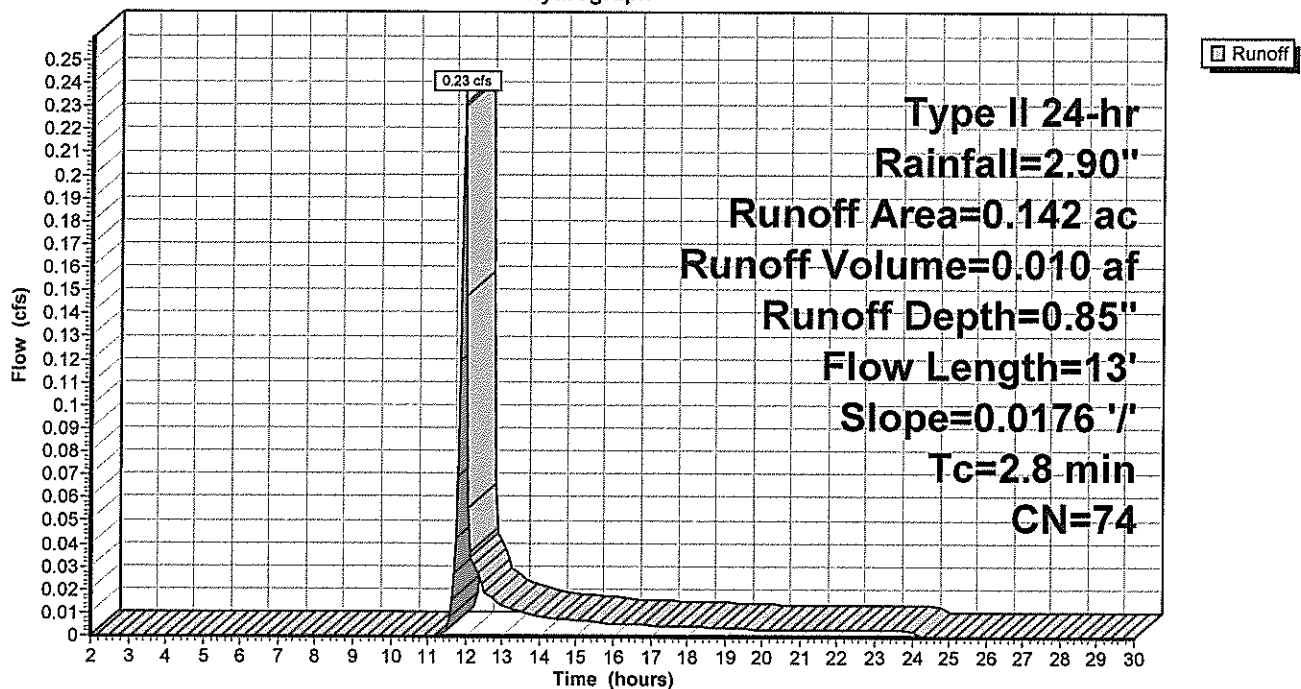
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=2.90"

Area (ac)	CN	Description
0.142	74	>75% Grass cover, Good, HSG C
0.142		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.8	13	0.0176	0.08		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 5P: (new Subcat)

Hydrograph



Summary for Subcatchment 6P: (new Subcat)

Runoff = 0.20 cfs @ 12.00 hrs, Volume= 0.010 af, Depth= 0.85"

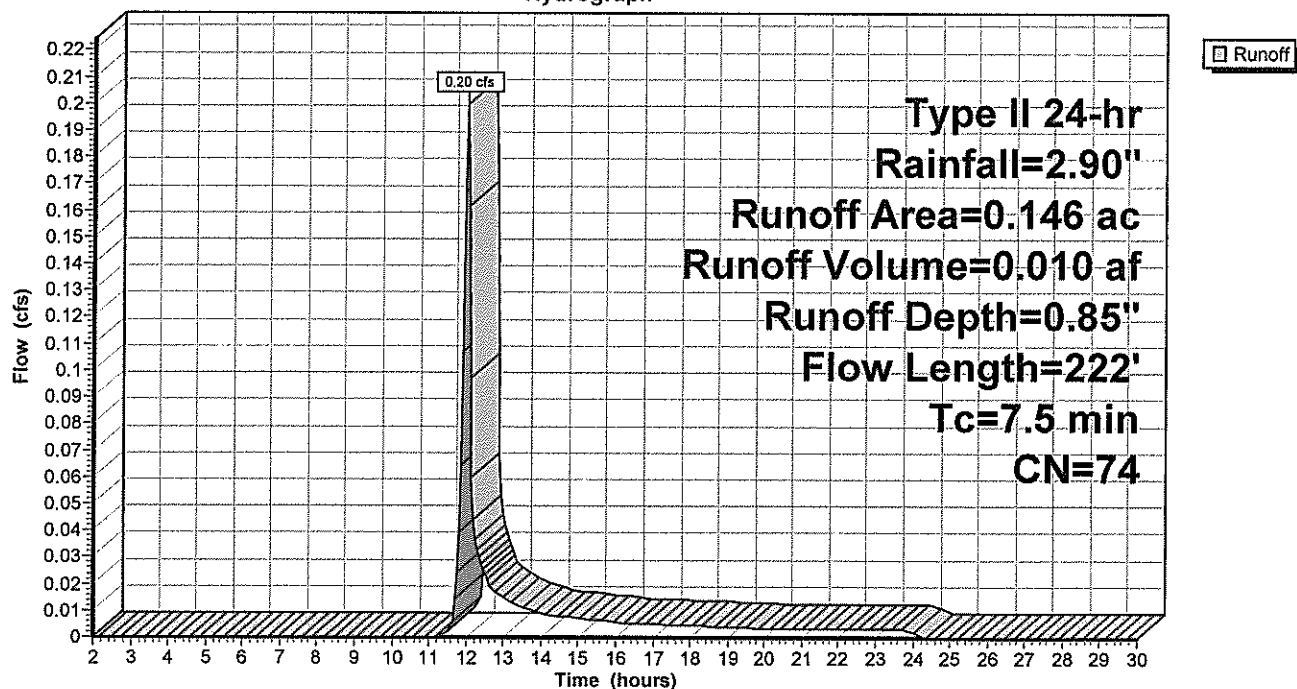
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs
Type II 24-hr Rainfall=2.90"

Area (ac)	CN	Description
0.146	74	>75% Grass cover, Good, HSG C
0.146		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.9	60	0.0400	0.15		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"
0.6	162	0.0775	4.18		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
7.5	222	Total			

Subcatchment 6P: (new Subcat)

Hydrograph



Summary for Pond DET1: (new Pond)

Inflow Area = 1.287 ac, 67.91% Impervious, Inflow Depth = 1.93"
 Inflow = 4.56 cfs @ 11.93 hrs, Volume= 0.207 af
 Outflow = 1.70 cfs @ 12.03 hrs, Volume= 0.207 af, Atten= 63%, Lag= 6.0 min
 Primary = 1.70 cfs @ 12.03 hrs, Volume= 0.207 af

Routing by Stor-Ind method, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs
 Peak Elev= 983.05' @ 12.03 hrs Surf.Area= 0.085 ac Storage= 0.064 af

Plug-Flow detention time= 29.3 min calculated for 0.207 af (100% of inflow)
 Center-of-Mass det. time= 29.1 min (827.6 - 798.5)

Volume	Invert	Avail.Storage	Storage Description
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#1	982.03'	0.211 af	36.0" Round Pipe Storage L= 1,300.0'
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Device	Routing	Invert	Outlet Devices
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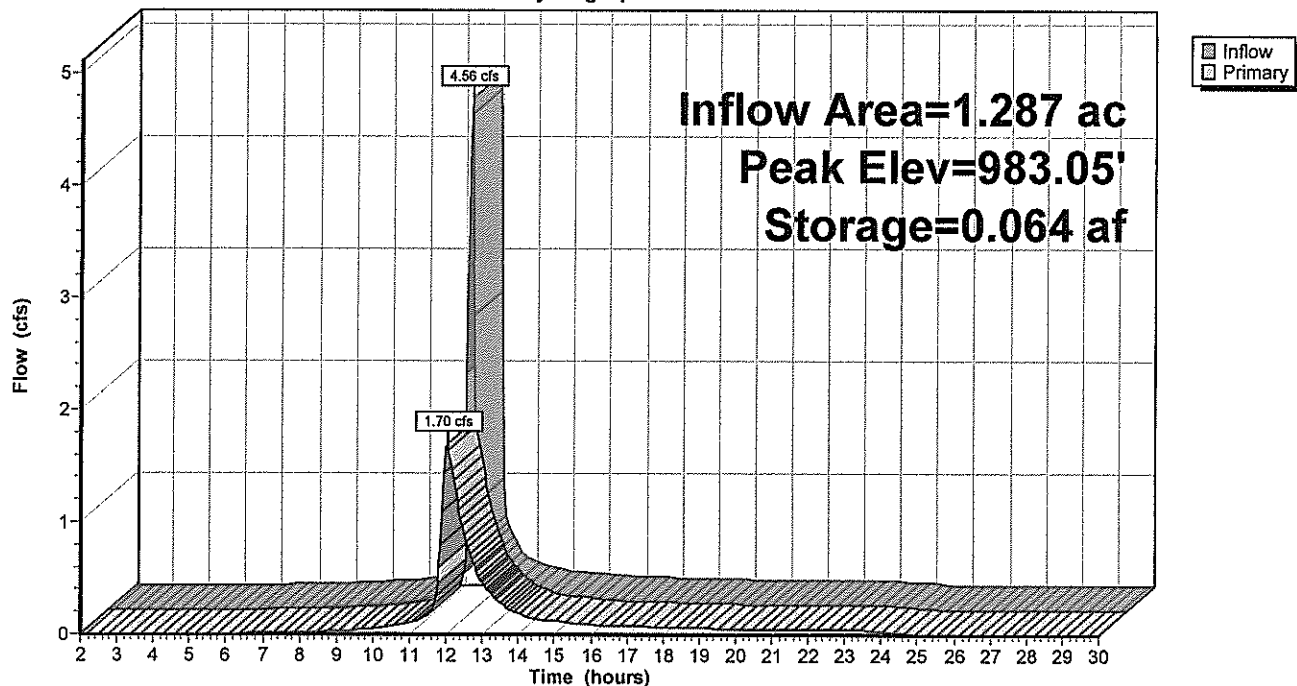
#1	Primary	982.03'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28) Head (feet) 0.00 1.03 1.03 1.93 1.93 3.00 Width (feet) 0.50 0.50 0.79 0.79 2.50 2.50
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Primary OutFlow Max=1.68 cfs @ 12.03 hrs HW=983.05' (Free Discharge)

↑1=Custom Weir/Orifice (Weir Controls 1.68 cfs @ 3.31 fps)

Pond DET1: (new Pond)

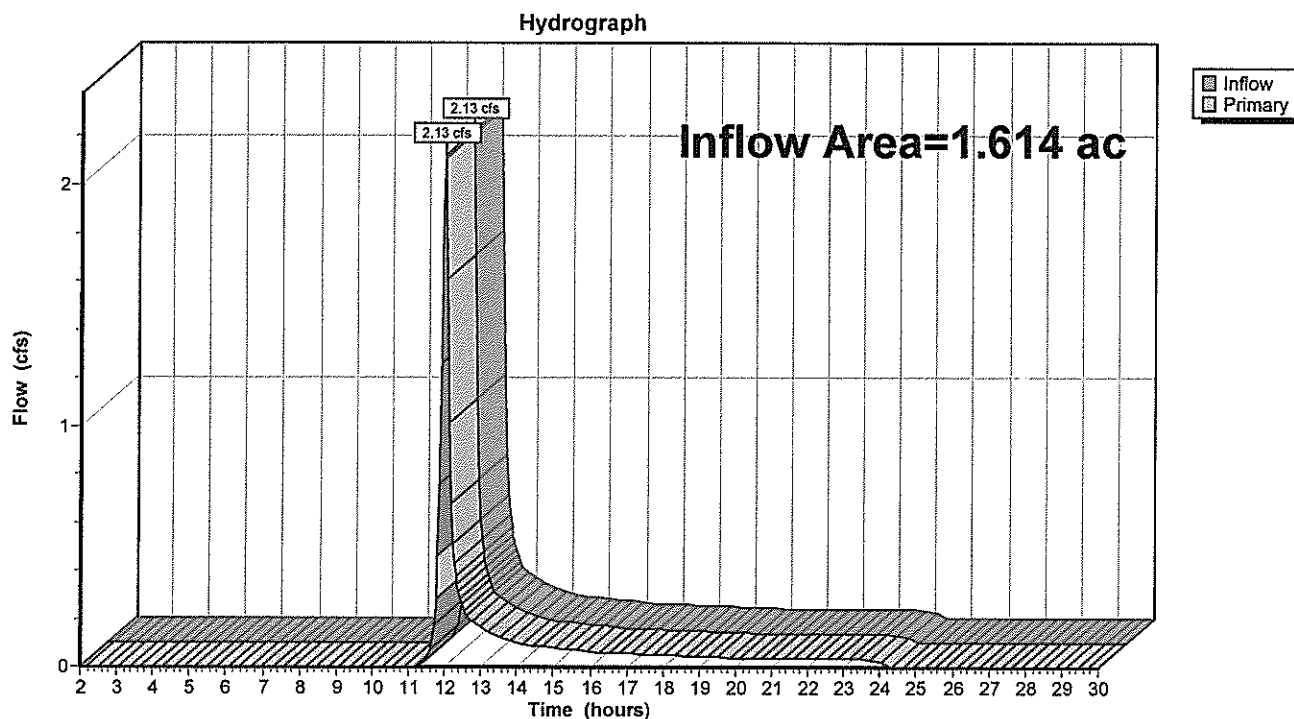
Hydrograph



Summary for Link 4E: (new Link)

Inflow Area = 1.614 ac, 0.00% Impervious, Inflow Depth = 0.85"
Inflow = 2.13 cfs @ 11.99 hrs, Volume= 0.114 af
Primary = 2.13 cfs @ 11.99 hrs, Volume= 0.114 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs

Link 4E: (new Link)

Summary for Link 10L: (new Link)

Inflow Area = 1.614 ac, 54.15% Impervious, Inflow Depth = 1.71"
Inflow = 2.06 cfs @ 12.00 hrs, Volume= 0.230 af
Primary = 2.06 cfs @ 12.00 hrs, Volume= 0.230 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs

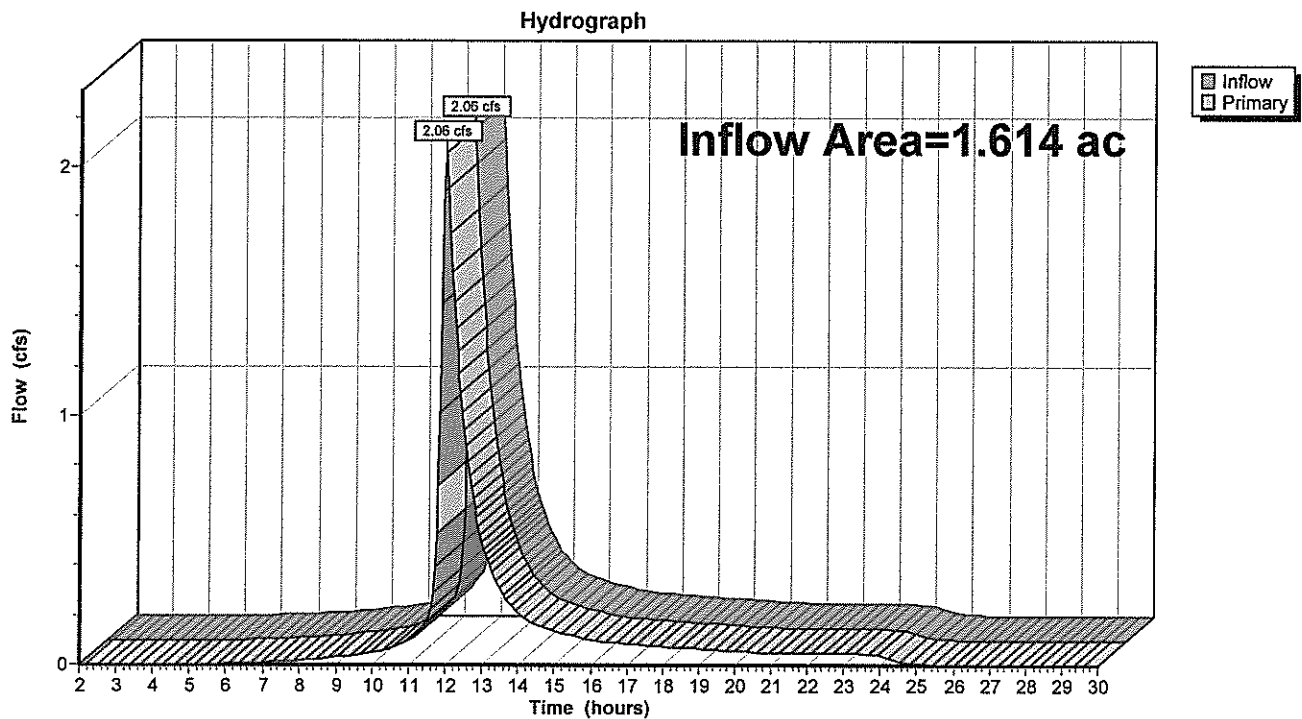
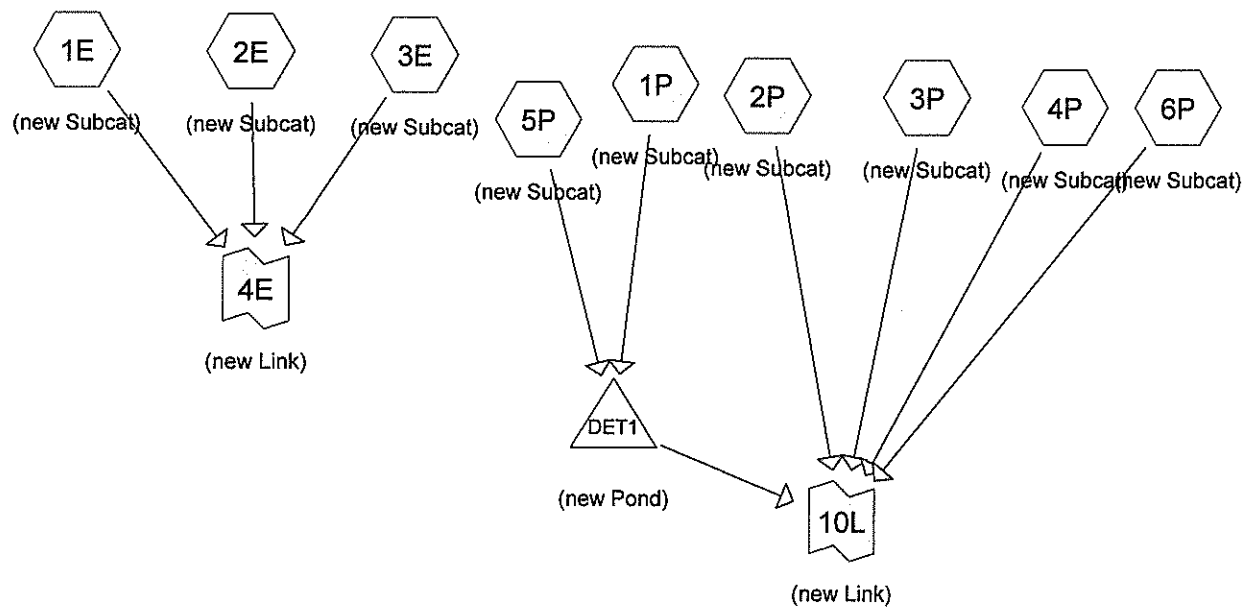
Link 10L: (new Link)

Exhibit 3
10-year Storm Calculations



Subcat



Reach



Pond



Link

Routing Diagram for 400 NW 72 Street

Prepared by HP, Printed 7/20/2023

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400 NW 72 Street

Prepared by HP

Printed 7/20/2023

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Page 2

Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
2.354	74	>75% Grass cover, Good, HSG C (1E, 1P, 2E, 2P, 3E, 3P, 4P, 5P, 6P)
0.874	98	Paved parking, HSG C (1P)
3.228	80	TOTAL AREA

Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
3.228	HSG C	1E, 1P, 2E, 2P, 3E, 3P, 4P, 5P, 6P
0.000	HSG D	
0.000	Other	
3.228		TOTAL AREA

400 NW 72 Street

Prepared by HP

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Page 4

Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	2.354	0.000	0.000	2.354	>75% Grass cover, Good	1E, 1P, 2E, 2P, 3E, 3P, 4P, 5P, 6P
0.000	0.000	0.874	0.000	0.000	0.874	Paved parking	1P
0.000	0.000	3.228	0.000	0.000	3.228	TOTAL AREA	

Time span=2.00-30.00 hrs, dt=0.05 hrs, 561 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1E: (new Subcat) Runoff Area=0.544 ac 0.00% Impervious Runoff Depth=2.52"
 Flow Length=81' Slope=0.0247 '/ Tc=10.6 min CN=74 Runoff=2.04 cfs 0.114 af

Subcatchment 1P: (new Subcat) Runoff Area=1.145 ac 76.33% Impervious Runoff Depth=4.28"
 Flow Length=249' Tc=2.8 min CN=92 Runoff=8.53 cfs 0.409 af

Subcatchment 2E: (new Subcat) Runoff Area=0.017 ac 0.00% Impervious Runoff Depth=2.52"
 Flow Length=30' Slope=0.0732 '/ Tc=3.1 min CN=74 Runoff=0.08 cfs 0.004 af

Subcatchment 2P: (new Subcat) Runoff Area=0.007 ac 0.00% Impervious Runoff Depth=2.52"
 Flow Length=33' Slope=0.0758 '/ Tc=3.3 min CN=74 Runoff=0.03 cfs 0.001 af

Subcatchment 3E: (new Subcat) Runoff Area=1.053 ac 0.00% Impervious Runoff Depth=2.52"
 Flow Length=237' Tc=5.8 min CN=74 Runoff=4.62 cfs 0.222 af

Subcatchment 3P: (new Subcat) Runoff Area=0.007 ac 0.00% Impervious Runoff Depth=2.52"
 Flow Length=43' Slope=0.5116 '/ Tc=1.9 min CN=74 Runoff=0.03 cfs 0.001 af

Subcatchment 4P: (new Subcat) Runoff Area=0.167 ac 0.00% Impervious Runoff Depth=2.52"
 Flow Length=83' Tc=2.6 min CN=74 Runoff=0.82 cfs 0.035 af

Subcatchment 5P: (new Subcat) Runoff Area=0.142 ac 0.00% Impervious Runoff Depth=2.52"
 Flow Length=13' Slope=0.0176 '/ Tc=2.8 min CN=74 Runoff=0.70 cfs 0.030 af

Subcatchment 6P: (new Subcat) Runoff Area=0.146 ac 0.00% Impervious Runoff Depth=2.52"
 Flow Length=222' Tc=7.5 min CN=74 Runoff=0.61 cfs 0.031 af

Pond DET1: (new Pond) Peak Elev=983.76' Storage=0.126 af Inflow=9.22 cfs 0.439 af
 Outflow=4.30 cfs 0.439 af

Link 4E: (new Link) Inflow=6.54 cfs 0.340 af
 Primary=6.54 cfs 0.340 af

Link 10L: (new Link) Inflow=5.38 cfs 0.508 af
 Primary=5.38 cfs 0.508 af

Total Runoff Area = 3.228 ac Runoff Volume = 0.847 af Average Runoff Depth = 3.15"
72.92% Pervious = 2.354 ac 27.08% Impervious = 0.874 ac

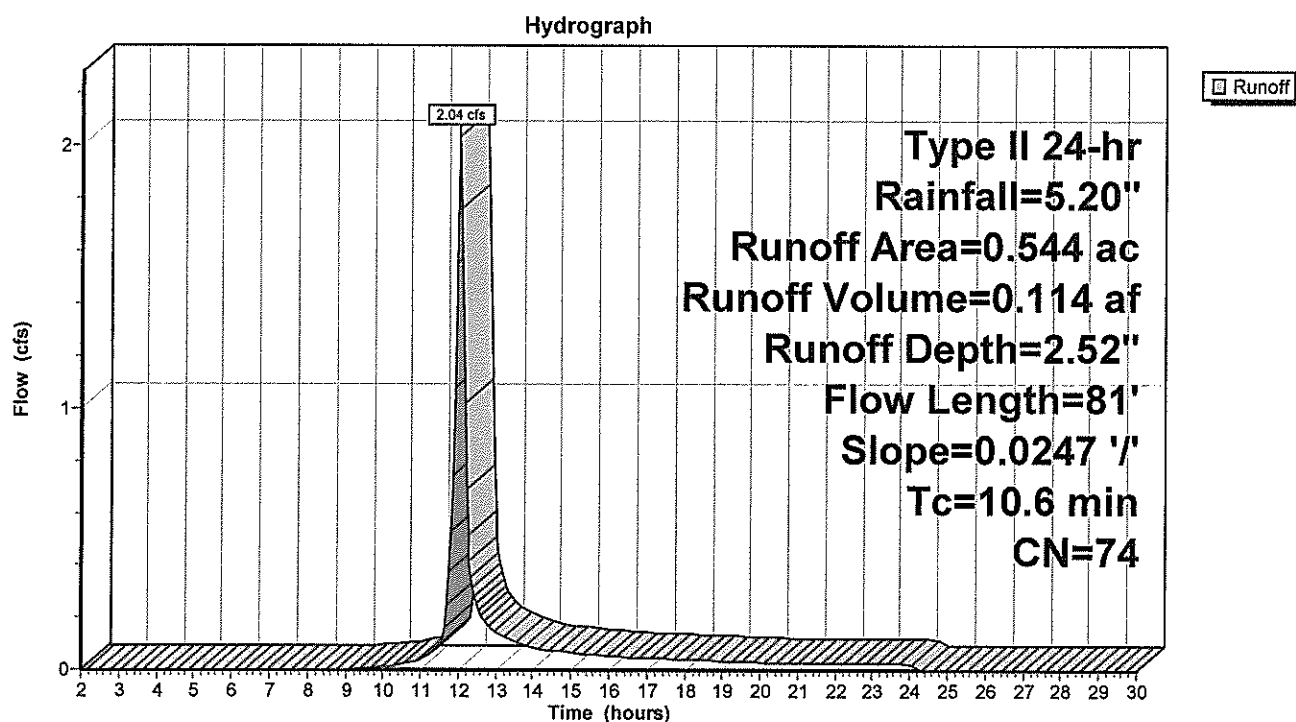
Summary for Subcatchment 1E: (new Subcat)

Runoff = 2.04 cfs @ 12.03 hrs, Volume= 0.114 af, Depth= 2.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs
Type II 24-hr Rainfall=5.20"

Area (ac)	CN	Description
0.544	74	>75% Grass cover, Good, HSG C
0.544		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.6	81	0.0247	0.13		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 1E: (new Subcat)

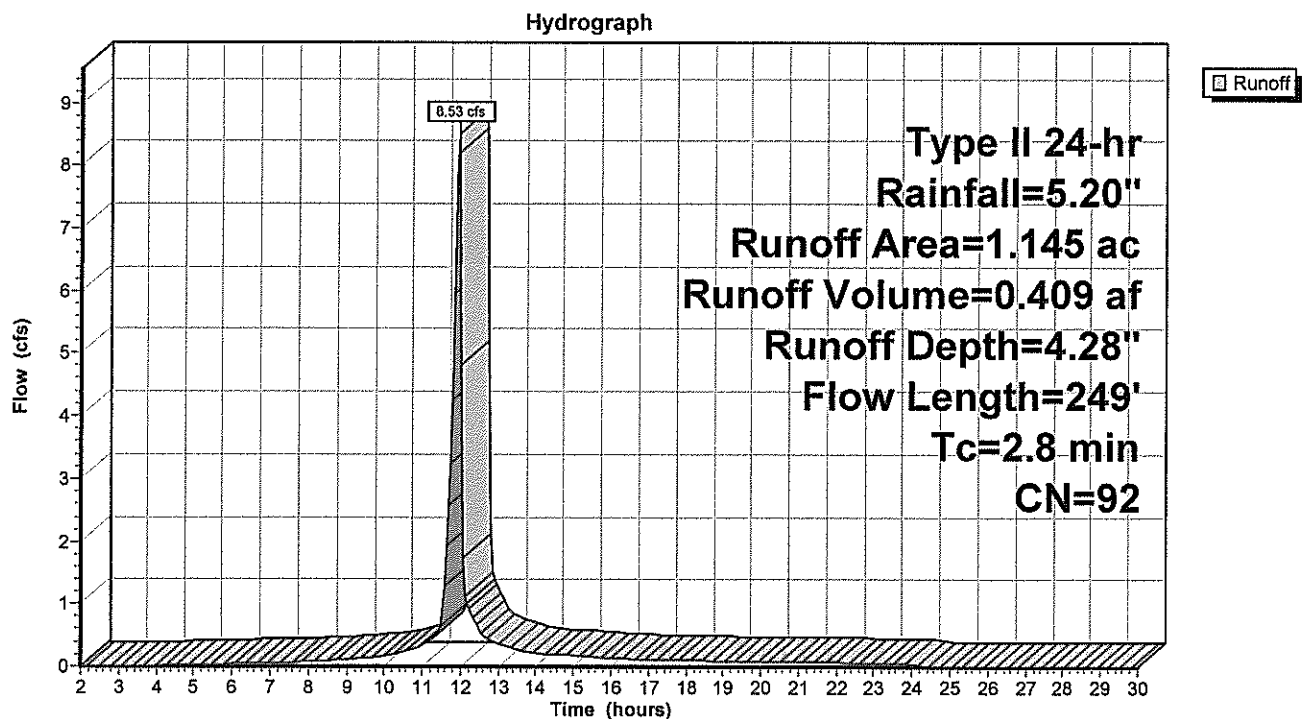
Summary for Subcatchment 1P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 8.53 cfs @ 11.93 hrs, Volume= 0.409 af, Depth= 4.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=5.20"

Area (ac)	CN	Description
0.271	74	>75% Grass cover, Good, HSG C
0.874	98	Paved parking, HSG C
1.145	92	Weighted Average
0.271		23.67% Pervious Area
0.874		76.33% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0065	0.92		Sheet Flow, Smooth surfaces $n=0.011$ $P2=3.50"$
1.0	149	0.0151	2.49		Shallow Concentrated Flow, Paved $K_v=20.3$ fps
2.8	249	Total			

Subcatchment 1P: (new Subcat)

Summary for Subcatchment 2E: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.08 cfs @ 11.94 hrs, Volume= 0.004 af, Depth= 2.52"

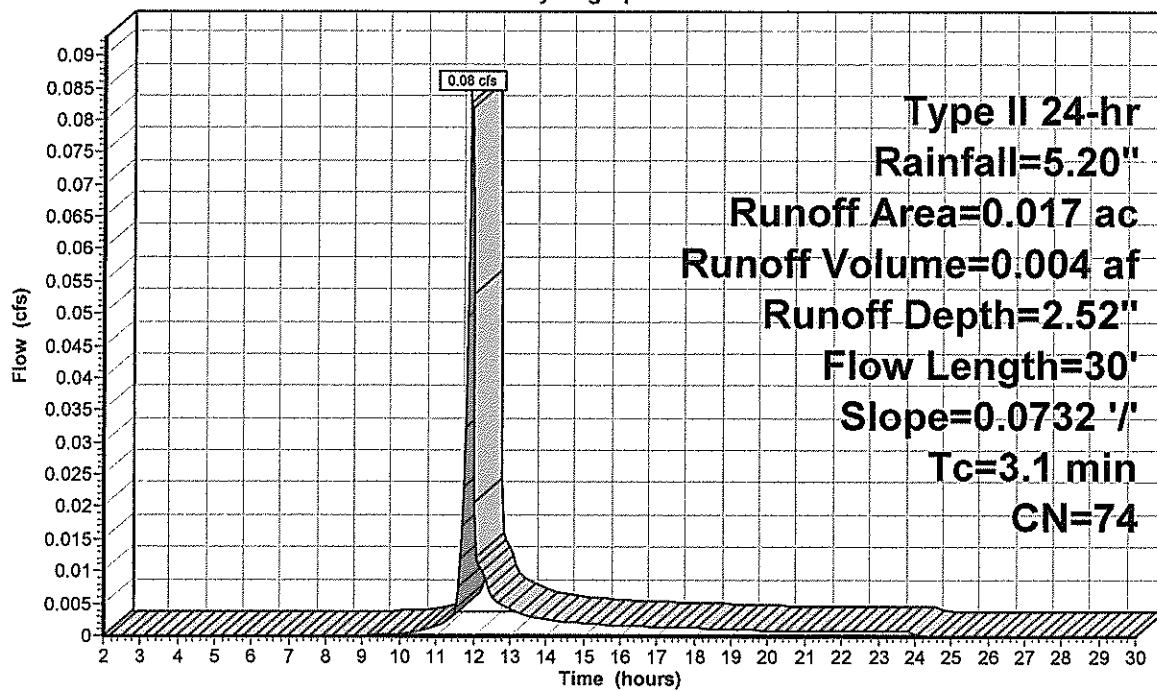
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=5.20"

Area (ac)	CN	Description
0.017	74	>75% Grass cover, Good, HSG C
0.017		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	30	0.0732	0.16		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 2E: (new Subcat)

Hydrograph



Runoff

Summary for Subcatchment 2P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.03 cfs @ 11.94 hrs, Volume= 0.001 af, Depth= 2.52"

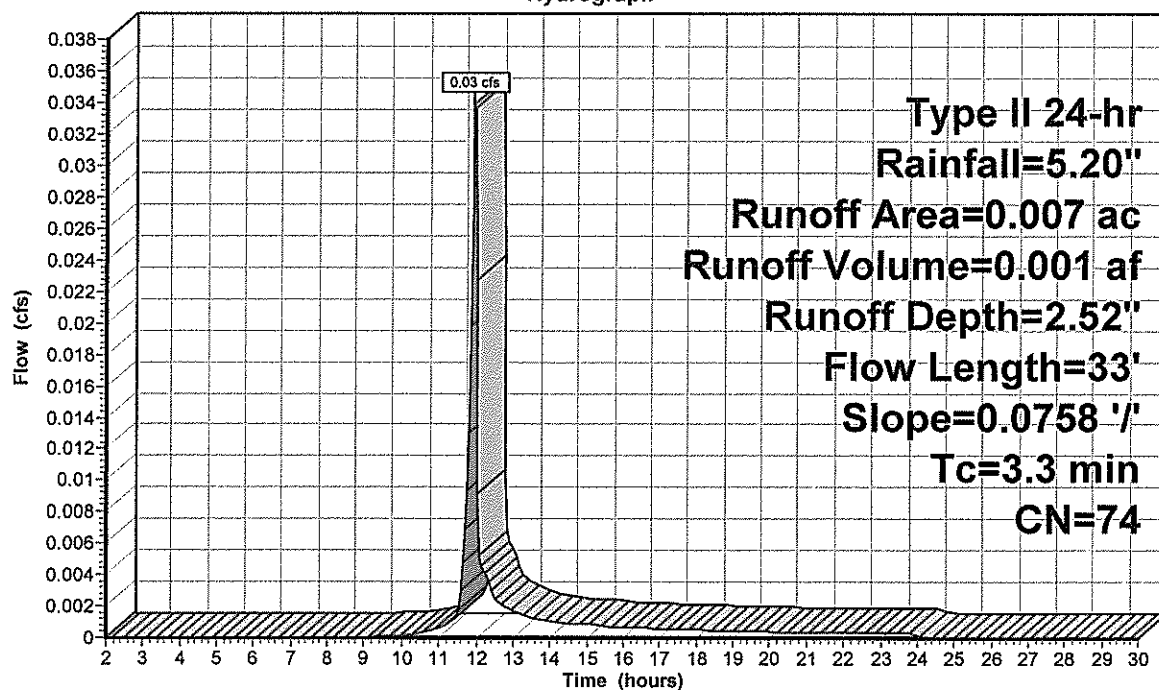
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=5.20"

Area (ac)	CN	Description
0.007	74	>75% Grass cover, Good, HSG C
0.007		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	33	0.0758	0.17		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$

Subcatchment 2P: (new Subcat)

Hydrograph



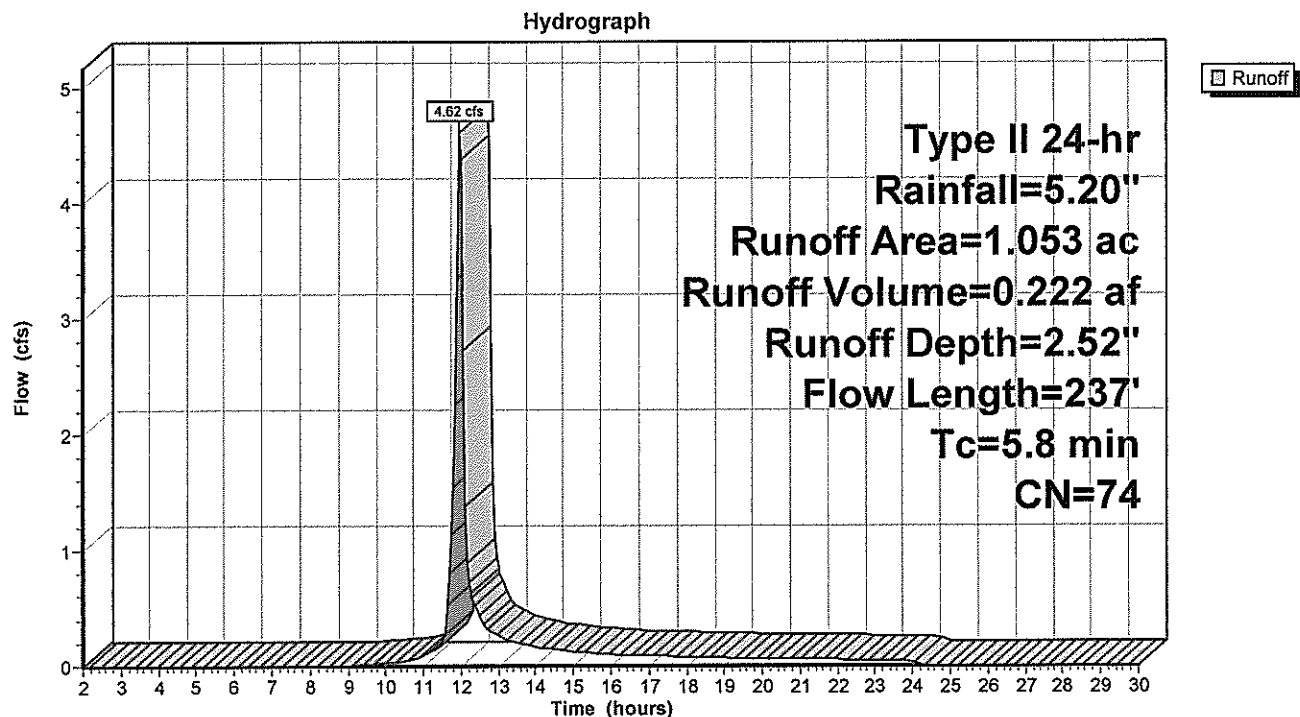
Summary for Subcatchment 3E: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 4.62 cfs @ 11.97 hrs, Volume= 0.222 af, Depth= 2.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=5.20"

Area (ac)	CN	Description
1.053	74	>75% Grass cover, Good, HSG C
1.053		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.4	100	0.2000	0.31		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$
0.4	137	0.1339	5.49		Shallow Concentrated Flow, Grassed Waterway $K_v=15.0$ fps
5.8	237	Total			

Subcatchment 3E: (new Subcat)

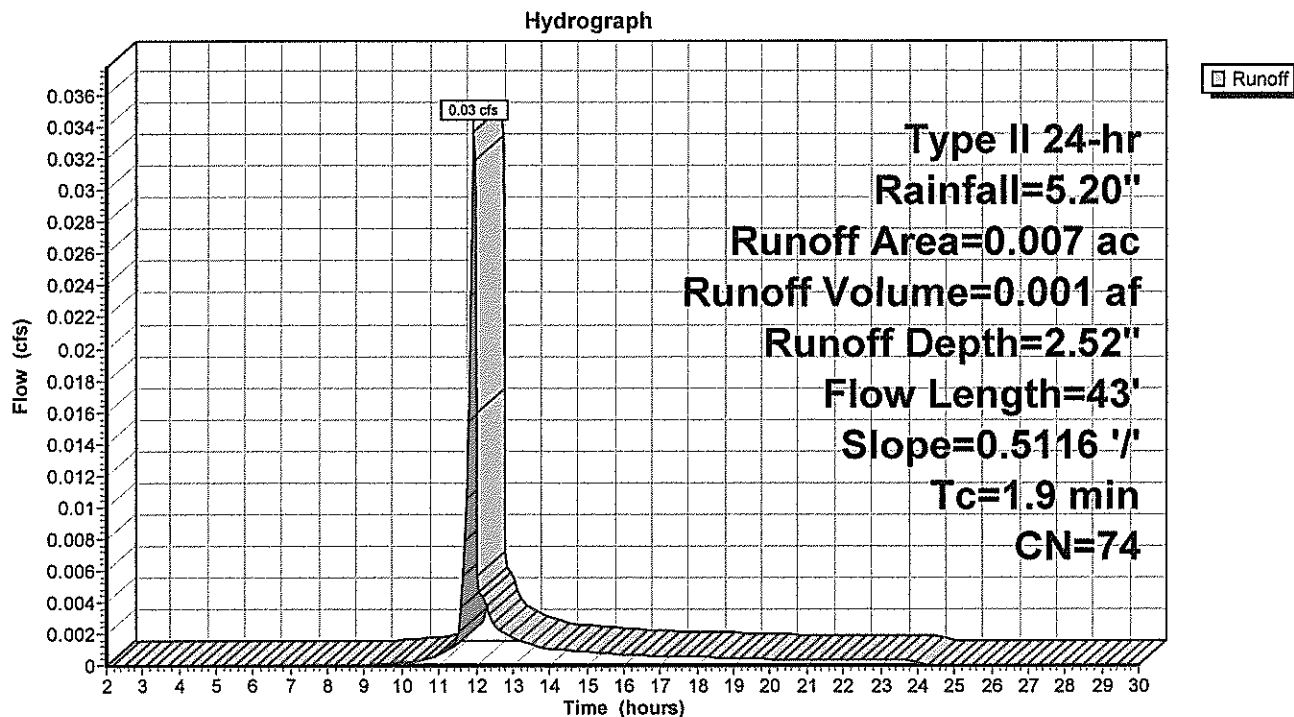
Summary for Subcatchment 3P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.03 cfs @ 11.92 hrs, Volume= 0.001 af, Depth= 2.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=5.20"

Area (ac)	CN	Description
0.007	74	>75% Grass cover, Good, HSG C
0.007		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	43	0.5116	0.38		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$

Subcatchment 3P: (new Subcat)

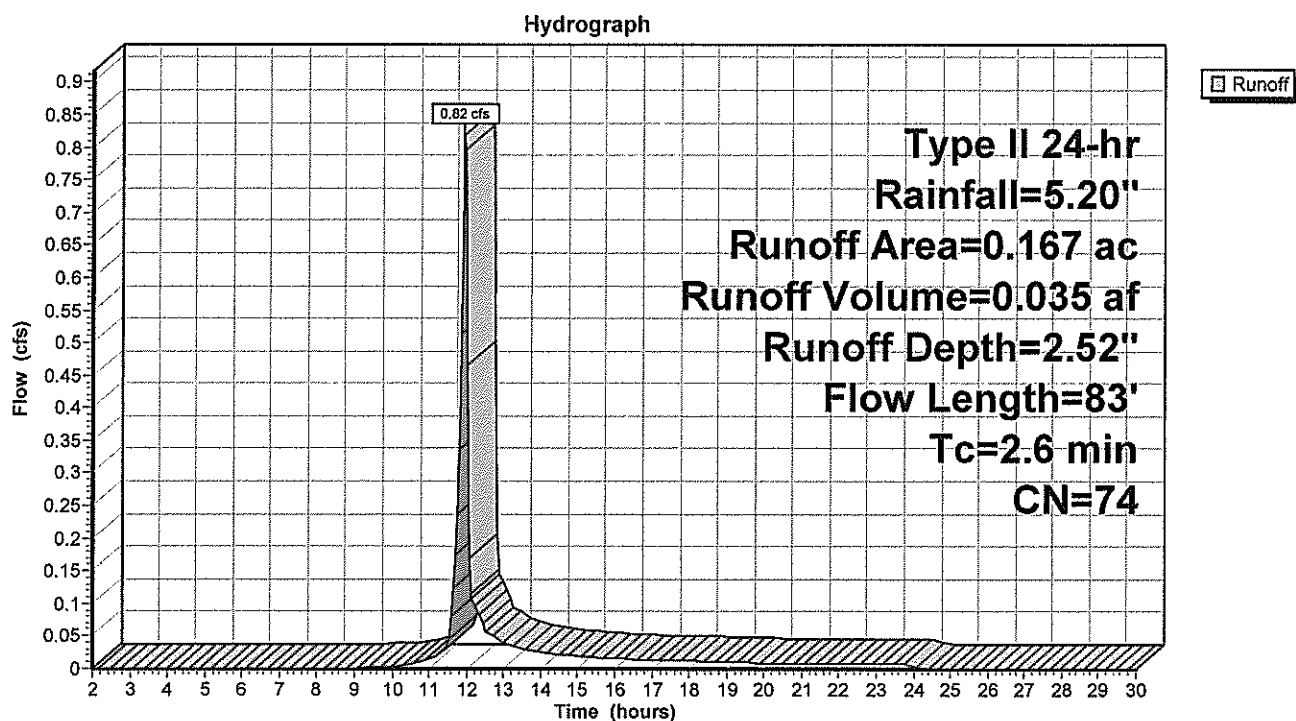
Summary for Subcatchment 4P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.82 cfs @ 11.93 hrs, Volume= 0.035 af, Depth= 2.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=5.20"

Area (ac)	CN	Description
0.167	74	>75% Grass cover, Good, HSG C
0.167		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	30	0.1453	0.21		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$
0.2	53	0.0967	5.01		Shallow Concentrated Flow, Unpaved $K_v=16.1$ fps
2.6	83	Total			

Subcatchment 4P: (new Subcat)

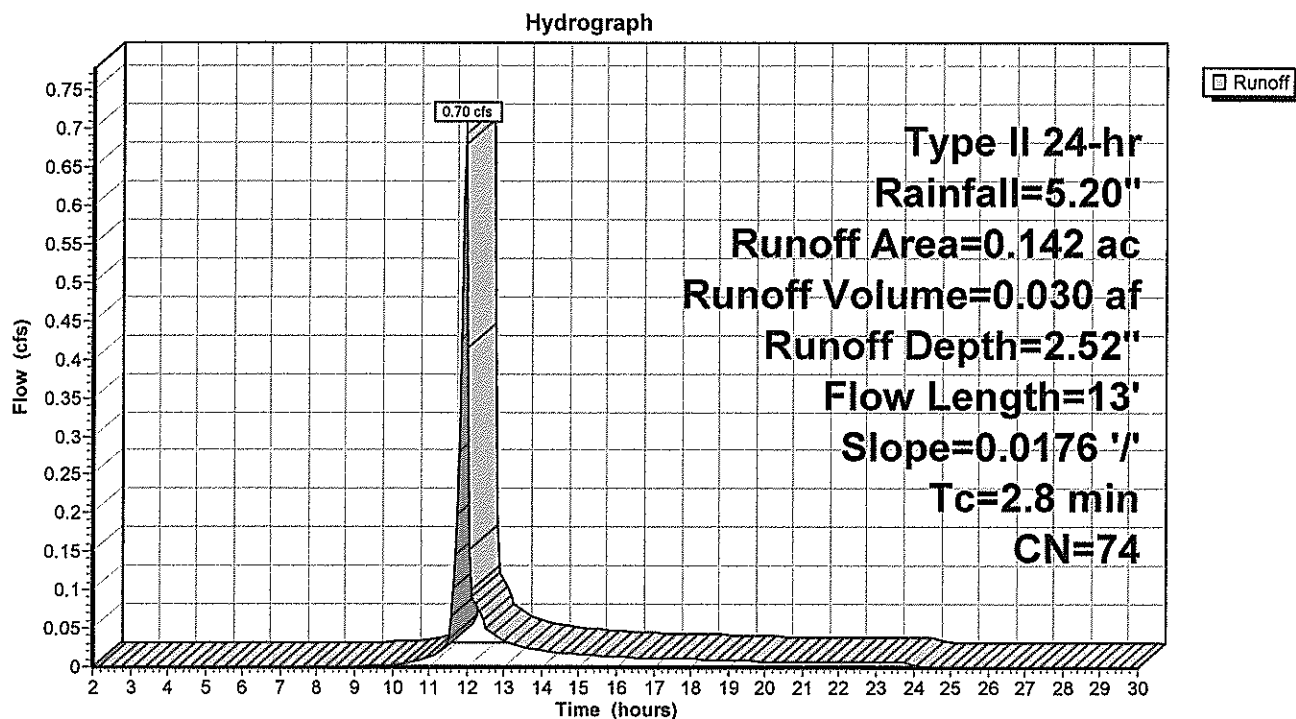
Summary for Subcatchment 5P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.70 cfs @ 11.94 hrs, Volume= 0.030 af, Depth= 2.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=5.20"

Area (ac)	CN	Description
0.142	74	>75% Grass cover, Good, HSG C
0.142		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.8	13	0.0176	0.08		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 5P: (new Subcat)

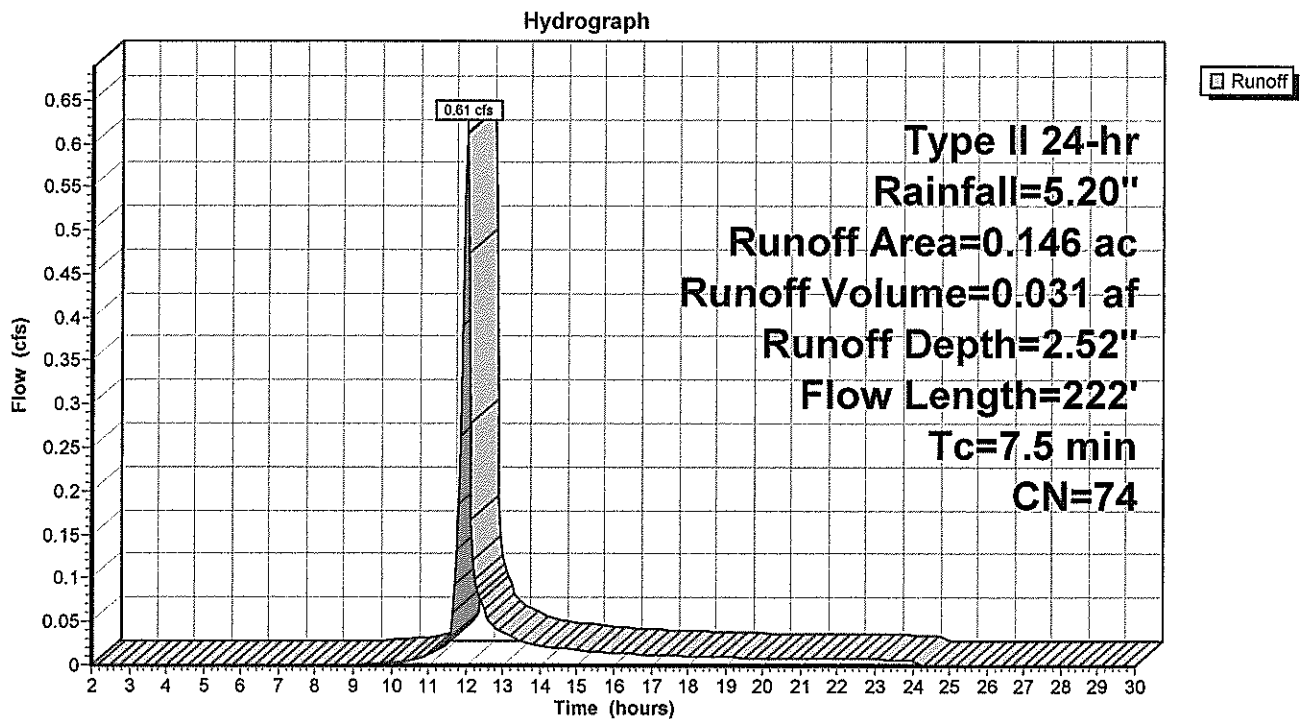
Summary for Subcatchment 6P: (new Subcat)

Runoff = 0.61 cfs @ 11.99 hrs, Volume= 0.031 af, Depth= 2.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs
Type II 24-hr Rainfall=5.20"

Area (ac)	CN	Description
0.146	74	>75% Grass cover, Good, HSG C
0.146		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.9	60	0.0400	0.15		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"
0.6	162	0.0775	4.18		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
7.5	222	Total			

Subcatchment 6P: (new Subcat)

Summary for Pond DET1: (new Pond)

Inflow Area = 1.287 ac, 67.91% Impervious, Inflow Depth = 4.09"
 Inflow = 9.22 cfs @ 11.93 hrs, Volume= 0.439 af
 Outflow = 4.30 cfs @ 12.02 hrs, Volume= 0.439 af, Atten= 53%, Lag= 5.2 min
 Primary = 4.30 cfs @ 12.02 hrs, Volume= 0.439 af

Routing by Stor-Ind method, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs
 Peak Elev= 983.76' @ 12.02 hrs Surf.Area= 0.088 ac Storage= 0.126 af

Plug-Flow detention time= 27.3 min calculated for 0.438 af (100% of inflow)
 Center-of-Mass det. time= 27.4 min (806.2 - 778.8)

Volume	Invert	Avail.Storage	Storage Description
#1	982.03'	0.211 af	36.0" Round Pipe Storage L= 1,300.0'

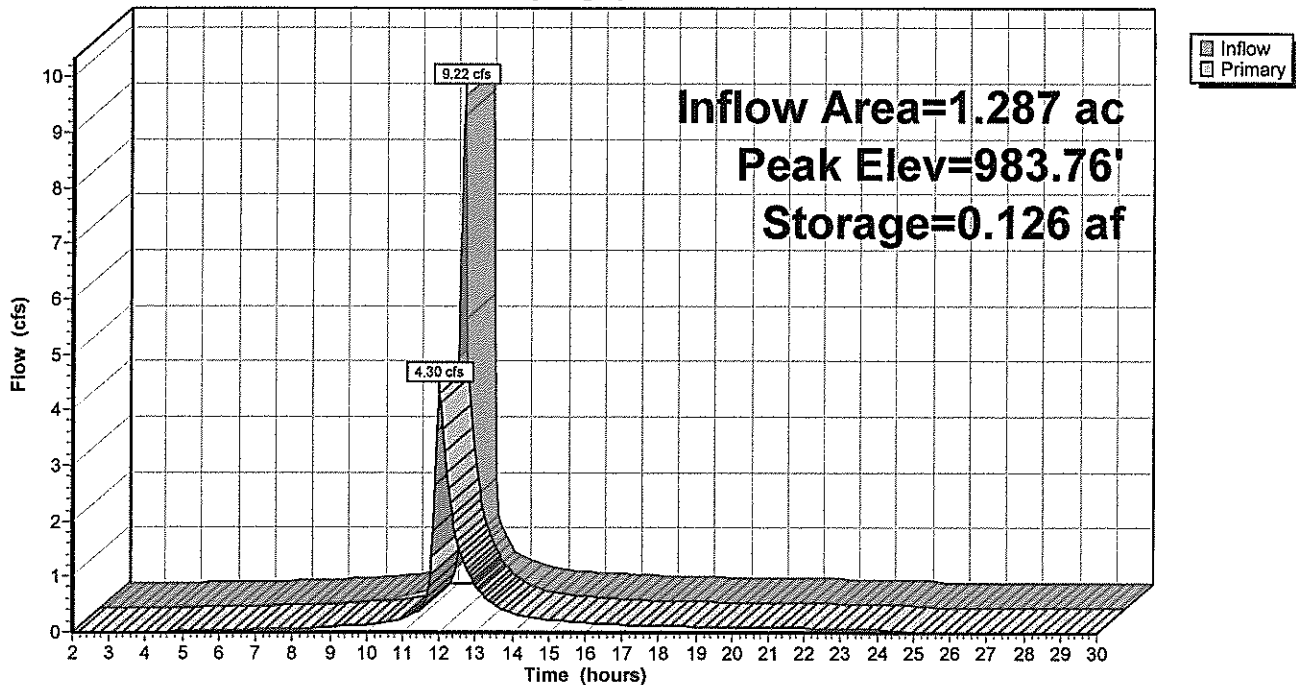
Device	Routing	Invert	Outlet Devices
#1	Primary	982.03'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28) Head (feet) 0.00 1.03 1.03 1.93 1.93 3.00 Width (feet) 0.50 0.50 0.79 0.79 2.50 2.50

Primary OutFlow Max=4.21 cfs @ 12.02 hrs HW=983.74' (Free Discharge)

↑1=Custom Weir/Orifice (Weir Controls 4.21 cfs @ 3.99 fps)

Pond DET1: (new Pond)

Hydrograph



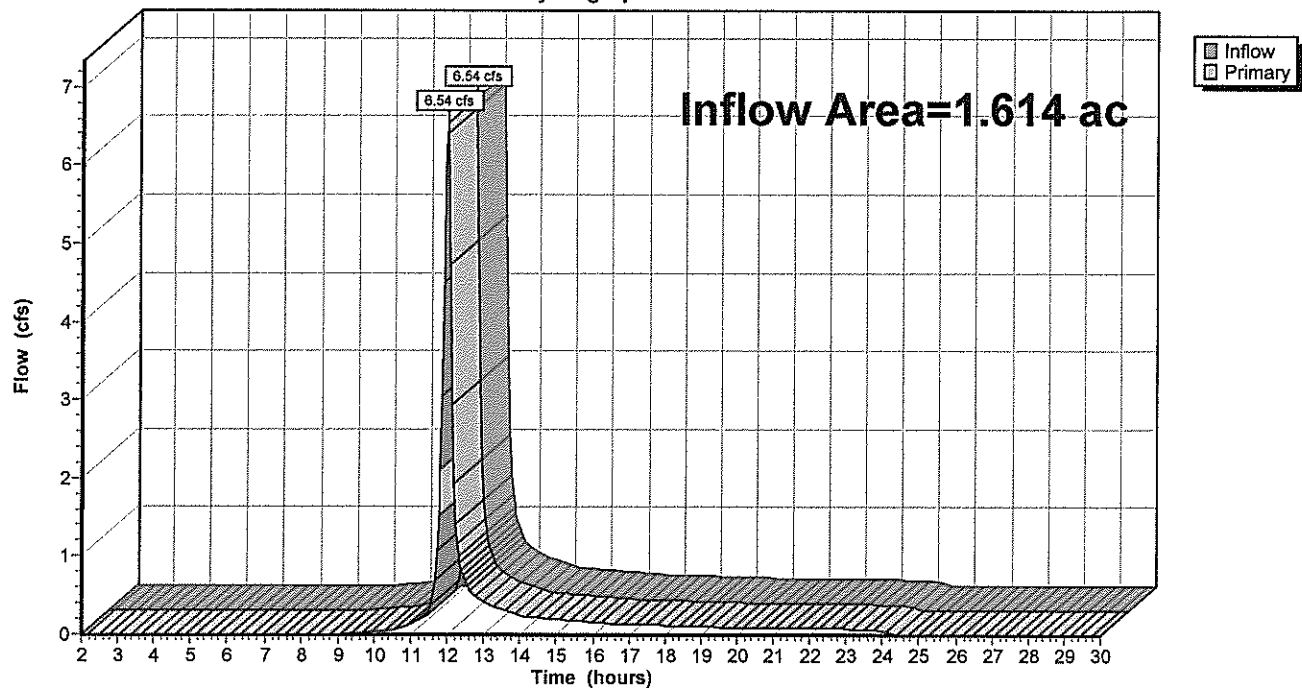
Summary for Link 4E: (new Link)

Inflow Area = 1.614 ac, 0.00% Impervious, Inflow Depth = 2.52"
Inflow = 6.54 cfs @ 11.98 hrs, Volume= 0.340 af
Primary = 6.54 cfs @ 11.98 hrs, Volume= 0.340 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs

Link 4E: (new Link)

Hydrograph



Summary for Link 10L: (new Link)

Inflow Area = 1.614 ac, 54.15% Impervious, Inflow Depth = 3.77"
Inflow = 5.38 cfs @ 11.99 hrs, Volume= 0.508 af
Primary = 5.38 cfs @ 11.99 hrs, Volume= 0.508 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs

Link 10L: (new Link)

Hydrograph

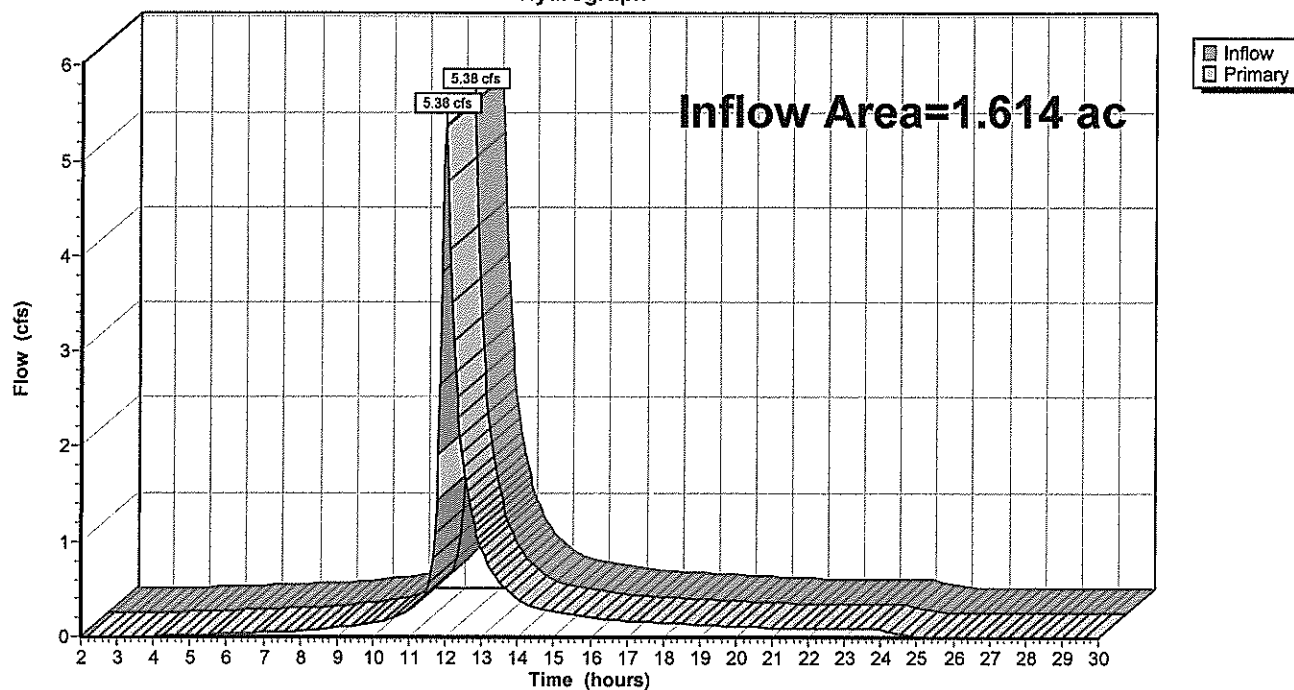
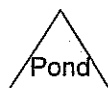
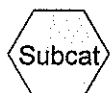
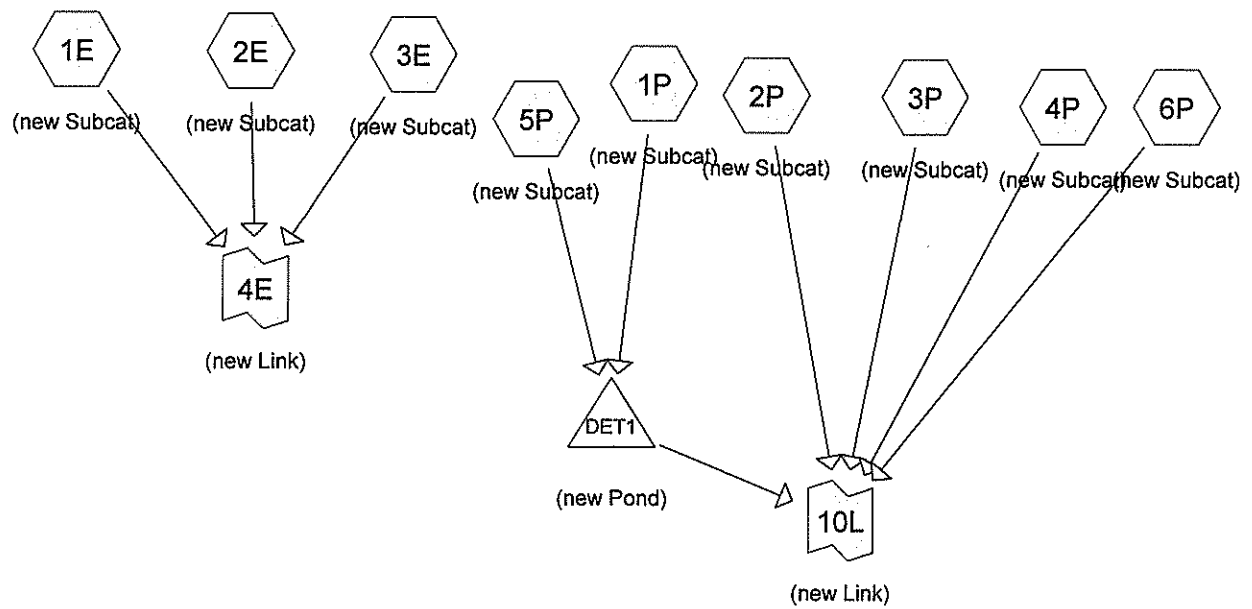


Exhibit 4
100-year Storm Calculations



Routing Diagram for 400 NW 72 Street

Prepared by HP, Printed 7/20/2023

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400 NW 72 Street

Prepared by HP

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Page 2

Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
2.354	74	>75% Grass cover, Good, HSG C (1E, 1P, 2E, 2P, 3E, 3P, 4P, 5P, 6P)
0.874	98	Paved parking, HSG C (1P)
3.228	80	TOTAL AREA

Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
3.228	HSG C	1E, 1P, 2E, 2P, 3E, 3P, 4P, 5P, 6P
0.000	HSG D	
0.000	Other	
3.228		TOTAL AREA

400 NW 72 Street

Prepared by HP

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Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	2.354	0.000	0.000	2.354	>75% Grass cover, Good	1E, 1P, 2E, 2P, 3E, 3P, 4P, 5P, 6P
0.000	0.000	0.874	0.000	0.000	0.874	Paved parking	1P
0.000	0.000	3.228	0.000	0.000	3.228	TOTAL AREA	

Time span=2.00-30.00 hrs, dt=0.05 hrs, 561 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1E: (new Subcat) Runoff Area=0.544 ac 0.00% Impervious Runoff Depth=4.57"
 Flow Length=81' Slope=0.0247 '/' Tc=10.6 min CN=74 Runoff=3.65 cfs 0.207 af

Subcatchment 1P: (new Subcat) Runoff Area=1.145 ac 76.33% Impervious Runoff Depth=6.65"
 Flow Length=249' Tc=2.8 min CN=92 Runoff=12.83 cfs 0.634 af

Subcatchment 2E: (new Subcat) Runoff Area=0.017 ac 0.00% Impervious Runoff Depth=4.57"
 Flow Length=30' Slope=0.0732 '/' Tc=3.1 min CN=74 Runoff=0.15 cfs 0.006 af

Subcatchment 2P: (new Subcat) Runoff Area=0.007 ac 0.00% Impervious Runoff Depth=4.57"
 Flow Length=33' Slope=0.0758 '/' Tc=3.3 min CN=74 Runoff=0.06 cfs 0.003 af

Subcatchment 3E: (new Subcat) Runoff Area=1.053 ac 0.00% Impervious Runoff Depth=4.57"
 Flow Length=237' Tc=5.8 min CN=74 Runoff=8.24 cfs 0.401 af

Subcatchment 3P: (new Subcat) Runoff Area=0.007 ac 0.00% Impervious Runoff Depth=4.57"
 Flow Length=43' Slope=0.5116 '/' Tc=1.9 min CN=74 Runoff=0.06 cfs 0.003 af

Subcatchment 4P: (new Subcat) Runoff Area=0.167 ac 0.00% Impervious Runoff Depth=4.57"
 Flow Length=83' Tc=2.6 min CN=74 Runoff=1.45 cfs 0.064 af

Subcatchment 5P: (new Subcat) Runoff Area=0.142 ac 0.00% Impervious Runoff Depth=4.57"
 Flow Length=13' Slope=0.0176 '/' Tc=2.8 min CN=74 Runoff=1.23 cfs 0.054 af

Subcatchment 6P: (new Subcat) Runoff Area=0.146 ac 0.00% Impervious Runoff Depth=4.57"
 Flow Length=222' Tc=7.5 min CN=74 Runoff=1.10 cfs 0.056 af

Pond DET1: (new Pond) Peak Elev=984.37' Storage=0.177 af Inflow=14.06 cfs 0.688 af
 Outflow=8.78 cfs 0.688 af

Link 4E: (new Link) Inflow=11.69 cfs 0.615 af
 Primary=11.69 cfs 0.615 af

Link 10L: (new Link) Inflow=10.81 cfs 0.813 af
 Primary=10.81 cfs 0.813 af

Total Runoff Area = 3.228 ac Runoff Volume = 1.427 af Average Runoff Depth = 5.31"
72.92% Pervious = 2.354 ac 27.08% Impervious = 0.874 ac

Summary for Subcatchment 1E: (new Subcat)

Runoff = 3.65 cfs @ 12.02 hrs, Volume= 0.207 af, Depth= 4.57"

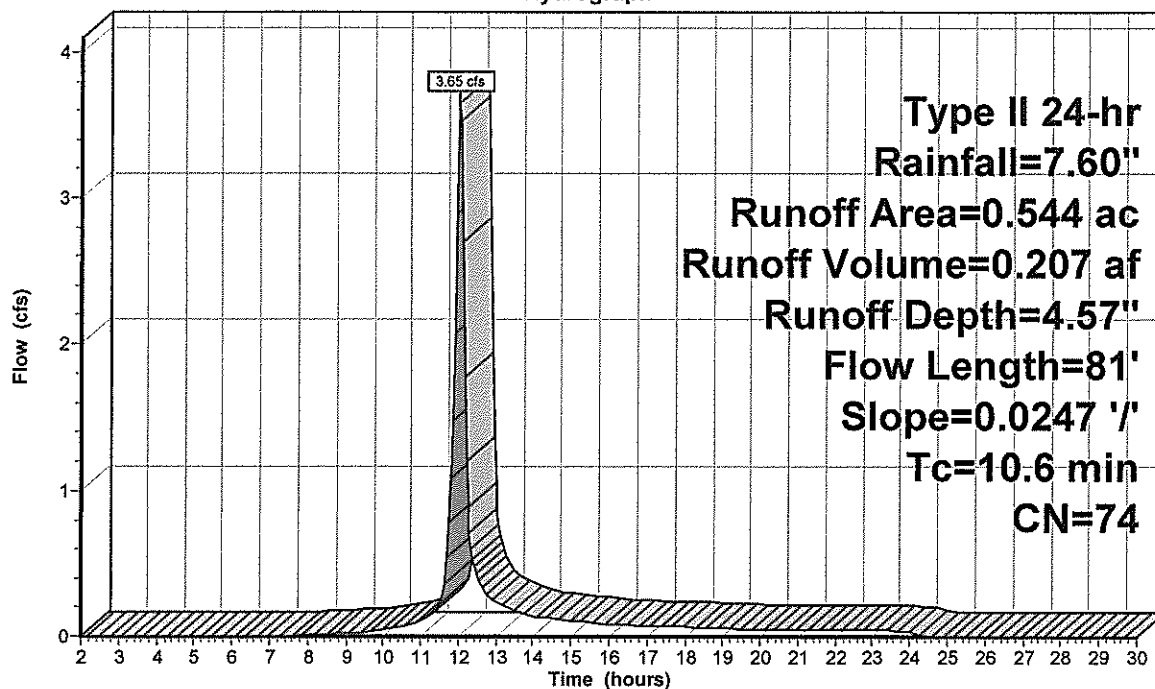
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs
Type II 24-hr Rainfall=7.60"

Area (ac)	CN	Description
0.544	74	>75% Grass cover, Good, HSG C
0.544		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.6	81	0.0247	0.13		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 1E: (new Subcat)

Hydrograph



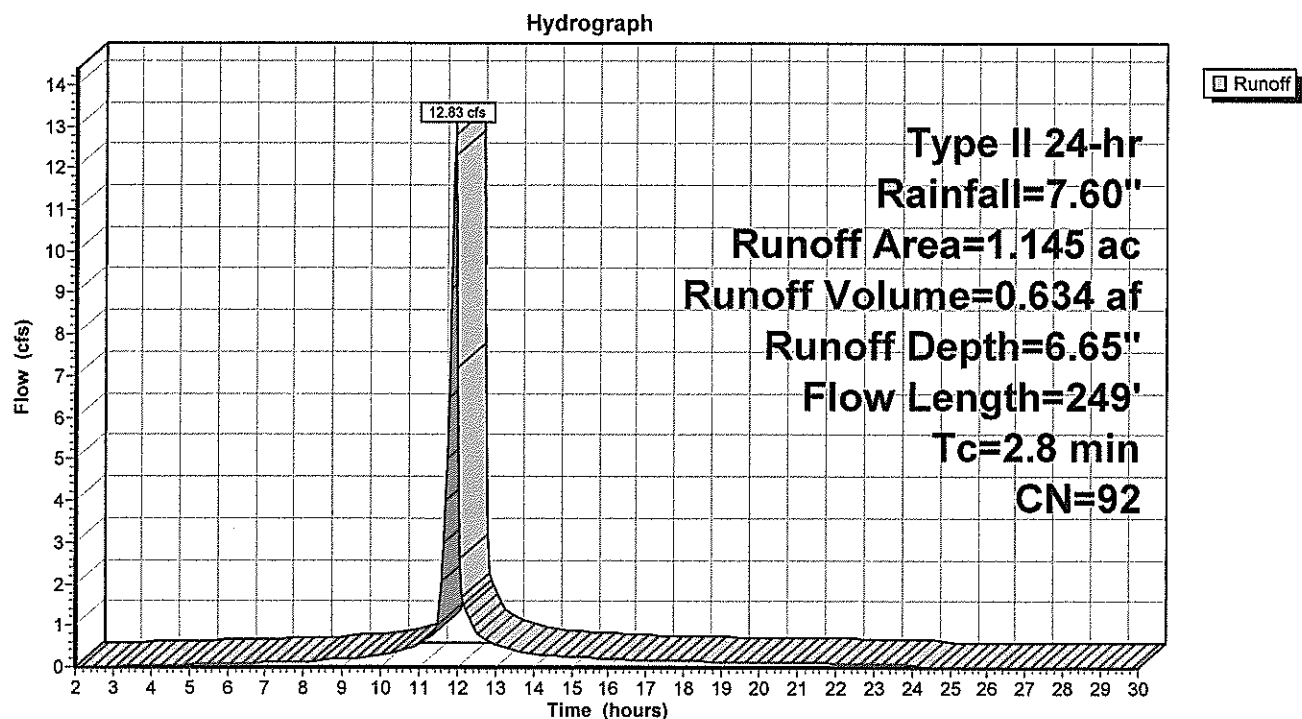
Summary for Subcatchment 1P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 12.83 cfs @ 11.93 hrs, Volume= 0.634 af, Depth= 6.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=7.60"

Area (ac)	CN	Description
0.271	74	>75% Grass cover, Good, HSG C
0.874	98	Paved parking, HSG C
1.145	92	Weighted Average
0.271		23.67% Pervious Area
0.874		76.33% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0065	0.92		Sheet Flow, Smooth surfaces n= 0.011 P2= 3.50"
1.0	149	0.0151	2.49		Shallow Concentrated Flow, Paved Kv= 20.3 fps
2.8	249	Total			

Subcatchment 1P: (new Subcat)

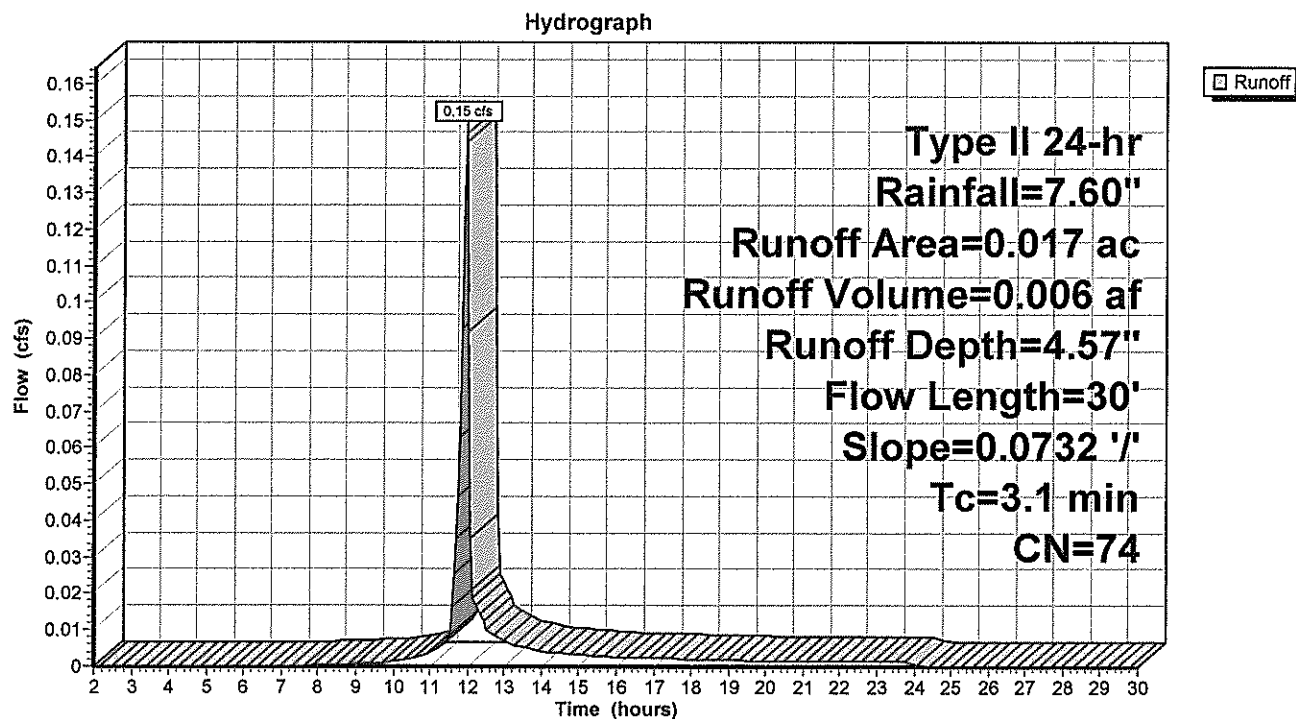
Summary for Subcatchment 2E: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.15 cfs @ 11.94 hrs, Volume= 0.006 af, Depth= 4.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=7.60"

Area (ac)	CN	Description
0.017	74	>75% Grass cover, Good, HSG C
0.017		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	30	0.0732	0.16		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 2E: (new Subcat)

Summary for Subcatchment 2P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.06 cfs @ 11.94 hrs, Volume= 0.003 af, Depth= 4.57"

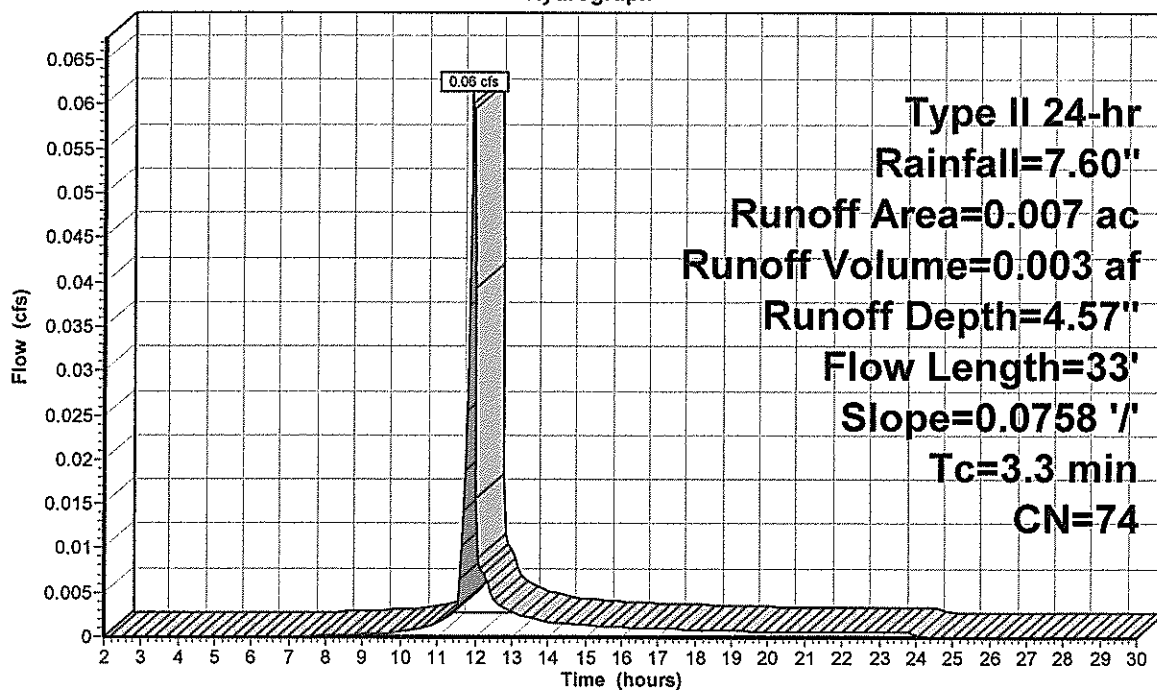
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=7.60"

Area (ac)	CN	Description
0.007	74	>75% Grass cover, Good, HSG C
0.007		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	33	0.0758	0.17		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$

Subcatchment 2P: (new Subcat)

Hydrograph



Runoff

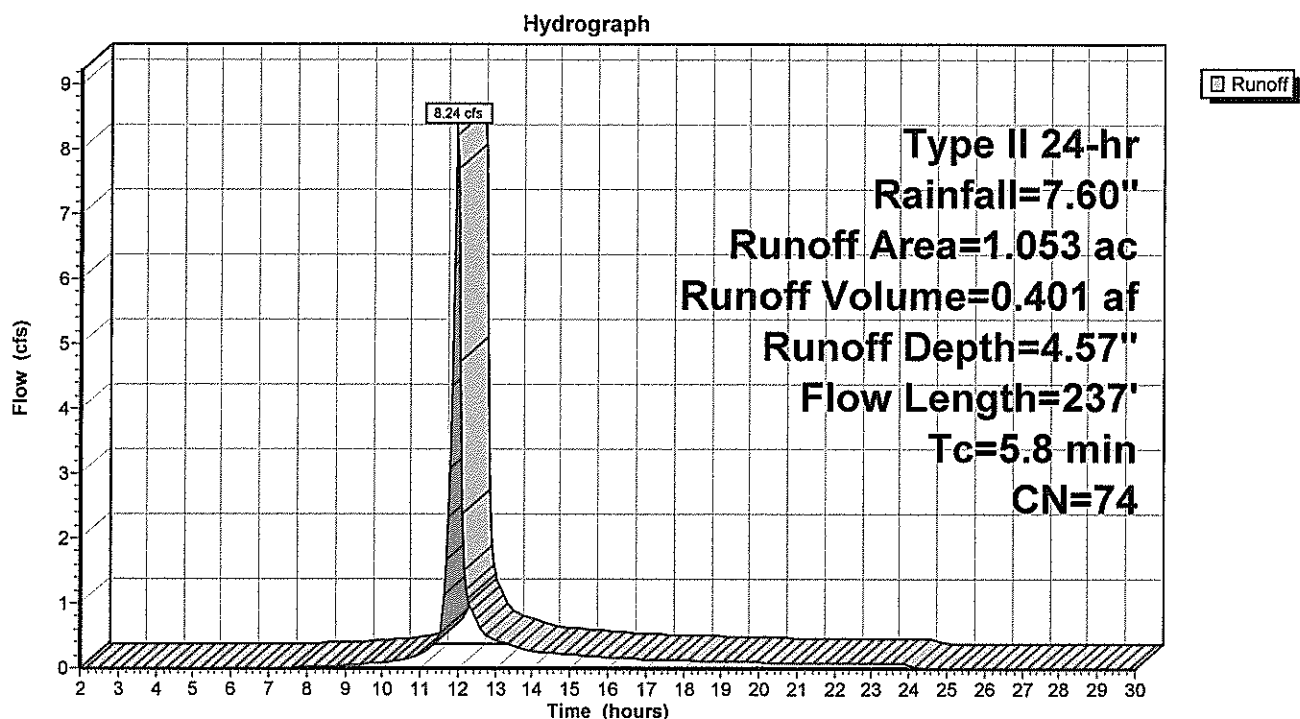
Summary for Subcatchment 3E: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 8.24 cfs @ 11.97 hrs, Volume= 0.401 af, Depth= 4.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=7.60"

Area (ac)	CN	Description
1.053	74	>75% Grass cover, Good, HSG C
1.053		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.4	100	0.2000	0.31		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$
0.4	137	0.1339	5.49		Shallow Concentrated Flow, Grassed Waterway $K_v=15.0$ fps
5.8	237	Total			

Subcatchment 3E: (new Subcat)

Summary for Subcatchment 3P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.06 cfs @ 11.92 hrs, Volume= 0.003 af, Depth= 4.57"

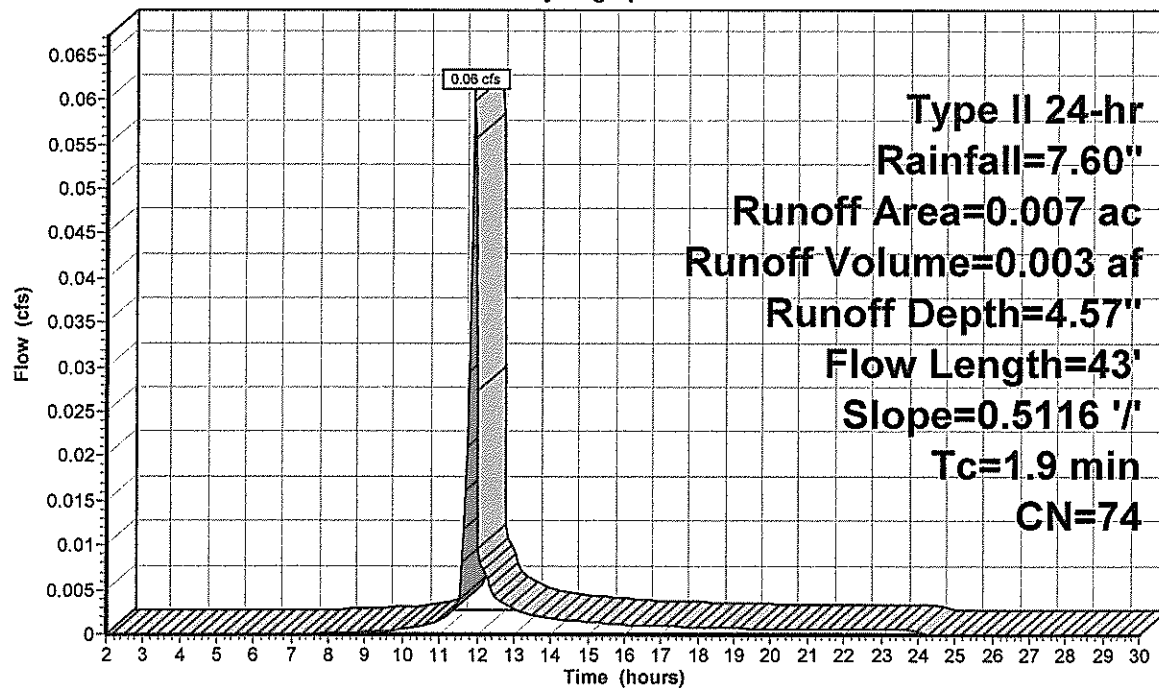
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=7.60"

Area (ac)	CN	Description
0.007	74	>75% Grass cover, Good, HSG C
0.007		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	43	0.5116	0.38		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 3P: (new Subcat)

Hydrograph



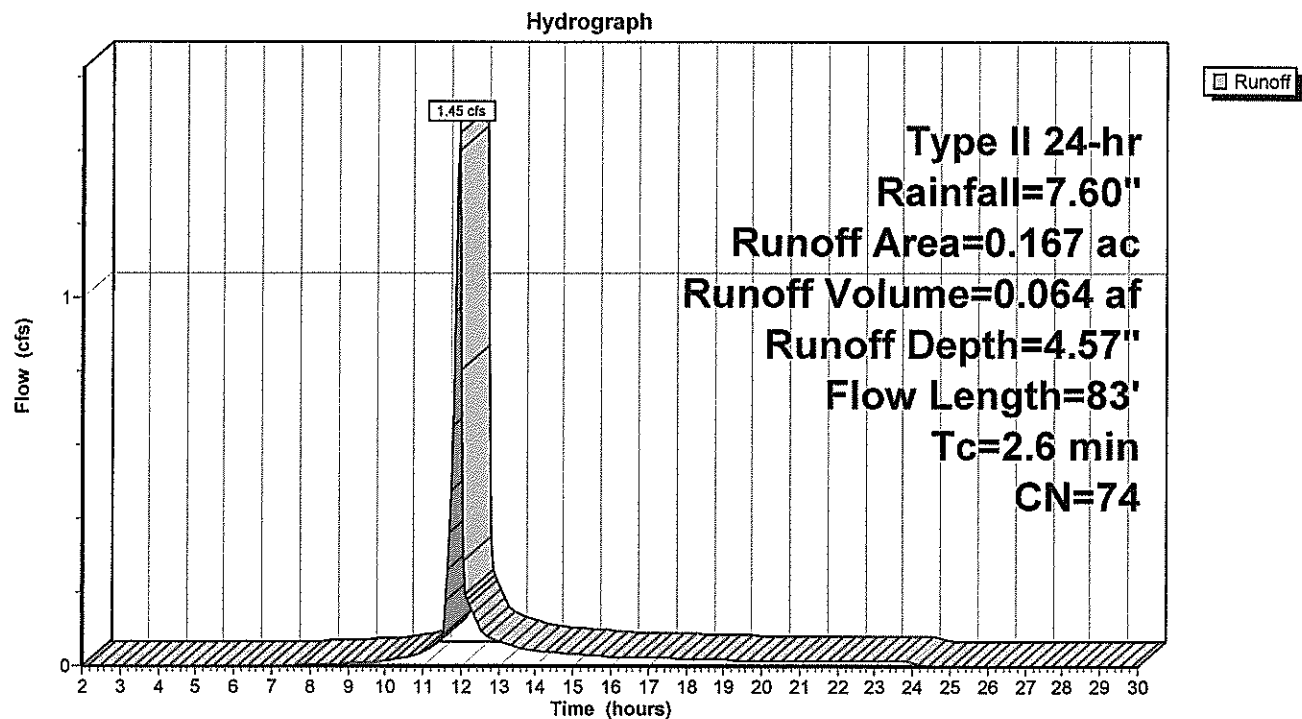
Summary for Subcatchment 4P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 1.45 cfs @ 11.93 hrs, Volume= 0.064 af, Depth= 4.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=7.60"

Area (ac)	CN	Description
0.167	74	>75% Grass cover, Good, HSG C
0.167		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	30	0.1453	0.21		Sheet Flow, Grass: Dense $n=0.240$ $P2=3.50"$
0.2	53	0.0967	5.01		Shallow Concentrated Flow, Unpaved $K_v=16.1$ fps
2.6	83	Total			

Subcatchment 4P: (new Subcat)

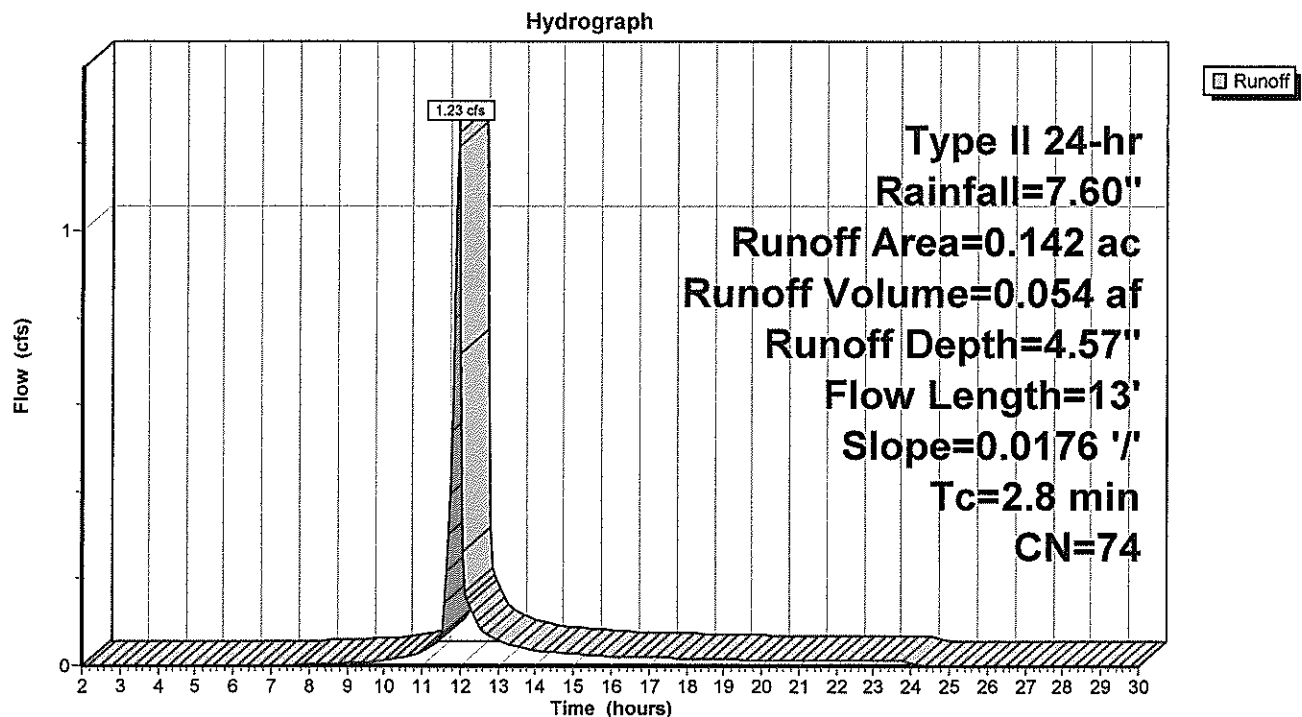
Summary for Subcatchment 5P: (new Subcat)[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 1.23 cfs @ 11.93 hrs, Volume= 0.054 af, Depth= 4.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, $dt=0.05$ hrs
Type II 24-hr Rainfall=7.60"

Area (ac)	CN	Description
0.142	74	>75% Grass cover, Good, HSG C
0.142		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.8	13	0.0176	0.08		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"

Subcatchment 5P: (new Subcat)

Summary for Subcatchment 6P: (new Subcat)

Runoff = 1.10 cfs @ 11.99 hrs, Volume= 0.056 af, Depth= 4.57"

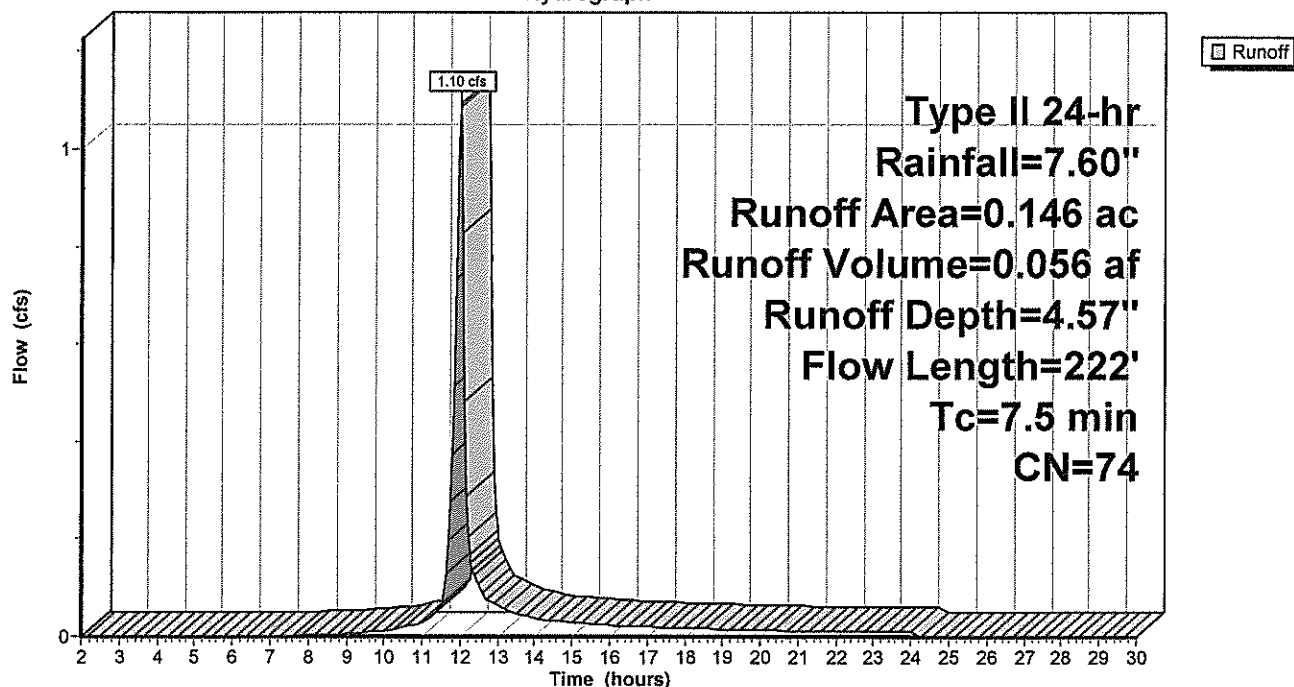
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs
Type II 24-hr Rainfall=7.60"

Area (ac)	CN	Description
0.146	74	>75% Grass cover, Good, HSG C
0.146		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.9	60	0.0400	0.15		Sheet Flow, Grass: Dense n= 0.240 P2= 3.50"
0.6	162	0.0775	4.18		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
7.5	222	Total			

Subcatchment 6P: (new Subcat)

Hydrograph



Summary for Pond DET1: (new Pond)

Inflow Area = 1.287 ac, 67.91% Impervious, Inflow Depth = 6.42"
 Inflow = 14.06 cfs @ 11.93 hrs, Volume= 0.688 af
 Outflow = 8.78 cfs @ 12.00 hrs, Volume= 0.688 af, Atten= 38%, Lag= 4.3 min
 Primary = 8.78 cfs @ 12.00 hrs, Volume= 0.688 af

Routing by Stor-Ind method, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs
 Peak Elev= 984.37' @ 12.00 hrs Surf.Area= 0.074 ac Storage= 0.177 af

Plug-Flow detention time= 25.7 min calculated for 0.688 af (100% of inflow)
 Center-of-Mass det. time= 25.5 min (793.2 - 767.7)

Volume	Invert	Avail.Storage	Storage Description
#1	982.03'	0.211 af	36.0" Round Pipe Storage L= 1,300.0'

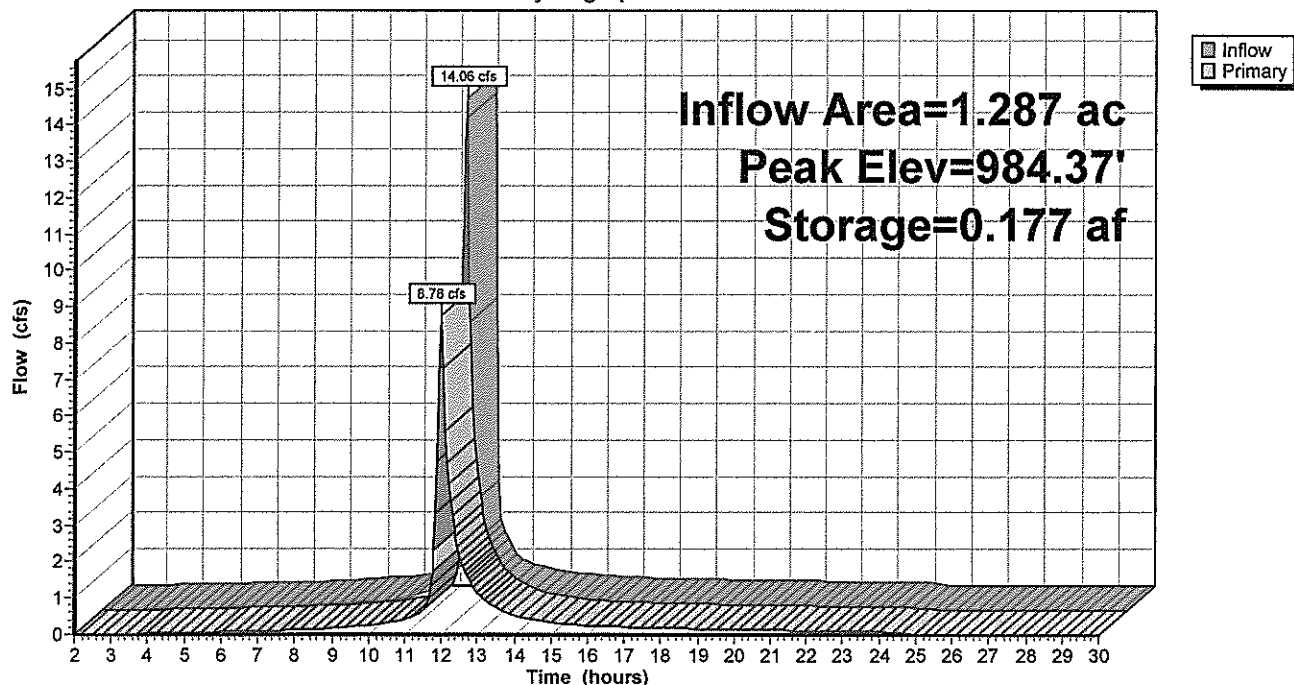
Device	Routing	Invert	Outlet Devices
#1	Primary	982.03'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28) Head (feet) 0.00 1.03 1.03 1.93 1.93 3.00 Width (feet) 0.50 0.50 0.79 0.79 2.50 2.50

Primary OutFlow Max=8.78 cfs @ 12.00 hrs HW=984.37' (Free Discharge)

↑1=Custom Weir/Orifice (Weir Controls 8.78 cfs @ 3.89 fps)

Pond DET1: (new Pond)

Hydrograph



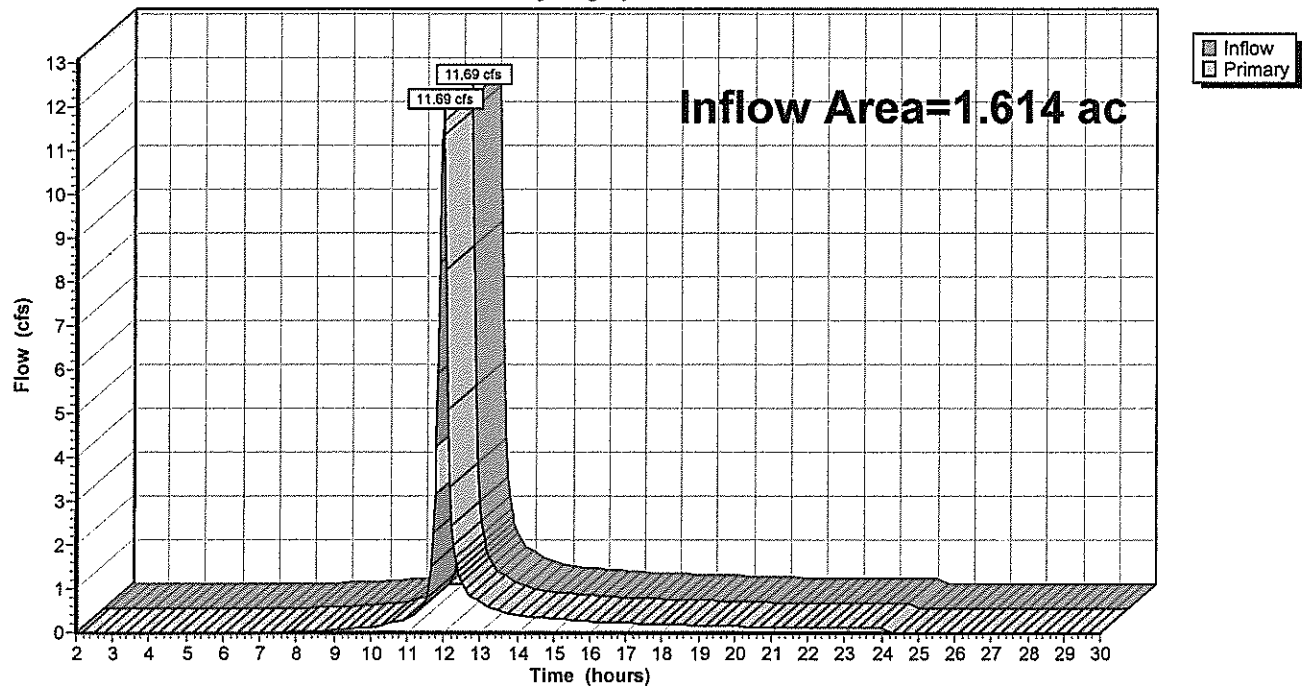
Summary for Link 4E: (new Link)

Inflow Area = 1.614 ac, 0.00% Impervious, Inflow Depth = 4.57"
Inflow = 11.69 cfs @ 11.98 hrs, Volume= 0.615 af
Primary = 11.69 cfs @ 11.98 hrs, Volume= 0.615 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs

Link 4E: (new Link)

Hydrograph



Summary for Link 10L: (new Link)

Inflow Area = 1.614 ac, 54.15% Impervious, Inflow Depth = 6.04"

Inflow = 10.81 cfs @ 11.99 hrs, Volume= 0.813 af

Primary = 10.81 cfs @ 11.99 hrs, Volume= 0.813 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 2.00-30.00 hrs, dt= 0.05 hrs

Link 10L: (new Link)

Hydrograph

